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## FLOW MONITORING IN STORMWATER TREATMENT AREA NO. 6



By<br>Muluneh Imru<br>Senior Engineer

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Hydrology and Hydraulics Division
Environmental Monitoring \& Assessment Department
South Florida Water Management District West Palm Beach, Florida

## EXECUTIVE SUMMARY

This report describes the criteria, equations and procedures used to quantify flow through Stormwater Treatment Area No. 6 (STA-6). To evaluate the performance of STA-6 in terms of phosphorus reduction, it is essential that flows into and out of this constructed wetland be estimated using rigorous methods. This poses a challenge due to the configuration of the hydraulic structures and the complexity of water movement through the system.

Flow control structures at STA-6 include trapezoidal weirs (G601, G602 and G603) for inflow, and culverts with weir-box inlets (G354 and G393) for outflow. STA-6 receives agricultural drainage delivered through the pumps at G600. In STA-6, like in several other District sites, two or more structure types are built next to each other. At such sites, there is no separate stage monitoring for each structure type. This is especially true where a typical structure is a culvert with a weir-box inlet (G354 and G393). While culvert flow conditions prevail over the downstream portion of such a combination structure, weir flow characteristics may dominate at the inlet. The weir box at the inlet of a typical culvert in STA-6 is needed to retain water in the treatment cell and keep it wet as much as possible.

Procedures have been developed to monitor all inflows and outflows at STA-6 Section 1. The criteria and steps to be followed for computing flows into STA- 6 cells through the inflow weirs have been established. A method has been presented that will enable the computation of flow through the weir box and gated-culvert combination structures at G354 and G393 (weir-culvert) in order to monitor outflows from each cell.

Data derived from these methods are validated by a good correlation between inflows at G600 and outflows through G354 and G393. The flows through G601, G602 and G603 are slightly different from G600 inflows, as well as the outflows through G354 and G393. There is room for improvement of the weir inflow estimates. It is also possible to gain some improvement on the overall accuracy of flow computation at STA-6 structures through streamgauging and calibration.

The criteria, equations and procedures developed for STA-6 can, with applicable adaptations, be used for flow monitoring at similar stations in other stormwater treatment areas when they come on line. The adaptations will primarily involve determining sitespecific coefficients for similar structure types on the basis of streamgauging data.

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## Notation

The following notations are used to characterize flow through weirs and culverts:

| A | = | flow cross section (maximum $\mathrm{A}_{0}$ ) |
| :---: | :---: | :---: |
| $\mathrm{Ag}_{\mathrm{g}}$ | = | entrance cross section (gate opening) area |
| $\mathrm{A}_{0}$ | = | culvert cross section area $=\pi \mathrm{D}^{2} / 4$ |
| B | $=$ | culvert bottom width or weir length (bottom width of trapezoidal section) |
| $\mathrm{B}_{\mathrm{m}}$ | = | average width of trapezoidal weir section under water |
| $\mathrm{B}_{\text {e }}$ | $=$ | effective weir length |
| $\mathrm{c}_{\mathrm{d}}$ | $=$ | culvert discharge coefficient |
| $\mathrm{c}_{\mathrm{w}}$ | $=$ | weir flow coefficient |
| CW | = | (approach) channel width |
| D | $=$ | diameter of circular culvert or depth of box culvert |
| $\mathrm{D}_{\mathrm{m}}$ | $=$ | mean depth (area/water surface width) |
| e | $=$ | width of bank or side of trapezoidal section under water |
| h | $=$ | tailwater depth above weir crest or above culvert invert or flow depth at any location |
| $\mathrm{h}_{1}$ | $=$ | stage above datum upstream of inlet weir box |
| $\mathrm{h}_{2}$ | $=$ | stage above datum at upstream face of culvert inside the weir box |
| $\mathrm{h}_{3}$ | = | water depth above the downstream invert elevation at the location of the invert. |
| $\mathrm{h}_{4}$ | $=$ | tailwater depth above the downstream invert elevation. |
| $\mathrm{h}_{\text {c }}$ | $=$ | critical flow depth |
| $\mathrm{h}_{\mathrm{f}}$ | = | head loss due to friction |
| $\mathrm{h}_{\mathrm{w}}$ | $=$ | elevation difference between weir crest and downstream invert |
| H | = | headwater depth above weir crest or above culvert invert |
| HWE | $=$ | head water elevation |

\(\left.\begin{array}{lll}INEL \& = \& inlet invert elevation <br>
\mathrm{k}_{\mathrm{e}} \& = \& minor (entrance) loss coefficient (default \mathrm{K}_{\mathrm{e}}=0.5 ) <br>
\mathrm{L} \& = \& length of culvert barrel <br>
\mathrm{m} \& = \& side slope(horizontal:vertical) of trapezoidal flow section <br>

\mathrm{n} \& = \& Manning's roughness coefficient\end{array}\right]\)| ND | $=$ |
| :--- | :--- |
| v | vertical depth of inclined surface of trapezoidal weir (notch depth) |
| N | $=$ |
| number of contractions in weir flow |  |

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### 1.0 INTRODUCTION

The Everglades Forever Act (EFA) mandated the South Florida Water Management District (District) to implement the Everglades Construction Project (ECP) as an important step for restoring and protecting the Everglades ecosystem. Stormwater Treatment Area No. 6 (STA-6) is a component of the ECP. It was constructed in 1997 and has been in operation since December 1997.

STA-6 is a constructed wetland designed to reduce total phosphorus in the drainage water coming primarily from the Everglades Agricultural Area (EAA). Comprised of two parts (Northern Cell 5 and Southern Cell3), the wetland provides an effective treatment area of about 870 acres for drainage from approximately 10,400 acres of agricultural land. The inflow into STA-6 comes through G600, a pump station owned and operated by United States Sugar Corporation (USSC). Three trapezoidal weirs (G601, G602 and G603) control inflow into STA-6. Six culverts with weir-box inlets (G354A-C and G393A-C) control outflow from Cell 5 and Cell 3. Bypass flow control is provided at G604. All flows from G354, G393 and G604 are discharged out of STA-6 via the terminal structure (culvert) G607.

Flow monitoring is conducted at more than 400 water control structures in the District. The major types of flow monitoring stations include spillways, weirs, culverts, pumping stations and open channel reaches. At many of the flow monitoring sites in the District, flow is controlled by one type of structure. In such a case, the flow monitoring equations used are those appropriate for the particular structure. However, at some sites two or more structure types are joined in series affecting flow through the station. At such sites, there is not enough space between the structures to assess the independent effects of each structure on the flow. There is no separate stage monitoring for each structure type. This is especially true at those sites whose typical structure is a weir-culvert combination, i.e., where a weir box discharges directly into a culvert. While culvert flow conditions prevail over the downstream portion of such a combination structure, the flow characteristics of the inlet may be those of a weir.

At the outlets of STA-6, as in other STAs, there are gated culverts with weir-box inlets. The weir box at the inlet of a typical culvert in STA-6 helps to retain some water in the treatment cells to keep the treatment cells moist at all times (EES 1997). The inflow into the culvert is affected by the presence of the weir box at the inlet.

The effects of various structure shapes and types on water flow have been investigated in the past and appropriate equations have been developed to estimate velocity, discharge and related parameters. Standard methods of computing flow through water control structures are presented in other District publications (Otero 1995). Most textbooks in hydraulics provide equations, criteria and procedures for estimating flow through a simple structure, that is, a structure consisting of only one hydraulic element, e.g. a weir. The available equations cannot, however, be directly applied when a site contains a series of joined hydraulic structures, e.g. a weir joined to a culvert (weir-box culvert). In such a structure, it is difficult to isolate the effect of each structure type on flow.


Figure 1. Project Location and Site Layout

A culvert with a weir type inlet poses a challenge to direct discharge estimation using existing flow computation procedures. In computing flow through a culvert with a weir inlet, several key issues need to be addressed:

- identification of the control (the weir, the culvert inlet or the culvert outlet);
- effects of transition from weir-controlled to culvert-controlled flow or vice-versa;
- occurrence of critical flow; and
- the influence of the tailwater stage on the flow.

This report describes the criteria, equations and procedures used for flow monitoring in STA-6.
The following section states the objectives of this report. Sections 3 through 8 present the equations and procedures used to estimate flow at STA-6 weirs and culverts. Flow estimation parameters and qualitative evaluation of flow estimates are given in Section 9 and Section 10, respectively. The last section provides conclusions and recommendations.

### 2.0 OBJECTIVES

The overall objective of this study was to provide validated means for estimating inflows and outflows for STA-6. This work will be useful for STA-6 performance optimization research and permit compliance
monitoring. We currently monitor inflow into STA-6 at G600, the pumping station owned and operated by US Sugar Corporation (USSC). Water delivery into Cell 5 takes place through two inflow weirs, G601 and G602. Inflow into Cell 3 is through weir G603. Weirs G601, G602 and G603 have trapezoidal sections and, therefore, procedures are needed to compute flows into the treatment cells through the trapezoidal weirs.

Outflow from STA-6 was monitored at G606, the UVM (ultrasonic velocity meter) site in the discharge canal for permit compliance until March 2001. Because of possible influences from seepage and drawdown in the supply canal, flow through the G606 UVM was, at times, different from surface outflows from the treatment cells. In order to determine STA-6 outflows, it was necessary to calculate flows at G393 and G354. The structures at G393 and G354 are weir-culvert combinations requiring a flow computation procedure different from those employed for simple structures.

The purpose of this report is to document the results of planning and implementation of flow monitoring for STA-6, including:

- algorithms to compute flows into the treatment cells through the trapezoidal inflow weirs G601, G602 and G603;
- algorithms to compute discharge through G393 and G354, i.e., the outlets from Treatment Cell 3 and Treatment Cell 5, respectively;
- a methodology to determine control of flow through culverts with weir-box inlets; and
- an assessment of the results of flow monitoring in STA-6.

All equations are in the foot-pound-second system of units; i.e. all lengths are in feet ( ft .), all weights are in pounds (lb.), and all time dimensions are in seconds (s).

### 3.0 WEIR FLOW EQUATIONS

Discharge over a weir depends on the relative elevations of headwater, tailwater and weir crest. Depending on these relative elevations, weir flow is categorized as either free weir flow or submerged weir flow. The inflows considered in this study are uncontrolled, because there are no gates over the weirs. Since STA-6 inflow structures (G601, G602, G603) have no gates, the discussion in this study focuses on uncontrolled submerged and uncontrolled free (weir) flows.

STA-6 inflow structures are broad-crested trapezoidal weirs. Many hydraulics text books provide equations for estimating discharge through broad-crested weirs. The main difference shown between sharp-crested and broad-crested weirs is that the coefficient for broad-crested weirs is a function of upstream water depth and weir depth (Chow, 1959). Other than for the coeffiecient, the general form of the free flow equation for the broad-crested weir is similar to that of the sharp-crested weir Eq.(2). French (1985) notes that if the ratio of the total head $(\mathrm{H})$ over the crest to the thickness of the weir in the direction of flow is greater than 15 , the weir is sharp-crested, and he gives an equation each for a broad-crested rectangular weir and for a broad-crested v-notch. He also gives an equation for a broad-crested trapezoidal weir, which, however, does not exhibit a clear relationship to the equations of the rectangular and the v-notch types.

Featherstone et al. (1982) indicate that a trapezoidal notch may be considered as one rectangular weir of width B and two half notches (angle $\theta$ ). On this basis Eq. (5) is developed as the primary equation for computing free flow through a trapezoidal weir. The issue of sharp-crested and broad-crested configurations can be resolved when the discharge coefficient is determined through calibration. The discharge coefficient can be assigned a constant value at the initial stage. Equation (5) can be used for a rectangular section, with $\theta=0$, and for a v-notch, with $B=0$. The equation is robust enough to account for triangular, rectangular and trapezoidal sections.

### 3.1 Discharge through Weirs of Rectangular Flow Section

The weir length denotes the horizontal dimension of the crest over which water flows. The existence and configuration of walls at the ends of the weir crest may cause horizontal contractions of the flow section as represented by the effective weir length. The effective weir length $\left(B_{e}\right)$ is used to account for end contractions and is determined using Eq. (1).

$$
\begin{equation*}
\mathrm{B}_{\mathrm{e}}=\mathrm{B}-0.1 \mathrm{NH} \tag{1}
\end{equation*}
$$

In Eq. (1), $N=0,1$ or 2 depending on the number of end contractions, and $H$ is the total head over the weir. If the flow does not experience end contractions, if it is reasonable to assume so, N may be set to zero.

### 3.1.1 Free Weir Flow

This is a condition where the tailwater stage does not affect the discharge. The District's flow computation software (FLOW) uses the criterion (TWE-WCE)/(HWE-WCE) $\geq 0.5$ for uncontrolled free flow over a spillway, where HWE is headwater elevation, WCE is weir crest elevation and TWE is tailwater elevation. For free flow over a rectangular weir, it uses the criterion (TWE-WCE)/(HWE-WCE) $\leq 0.5$. It is necessary to standardize the criterion for free flow over weirs and spillways under uncontrolled conditions.

To standardize the criterion it is recommended that flow that meets the following criterion be under free weir flow condition:
(HWE - WCE) / (TWE-WCE) $\geq 1.5$
This criterion indicates that free weir flow is characterized by a headwater elevation (HWE) that is higher than the weir crest and has a depth above the weir crest of at least 1.5 times that of the tailwater. This assumes that a critical depth is created at the weir crest and relates to the principle that at critical flow, the total head is 1.5 times the static head. It also assumes that the effect of the approach velocity in the upstream channel is negligible.

When the free weir flow condition prevails over the crest of a rectangular weir section, Eq. (2) is used to estimate discharge, Q. It follows the definition that discharge is a product of velocity and flow section.

$$
\begin{equation*}
Q_{s}=c_{w} B_{e} H^{1.5} \tag{2}
\end{equation*}
$$

The free weir flow coefficient $\mathrm{C}_{\mathrm{w}}$ is determined through calibration. This coefficient has been expressed as a function of various parameters by different authors. For sharp-crested weirs, Chow (1959) and Henderson (1966, p. 175) give the discharge coefficient as a function of the ratio of water depth above weir to weir height $(H / w)$. For broad-crested weirs the coefficient is a function of upstream water depth and weir height, according to Chow (1959). Henderson (1966, p. 211) indicates that if a crest is broad enough to maintain hydrostatic pressure distribution in the flow across it, the flow will apparently be critical and the discharge can be readily determined using a modified form of Eq. (2). The equation gives a constant discharge coefficient of about 3.09. Since the equation has to be calibrated using field data, initially the theoretical equation can be applied with the constant coefficient. The subsequent calibration process needs to look at whether the discharge coefficient should be a constant or a variable, and what parameters must be used to determine the coefficient. It is necessary to investigate the effects of the various parameters identified, by different authors, as essential in the determination of the discharge coefficients for broad-crested weirs.

A definition sketch is given as Fig. 2 to show parameters used to calculate flow through a weir. The figure shows when the tailwater level is above, as well as below, the weir crest. When the tailwater elevation rises above the weir crest, it starts influencing the discharge over the weir. The effect of the tailwater on the discharge increases with increasing tailwater depth above the weir crest.


Figure 2. Parameters used to calculate flow through a weir

### 3.1.2 Submerged Weir Flow

Following the discussion and the recommendation made in Section 3.1.1, Free Weir Flow, the flow over a weir becomes submerged when the tailwater level exceeds the weir crest (Fig. 2) and the depth above the weir crest of the headwater is less than 1.5 times that of the tailwater. This condition assumes that if the headwater depth above the weir crest is not at least 1.5 times that of the tailwater, a critical depth is not attained at the weir crest.
$($ HWE - WCE $) /($ TWE - WCE $)<1.5$

For the same headwater stage, the discharge decreases with increasing tailwater stage. This is due to the decrease in the hydraulic gradient, which is an important factor causing flow. Submerged weir flow can be determined by multiplying the free weir flow equation by a submergence coefficient. For sharp-crested weirs and ogee spillways, the submergence coefficient is estimated using Eq. (3), known as the Villemonte Equation, below:

$$
\begin{equation*}
c_{s}=\left[1-\left(\frac{h}{H}\right)^{1.5}\right]^{0.385} \tag{3}
\end{equation*}
$$

Since the submergence coefficient in the form of Eq. (3) was developed for sharp-crested weirs, it can be adopted for broad-crested weirs and modified during calibration with streamgauging data as necessary. Its use is likely to give satisfactory results.

$$
\begin{equation*}
Q=c_{s} c_{w} B_{e} H^{1.5} \tag{4}
\end{equation*}
$$

By substituting Eq. (3) into Eq. (2), we obtain the submerged weir flow equation, Eq. (4).

### 3.2 Discharge Through Weirs of Trapezoidal Section

A trapezoidal weir section is shown in Figure 3. The top dimension CW indicates the width of the approach channel to the weir. ND denotes the depth of the trapezoidal weir. T represents the top width of the weir corresponding to the depth ND. This section considers various scenarios of headwater and tailwater stages and provides suitable discharge equations.

A trapezoidal flow section weir can be treated as a combination of a rectangular weir and a v-notch. Thus the flow through a trapezoidal weir can be fairly approximated by adding the flows through the triangular sections at the two ends treated together as the v-notch portion and the flow through the main rectangular-weir section in the middle. This section presents the algorithms to compute flow through a trapezoidal weir under various headwater and tailwater conditions. The side of a trapezoidal weir makes an angle, with the vertical defined by $\tan \theta=(\mathrm{T}-\mathrm{B}) /(2 \mathrm{ND})$.


Figure 3. Parameters used to compute flow through a Trapezoidal Flow Section Weir

### 3.2.1 Free weir flow

Free weir flow prevails when the tailwater stage does not influence the discharge. The literature provides a few equations for determining discharge through broad-crested trapezoidal weirs. French (1985, p. 339) gives a discharge equation in terms of critical depth ( $\mathrm{y}_{\mathrm{c}}$ ), an addition to the unknowns (discharge Q and coefficient $\mathrm{C}_{\mathrm{d}}$ ). A numerical solution for an equation with three unknowns requires a lot of assumptions, which may not be real. Further, French (1985, p. 343) notes that there are not enough published data to allow a generic estimate of the coefficients of discharge for trapezoidal broad-crested weirs.

An equation amenable to direct numerical solution is preferred. Equation (5) can be used to estimate free flow through a trapezoidal weir and can be solved directly. The following criterion characterizes free weir flow for a trapezoidal weir.

Criterion: $\quad \mathrm{ND} \geq \mathrm{H} \geq 1.5 \mathrm{~h}$ and $\mathrm{H}>0$

$$
\begin{equation*}
Q=C_{d} B H^{1.5}+C_{t} \tan \theta H^{2.5} \tag{5}
\end{equation*}
$$

The discharge through a trapezoidal weir under free flow condition can be estimated using Eq. (5), where $\mathrm{C}_{\mathrm{d}}$ is the discharge coefficient.

Equation (5) combines flows through a rectangular weir and a v-notch weir. This is consistent with the physical configuration of a trapezoidal weir, which may be considered as a rectangular flow section with a half v-notch section at each end of the rectangular section. When the sides are vertical (or $\theta$ approaches 0 ), Eq. (5) reduces to the free flow
equation for a rectangular weir, and if the crest length approaches zero ( B approaches 0 ), it reduces to the flow equation through a v-notch weir as it should.

### 3.2.2 Submerged flow

The following condition characterizes submerged weir flow for a trapezoidal weir. Submerged weir flow prevails when depth above the crest of the headwater is less than 1.5 times that of the tailwater.
Equation (6) can be used to estimate discharge through the trapezoidal weir under submerged conditions.

Criterion: $\quad \mathrm{ND} \geq \mathrm{H}>0$ and $\mathrm{H}<1.5 \mathrm{~h}$

$$
\begin{equation*}
Q=\left[C_{d} B H^{1.5}+C_{t} \tan \theta H^{2.5}\right]\left(1-\left(\frac{h}{H}\right)^{1.5}\right)^{0.385} \tag{6}
\end{equation*}
$$

### 3.2.3 Overtopped weir flow

Under extreme conditions, the flow may overtop the banks of the trapezoidal section and still be within the limits of the approach channel. When such a condition occurs, the flow may be treated in two sections, namely flow within the weir section and that over the limits of the weir section. Three scenarios are identified below.

Scenario 1: When the headwater is above the bank level, ( $\mathrm{H}>\mathrm{ND}$ ) and the tailwater is at or below the bank level, Eq. (7) can be used to estimate flow.

Criterion: $\quad(\mathrm{ND} \geq \mathrm{h}>0)$

$$
\begin{equation*}
\mathrm{Q}=\mathrm{C}_{\mathrm{d}}\left[(\mathrm{~T}-\mathrm{ND} \tan \theta)(\mathrm{ND}) \mathrm{H}^{0.5}\left(1-\left(\frac{\mathrm{h}}{\mathrm{H}}\right)^{1.5}\right)^{0.385}+\mathrm{CW}(\mathrm{H}-\mathrm{ND})^{1.5}\right] \tag{7}
\end{equation*}
$$

Scenario 2: If both the tailwater and headwater are above the bank level, Eq. (8) can be used to estimate flow.

Criterion: $\quad(\mathrm{H}>\mathrm{ND}$ and $\mathrm{h}>\mathrm{ND})$
$\mathrm{Q}=\mathrm{C}_{\mathrm{d}}\left[(\mathrm{T}-\mathrm{ND} \tan \theta)(\mathrm{ND}) \mathrm{H}^{0.5}\left(1-\left(\frac{\mathrm{h}}{\mathrm{H}}\right)^{1.5}\right)^{0.385}+\mathrm{CW}(\mathrm{H}-\mathrm{ND})^{1.5}\left(1-\left(\frac{\mathrm{h}-\mathrm{ND}}{\mathrm{H}-\mathrm{ND}}\right)^{1.5}\right)^{0.385}\right](8)$

Scenario 3: Though it is a scenario that one would not expect, under normal circumstances, the headwater being above the banks, $\mathrm{H}>\mathrm{ND}$, while the tailwater is at or below the weir crest ( $\mathrm{h} \leq 0$ ), it is a condition worth considering. Under such conditions, Eq. (9) may be used to estimate flow.

Criterion: $\quad \mathrm{H}>\mathrm{ND}$ and $\mathrm{h} \leq 0$

$$
\begin{equation*}
\mathrm{Q}=\mathrm{C}_{\mathrm{d}}\left[(\mathrm{~T}-\mathrm{ND} \tan \theta)(\mathrm{ND}) \mathrm{H}^{0.5}+\mathrm{CW}(\mathrm{H}-\mathrm{ND})^{1.5}\right. \tag{9}
\end{equation*}
$$

### 3.2.4 Zero flow

When the headwater and tailwater stages are below the weir crest level the flow is zero (neglecting seepage and leakage):

$$
\text { If } \mathrm{H} \leq 0 \text { and } \mathrm{h} \leq 0, \mathrm{Q}=0 \text {. }
$$

### 3.2.5 Reverse flow

If the tailwater stage is above the weir crest, the condition may indicate flow reversal (negative flow).

$$
\text { If } \mathrm{h}>\mathrm{H}, \mathrm{~h} \text { and } \mathrm{H} \text { switch, and } \mathrm{Q}=-1^{*} \mathrm{Q}
$$

If reverse flow occurs, it would be under a submerged condition. The accuracy of discharge estimation under a submerged reverse condition is lower than under the other conditions. The submerged flow estimation method in itself is of lower accuracy. Besides, parameters developed for estimating positive flow are used to estimate negative flow changing only the sign from positive to negative. Although this approach introduces more errors, it is the readily available method other than conducting research that will require time and money. The recommendation for the future is to conduct the necessary research to develop appropriate parameters for estimating reverse flows.

### 4.0 CULVERT FLOW EQUATIONS

The type of flow that occurs in a culvert depends on headwater and tailwater elevations, culvert invert elevations in relation to water stages, culvert length and slope. Either the inlet or the outlet can control the flow through a culvert. If the discharge as dictated by the inlet configuration and the stage is not affected by what the outlet can accommodate, the inlet is said to control the flow. A typical condition for inlet control is when critical depth is attained at the inlet, subcritical flow prevails upstream and supercritical downstream. Outlet control of flow is either when a controlling subcritical downstream water depth prevails or flow attains critical depth at the downstream invert.

The flow through a culvert depends on the location of the control. The control location influences the flow type and the hydraulic profile. Different equations are used to estimate discharge for different flow types. For classification of types of flow through culverts, readers may refer to Chow (1959), Henderson (1966) or other textbooks in hydraulics.

### 4.1 Critical Flow in Culverts

In most cases the occurrence of critical flow (flow with minimum specific energy and corresponding critical depth) determines the location of the control. Critical flow can occur at the inlet (inlet control) or at the outlet (outlet control) of the culvert. When the flow is subcritical (depth higher than critical) throughout including outlet, the flow is outlet-controlled (tailwater).


Figure 4. Key parameters used in calculating culvert flow
The occurrence of critical flow is characterized by the condition that for the given flow, the specific energy is the minimum. The specific energy (in terms of head) is given by Eq. (10),

$$
\begin{equation*}
\mathrm{H}=\mathrm{h}+\frac{\mathrm{Q}^{2}}{2 \mathrm{gA}^{2}} \tag{10}
\end{equation*}
$$

where g is acceleration of gravity, Q is discharge, H is the specific energy and h is the flow depth.
For minimum specific energy, the first derivative of Eq. (10) is set to zero: $\mathrm{dH} / \mathrm{dh}=0$. This results in Eq. (11), a condition that needs to be satisfied for critical depth in any flow cross section.

$$
\begin{equation*}
\frac{\mathrm{Q}^{2}}{\mathrm{~g}}=\frac{\mathrm{A}^{3}}{\mathrm{~T}} \tag{11}
\end{equation*}
$$

Applying Eq. (11) to different channel sections results in correspondingly different critical depth $\left(h_{\mathrm{c}}\right)$ values in relation to discharge Q .
(a) Trapezoidal and Rectangular Sections

For critical flow computation, geometric parameters may be defined as follows,

$$
\begin{aligned}
& \mathrm{y}=\mathrm{h}_{\mathrm{c}} / \mathrm{b} \\
& \mathrm{~m}= \\
& \mathrm{e} / \mathrm{h}
\end{aligned}
$$

where $h_{c}$ is critical depth and the other parameters are as shown in Fig. 5.
Using these parameters, critical flow can be estimated using Eq. (12).

$$
\begin{equation*}
Q=\frac{(1 / y+m)^{1.5}}{(1 / y+2 m)^{0.5}} g^{0.5} h_{c}^{2.5} \tag{12}
\end{equation*}
$$



Figure 5. Trapezoidal/Rectangular Culvert Section

A rectangular section can be taken as a special case of a trapezoidal one where the banks are vertical, i.e. $m$ $=0$, and thus the expression for discharge at critical depth reduces to Eq. (13).

$$
\begin{equation*}
Q=b \sqrt{g} h_{c}{ }^{1.5} \tag{13}
\end{equation*}
$$

For a triangular channel, the equation for critical flow is described by Eq. (14).

$$
\begin{equation*}
\mathrm{Q}=\sqrt{\frac{\mathrm{g}}{2}} \mathrm{~m}_{\mathrm{h}_{\mathrm{c}}}^{5 / 2} \tag{14}
\end{equation*}
$$

(b) Circular Sections


Figure 6. Circular Culvert Section

For the circular section indicated in Fig. 6, where A is the flow cross section, Equations
(15), (16) and (17) apply.

$$
\begin{align*}
& \mathrm{A}=\frac{\mathrm{D}^{2}}{4}\left(\theta_{\mathrm{r}}-1 / 2 \sin 2 \theta\right)  \tag{15}\\
& \mathrm{T}=\mathrm{D} \sin \theta  \tag{16}\\
& \mathrm{~h}=\frac{\mathrm{D}}{2}(1-\cos \theta) \tag{17}
\end{align*}
$$

The critical flow (at critical depth $h_{c}$ ) in a circular section can be obtained using Eq. (18).

$$
\begin{equation*}
\mathrm{Q}=4.01 \frac{\left(\theta_{\mathrm{r}}-1 / 2 \sin 2 \theta\right)^{1.5}}{(\sin \theta)^{0.5}(1-\cos \theta)^{2.5}} \mathrm{~h}_{\mathrm{c}}^{2.5} \tag{18}
\end{equation*}
$$

In Eq. (18), $\theta_{\mathrm{r}}$ is the angle in radians defined by $\cos \theta=1-(2 h / D)$ per Eq. (17).
For any flow, there is a critical slope that corresponds to the critical depth. Equation (19) can determine the

$$
\begin{equation*}
S_{c}=\frac{14.56 n^{2} D_{m}}{r^{4 / 3}} \tag{19}
\end{equation*}
$$

critical slope corresponding to the flow calculated using Eq. (18).
In Eq. (19) $D_{m}$ is mean depth, which is the ratio of flow area to top width of the flow section, $(\mathrm{b}+\mathrm{e}) \mathrm{h} /(\mathrm{b}+2 \mathrm{eh})$. The ratio of the flow area to the wetted perimeter is the hydraulic radius (r).

The value of $\mathrm{S}_{\mathrm{c}}$ from Eq. (19) has to be compared against the slope of the culvert invert $\mathrm{S}_{\mathrm{o}}$. If $\mathrm{S}_{\mathrm{c}}$ is greater than $S_{0}$, then the flow is subcritical and the control is the culvert outlet. If $S_{c}$ is equal to $S_{o}$, the flow is critical inside the culvert, and the control may be either the weir (rim of flashboard) or the culvert inlet.

### 5.0 FLOW EQUATIONS FOR GATED CULVERTS WITH WEIRS

There are several flow conditions and corresponding equations for estimating flow through culvert and weir combination structures. The culvert and weir combination flow conditions most likely to prevail at the STA-6 outflow structures are considered in this section.


Figure 7. Culvert flow profiles

In Fig. 7, $\mathrm{A}, \mathrm{B}, \mathrm{C}, \mathrm{E}$ and F are water levels, $\mathrm{D}=$ culvert diameter, $\mathrm{G}=$ gate opening,
$h_{1}=$ upstream water depth above culvert invert, $h_{c}=$ critical flow depth inside the culvert, $h_{3}=$ water depth at the downstream end of the culvert, and $h_{4}=$ tailwater depth downstream of the culvert. $Z$ denotes the drop in culvert invert between upstream and downstream ends. The culvert slope is $S_{0}$ and its length is $L$.

### 5.1 Full culvert flow

Flow through a culvert can either be under pressure (full culvert flow) or with a free surface (partial culvert flow). This is the flow type when the culvert is submerged at both the inlet and the outlet, i.e. headwater stage at A and tailwater stage at B (Fig. 7). The following criteria define the flow type.
$\left(h_{1}-z\right) / G>1$, i.e. the gate opening is smaller than the headwater depth above the invert. $\left(h_{1}-z\right)>h_{4}>D$, i.e. the tailwater depth above the downstream invert is greater than the diameter of the culvert.

When these conditions are met the culvert flows full. For full culvert flow condition, the discharge can be estimated using Eq. (20), according to Damisse et al. (1997).

$$
\begin{equation*}
Q=C_{d} A_{0} \sqrt{\frac{2 g\left(h_{1}-h_{4}\right)}{K_{e}\left(\frac{A_{0}}{A_{g}}\right)^{2}+\left(1+\frac{29 n^{2} L}{r^{4 / 3}}\right)}} \tag{20}
\end{equation*}
$$

The following default values may be adopted for subsequent verification and adjustment, as necessary, on the basis of field discharge measurements.

| $\mathrm{C}_{\mathrm{d}}$ | $=$ | 1 |
| :--- | :--- | :--- |
| n | $=$ | 0.022 for corrugated metal pipe of fair condition. |
| $\mathrm{K}_{\mathrm{e}}$ | $=$ | 0.5 for a pipe with a square-cut end |

The value of $\mathrm{A}_{\mathrm{g}}$ is determined using Eq. (15) with the value of $\theta$ determined from Eq. (21).
$\cos ^{-1} \theta=1-\frac{2 G}{D}$
Equation (21) is obtained by rearranging Eq. (17) replacing h with G.

### 5.2 Culvert partially submerged

Sometimes the culvert may be submerged at the upstream end while it is free downstream. This flow condition corresponds to headwater level at A , and tailwater level at C in Fig. 7. It is not a typical flow condition in lowland areas, where slopes are usually mild. It may occur in situations where invert slopes are significant and where the flow is controlled by the inlet capacity. This is flow under high head (Damisse et al. 1997) with the headwater stage at A and tailwater stage at C (Fig. 7). The following criteria are used to establish this flow type.
$\left(h_{1}-Z\right) / G>1.5$, i.e. the ratio of the headwater depth above the culvert to the gate opening is greater than 1.5 .
$h_{4} \leq D$, i.e. the tailwater depth above the invert is less than or equal to the culvert diameter.

$$
\begin{equation*}
Q=C_{d} A_{o} \sqrt{\frac{2 g(h-x D)}{K_{e}\left(\frac{A_{o}}{A_{g}}\right)^{2}+\left(1+\frac{29 n^{2} L}{r^{\frac{4}{3}}}\right)}} \tag{22}
\end{equation*}
$$

Under these conditions flow is estimated using Eq. (22).
In Eq. (22), x is a coefficient for the distance to the center of pressure from the outlet invert as a function of culvert diameter, and it varies from 0.5 to 1.0 (the default value is 0.75 ).

### 5.3 Subcritical free surface flow throughout the culvert

In most cases culverts on mild slopes carry flows with a free water surface, with no submergence at the upstream or downstream end. This condition corresponds to the headwater level at E , and the tailwater level at F . The criteria for this type of flow are the following.

$$
\left(h_{1}-Z\right) / G<1.5 \text { or } \quad\left(h_{1}-Z\right) / D<1.5 \text {, i.e. the headwater level }
$$

above the invert is less than 1.5 times the lesser of culvert diameter or the gate opening.

| $\mathrm{h}_{4} / \mathrm{h}_{\mathrm{c}}$ | $>$ |
| :--- | :--- |
| $\mathrm{h}_{4}$ |  |
| $\mathrm{~S}_{\mathrm{o}}$ |  |
| the flow. |  |

corresponding to the flow.
This flow type is under outlet control. At the terminal section of the culvert, the tailwater stage is above that corresponding to the critical depth. For this condition Eq. (23) is used to estimate flow, according to Damisse et al. (1997),

$$
\begin{equation*}
\mathrm{Q}=\mathrm{C}_{\mathrm{d}} \mathrm{~A}_{3} \sqrt{\frac{2 \mathrm{~g}\left(\mathrm{~h}_{1}-\mathrm{h}_{4}\right)}{1+\frac{2 \mathrm{gA}_{3}^{2} \mathrm{~L}}{\mathrm{~K}_{1} \mathrm{~K}_{3}}}} \tag{23}
\end{equation*}
$$

where $\mathrm{K}_{\mathrm{i}}$ stands for conveyance, defined as follows, in Eq. (24).

$$
\begin{equation*}
\mathrm{K}_{\mathrm{i}}=\frac{1.486}{\mathrm{n}} \mathrm{r}_{\mathrm{i}}^{2 / 3} \mathrm{~A}_{\mathrm{i}} \tag{24}
\end{equation*}
$$

The corresponding hydraulic radius ( $\mathrm{r}_{\mathrm{i}}$ ) for a free surface flow in a circular culvert at any section can be computed using Eq. (25).

$$
\begin{align*}
& r=\frac{D}{4}\left(1-\frac{\sin 2 \theta}{2 \theta}\right)  \tag{25}\\
&  \tag{26}\\
& \theta=\cos ^{-1}\left(1-\frac{2 h}{D}\right)
\end{align*}
$$

Rearranging Eq. (17) to determine the angle gives Eq. (26).

### 6.0 COMPUTATION OF INFLOW THROUGH WEIRS G601 AND G602

Inflow into Cell 5 of STA-6 takes place through two trapezoidal broad-crested weirs. The crest of each weir is at elevation 14 ft NGVD and is 11 ft wide. The trapezoid sides slope at 10:1 (horizontal: vertical). The equations and criteria to be used to determine inflow into Cell 5 of STA- 6 corresponding to the various headwater and tailwater combinations are given in this section. All elevations are in feet. In the following equations the notations are $\mathrm{H}=$ headwater depth, $\mathrm{h}=$ tailwater depth, $\mathrm{HWE}=$ headwater elevation, TWE $=$ tailwater elevation, $\mathrm{WCE}=$ weir crest elevation, $\mathrm{B}_{\mathrm{H}}=$ water surface width where depth above crest is $\mathrm{H}, \mathrm{B}$ $=$ weir crest length, $\mathrm{m}=$ trapezoidal weir side slopes and $\mathrm{ND}=$ notch depth.

$$
\begin{align*}
\mathrm{H} & =  \tag{27}\\
\mathrm{h} & \\
& =\mathrm{HWE}-\mathrm{WCE}  \tag{29}\\
\mathrm{~B}_{\mathrm{H}} & =\mathrm{B}+\mathrm{mH}-\mathrm{WCE}
\end{align*}
$$

The relevant dimensions of each weir are: $\quad \mathrm{ND}=2.5, \mathrm{~B}=11^{\prime}, \mathrm{m}=6$.

1. If $\mathrm{H} \leq 0, \mathrm{Q}=0$
2. If $\mathrm{ND} \geq \mathrm{H} \geq \mathrm{h}$ and $\mathrm{H}>0$

Equation (1) is used to determine $B_{e},\left(B_{e}=14-0.1 * 2 * H\right)$. Equation (6) is used to determine $Q$, with $C_{w}=$ 3.1 (default) until it is calibrated with stream flow data.
3. If $\mathrm{ND} \geq \mathrm{H}>\mathrm{h}>0$ and $\mathrm{H} \leq 1.5 \mathrm{~h}$

Equation (3) estimates submergence coefficient $\mathrm{C}_{\mathrm{s} .}$. Equation (5) is suitable to determine Q .
4. If $\mathrm{H}>\mathrm{ND}>0 \geq \mathrm{h}$

Equation (9) is suitable to determine Q.
5. If $\mathrm{H} \geq \mathrm{ND} \geq \mathrm{h}>0$

Equation (7) estimates Q.
6. If $\mathrm{H} \geq \mathrm{h}>\mathrm{ND}$

Equation (8) is suitable to determine Q .

### 7.0 COMPUTATION OF INFLOW THROUGH WEIR G603

Inflow into Cell 3 of STA- 6 is through a trapezoidal broad-crested weir. As per the "as-built" drawing, the crest of Weir 3 is at elevation 14.2 ft NGVD and 14 ft wide. The trapezoid sides slope at 10:1 (horizontal:vertical). The equations and criteria to be used to determine inflow into Cell 3 of STA-6 corresponding to the various headwater and tailwater combinations are given in this section.

$$
\begin{align*}
\mathrm{H} & =\mathrm{HWE}-\mathrm{WCE}\left(\text { i.e. } 14.2^{\prime}\right)  \tag{30}\\
\mathrm{h} & \left.=\text { TWE }- \text { WCE (i.e. } 14.2^{\prime}\right)  \tag{31}\\
\mathrm{B}_{\mathrm{m}} & =\mathrm{B}+\mathrm{mH}\left(\text { where } \mathrm{B}=14^{\prime}, \mathrm{m}=10\right) \tag{32}
\end{align*}
$$

The relevant dimensions of each weir are: $\quad \mathrm{ND}=3.34, \mathrm{~B}=14, \mathrm{~m}=10$

1. If $\mathrm{H} \leq 0, \mathrm{Q}=0$
2. If $\mathrm{ND} \geq \mathrm{H} \geq 0 \geq \mathrm{h}$

Use Eq. (1) to determine $\mathrm{B}_{\mathrm{e}},\left(\mathrm{B}_{\mathrm{e}}=\mathrm{B}-0.1 * 2 * \mathrm{H}\right)$.
Use Eq. (6) to determine Q , with $\mathrm{C}_{\mathrm{w}}=3.1$ (default) until it is calibrated with streamgauging data.
3. If $\mathrm{ND} \geq \mathrm{H} \geq \mathrm{h}>0$

Equation (3) is used to determine submergence coefficient $\mathrm{C}_{\mathrm{s}}$.
Equation (5) is suitable to determine Q.
4. If $\mathrm{H}>\mathrm{ND}>0 \geq \mathrm{h}$

Equation (9) is suitable to determine Q.
5. If $\mathrm{H}>\mathrm{ND} \geq \mathrm{h}>0$

Equation (7) is suitable to determine $Q$.
6. If $\mathrm{H}>\mathrm{h}>\mathrm{ND}$

Equation (8) is suitable to determine $Q$.

### 8.0 COMPUTATION OF OUTFLOW THROUGH G354 AND G393

The weir-culvert combination structure is provided with a slide gate at the culvert inlet, which will affect the flow. At first, an assumption was made that the slide gate is either fully closed or fully open with no intermediate degree of opening. The conditions of the slide gate would thus be either closed or open. Subsequently, the procedure was revised and a discharge computation algorithm was developed to account for the intermediate levels of gate opening. In this study, the low-level slide gates at the sides of the weir boxes G354A, G354C and G393B, provided to drain the cells if the need arises (an unlikely event), are assumed closed.

The relative elevations of tailwater, headwater, weir crest and culvert crown will determine the flow equation to be used at any time. The criteria and algorithms used to compute flow through a weir-culvert combination structure of STA-6 are described in the following sections.

The rim elevation of the weir box (WCE) at G354 is 14.1 ft and that of G393 is 14.0 ft NGVD. These elevations are the main reference for flow computation at those stations.

1. Stage upstream of weir box, HWE $\leq W C E$ ( 14.1 ft and 14.0 ft NGVD for G354 and G393, respectively) and weir box side gate closed, or slide gate at upstream face of culvert closed $(\mathrm{G}=0)$

In this condition it is assumed that there is no outflow from the treatment cells to the discharge canal. Leakage, if any, is neglected, and flow is estimated to be zero, $\mathrm{Q}=0$.

2 Slide gate open and stage upstream of weir box, HWE $>$ WCE ( 14.1 ft for G354 or 14.0 ft for G393 NGVD as appropriate).

Outflow occurs and discharge is computed using either a weir equation or a culvert equation. There is a condition where either a weir equation or a culvert equation may be acceptable. In such a situation the flow computed using a weir equation is compared to that obtained using a culvert equation, and the lower of the two values is adopted as the better estimate.

Computation Steps

- Determine $\theta$ using Eq. (21) for angle subtended by gate $\left(\theta_{g}\right)$.
- Determine $A_{g}$ from Eq. (15) using $\theta_{g}$.
- Determine $\theta_{3}$ from Eq. (21) using $h_{3}$ in place of $G$ for the angle subtended by the water surface.
- Determine $A_{3}$ corresponding to $\theta_{3}$ from Eq. (15).
- Determine hydraulic radius $r$ corresponding to $h_{3}$ using Eq. (25).
- Compute flow (Q) using Eq. (18), assuming $h_{3}$ corresponds to critical flow depth $\left(\mathrm{h}_{\mathrm{c}}\right)$ at the downstream end of the culvert.
- Use the resulting flow $Q$ to determine the corresponding critical slope $S_{c}$ from Eq. (19).
- Determine culvert invert slope $\mathrm{So}_{\mathrm{o}}=\mathrm{z} / \mathrm{L}$ and compare against the critical $\mathrm{S}_{\mathrm{c}}$.
- Determine friction slope from Eq. (37).
- Determine $\mathrm{h}_{2}$ from Eq. (38).
- Determine $\theta_{2}$ using $h_{2}$ in Eq. (21).
- Use $\theta_{2}$ in Eq. (15) to determine $A_{2}$, which shall be limited to a maximum of the full culvert cross-section area.
- Assume $h_{3}=h_{4}$, tailwater depth above outlet invert determined from Eq. (34).

$$
\begin{equation*}
\mathrm{h}_{1}=\mathrm{HWE}-\text { OUTEL } \tag{33}
\end{equation*}
$$

$$
\mathrm{h}_{3}=\text { TWE }- \text { OUTEL }
$$

$$
\begin{equation*}
\mathrm{z}=\mathrm{OUTEL}-\mathrm{INEL} \tag{34}
\end{equation*}
$$

$$
\begin{equation*}
\mathrm{h}_{\mathrm{w}}=\mathrm{WCE}-\mathrm{OUTEL} \tag{35}
\end{equation*}
$$

$$
\begin{equation*}
S_{f}=\left[\left(c_{w} L H^{1.5} n\right) /\left(1.486 A_{3} R^{0.667}\right)\right]^{2} \tag{37}
\end{equation*}
$$

$\mathrm{h}_{2}=\mathrm{h}_{3}+\mathrm{z}+\mathrm{s}_{\mathrm{f}}{ }^{*} \mathrm{~L}$

$$
\begin{equation*}
\mathrm{A}_{\mathrm{r}}=\mathrm{A}_{\mathrm{g}} / \mathrm{A}_{2} \tag{38}
\end{equation*}
$$

When $G<D$ and $G<\left(h_{2}-z\right)$, the discharge computed must be reduced by the factor $A_{r}$. The value of $A_{r}$ shall be limited to a maximum of 1.0 .

Condition 1: If $h_{1}-z \geq D \geq h_{2}-z$ and $S_{c} \geq S_{o}$, assume flow control at weir box crest.
If $h_{1}-h_{w} \geq 1.5\left(h_{2}-h_{w}\right)$, consider free weir flow and use Eq. (2) default $C_{w}=3.1$;
If $0<h_{1}-h_{w}<1.5\left(h_{2}-h_{w}\right)$, consider submerged weir flow and use Eq. (3) for submergence coefficient with Manning's $\mathrm{n}=0.022$ (default) and determine flow Q using Eq. (4).

Condition 2: If $\left(\mathrm{h}_{2}-\mathrm{z}\right) / \mathrm{D}>1, \mathrm{G} / \mathrm{D} \geq 1,\left(\mathrm{~h}_{2}-\mathrm{z}\right) / \mathrm{G}>1, \mathrm{~h}_{3}>\mathrm{D}$ outlet controlled submerged culvert flow prevails. Compute flow with Eq. (20), using $\mathrm{n}=0.022$ and $\mathrm{C}_{\mathrm{d}}=1$ (defaults). Use Eq. (21) for $\theta$ and Eq. (15) for gate opening area $\mathrm{A}_{\mathrm{g}}$. Slope is not considered as a criterion in this case.

Condition 3: If $\left(h_{2}-z\right) / D \geq 1.5, G / D \geq 1, h_{3} \leq D$, use Eq. (22) to compute flow and default values $\mathrm{m}=0.75, \mathrm{n}=0.022, \mathrm{~K}_{\mathrm{e}}=0.5, \mathrm{C}_{\mathrm{d}}=1$. Slope is not considered as a criterion in this case.

Condition 4: If $h_{2}-Z \geq 1.5 D, G / D \geq 1, h_{4} \geq D,\left(h_{1}-h_{w}\right)<1.5\left(h_{2}-h_{w}\right)$;
Determine $\mathrm{Q}_{1}$ using Eq. (4), $\mathrm{C}_{\mathrm{s}}$ from Eq. (3)
Determine $\mathrm{Q}_{2}$ using Eq. (23), $\mathrm{K}_{2}$ and $\mathrm{K}_{3}$ from Eq. (24), $\mathrm{r}_{2}$ and $\mathrm{r}_{3}$ from Eq. (25), and $\theta$ from Eq. (26).

If $\mathrm{Q}_{1}<\mathrm{Q}_{2}, \mathrm{Q}=\mathrm{Q}_{1}$ else, $\mathrm{Q}=\mathrm{Q}_{2} . \quad\left[\mathrm{Q}=\min \left(\mathrm{Q}_{1}, \mathrm{Q}_{2}\right)\right]$

### 9.0 FLOW ESTIMATION PARAMETERS

The FLOW program is used in conjunction with DBHYDRO (the hydrologic database) and the Archive database to estimate flow through the various control structures in the District. All static information (structure parameters) required for discharge computation is registered in the DBHYDRO database. The dynamic instantaneous data, including headwater stage, tailwater stage and control operation status, are available in the Archive database. The structure information registered in the DBHYDRO database for STA-6 structures is given in Table 1.

Table 1. Structure information for STA6 stations

| station | G600 | G601 | G602 | G603 | G354 | G393 | G605 | G606 | G607 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Type | pump | weir | weir | weir | culvert | culvert | uvm | uvm | culvert |
| Units | 5 | 1 | 1 | 1 | 3 | 3 | 1 | 1 | 6 |
| Dbkey (Source) | G6531 | J5566 | J5567 | J5568 | J0939 | J5569 | GA119 | GA116 | G7750 |
| Dbkey (Preferred) | GG955 |  |  |  | MC958 | MC959 | H3143 | H3144 |  |
| Max Q (Group) | 500 | 180 | 180 | 140 | 360 | 140 | 200 | 600 | 600 |
| Min. Q (Group) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -130 | -200 |
| Design Q (Group) | 500 | 180 | 180 | 140 | 360 | 140 | 200 | 650 | 500 |
| $\begin{gathered} \text { Maximum } \\ \text { HW(ft) } \\ \hline \end{gathered}$ | $\begin{aligned} & 10.2 \mathrm{on} \\ & 8.7 \mathrm{off} \end{aligned}$ | 16.34 | 16.34 | 16.09 | 17.6 | 17.6 | 16.4 | 16.4 | 16.4 |
| $\begin{gathered} \text { Maximum TW } \\ (\mathrm{ft}) \end{gathered}$ |  | 15.45 | 15.45 | 15.45 | 16.4 | 16.4 | 16.4 | 16.4 | N/A. |
| Bypass Stage (ft) |  | 20.50 | 20.50 | 20.5 | 19.5 | 19.5 | 20.5 | 19.5 | 19.0 |
| Section <br> Minimum <br> Elevation |  | 14.1 | 14.1 | 14.2 | 14.1 | 14.0 | 0 | 0 | 4.29 |
| Section <br> Length(ft) | N/A. | N/A | N/A | N/A | 75 | 75 | N/A | N/A | 70 |
| Section <br> Width(ft) | $\begin{gathered} \hline 4 \\ \text { Dia. } \end{gathered}$ | 11 <br> bottom | 11 bottom | 14 bottom | 7 | 7 |  | 34 | $\begin{aligned} & 4 \text { of } 5.5^{\prime} \\ & 2 \text { of } 7.0^{\prime} \end{aligned}$ |
| Section <br> Depth(tt) | $\begin{gathered} \hline 4 \\ \text { Dia. } \end{gathered}$ | $\begin{gathered} 2.4 \\ \text { notch } \end{gathered}$ | $\begin{gathered} 2.3 \\ \text { notch } \end{gathered}$ | $\begin{gathered} 3.3 \\ \text { notch } \end{gathered}$ | 7 | 7 |  | 13 | $\begin{aligned} & 4 \text { of } 5.5^{\prime} \\ & 2 \text { of } 7.0^{\prime} \end{aligned}$ |
| RPM | 150 | N/A | N/A | N/A | N/A | N/A | N/A | N/A | N/A |

[^0]Table 2 presents the discharge coefficients for the different flow conditions of each flow control structure. Four discharge coefficients are provided for discharge estimation through the pump station G600. For each weir (G601, G602 and G603), four flow conditions are considered. Correspondingly, four discharge coefficients are given. Inlet loss coefficient $\left(\mathrm{K}_{\mathrm{e}}\right)$ and Manning's coefficient ( n ) values are also given for the culverts G354 and G393.

Table 2. Discharge Coefficients for STA-6 Stations

| station | G600 | G601 | G602 | G603 | G354 | G393 | G607 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Type | Pump | Weir | Weir | weir | culvert | culvert | culvert |
| Units | 5 | 1 | 1 | 1 | 3 | 3 | 6 |
| Dbkey (Source) | G6531 | J5566 | J5567 | J5568 | J0939 | J5569 | G7750 |
| Dbkey <br> (Preferred) | GG955 |  |  |  | MC958 | MC959 |  |
| N | 1800 |  |  |  |  |  |  |
| COEF11 (A) | -1.1 |  |  |  |  |  |  |
| COEF12 (B) | 36000 |  |  |  |  |  |  |
| COEF13 (C) | 19 |  |  |  | 3.3 | 3.3 | 3.3 |
| WEIR COEF. <br> (Cw) |  | 3.1 | 3.1 |  |  | 0.5 | 0.5 |
| INLET_K |  |  |  |  | 0.022 | 0.022 | 0.022 |
| Manning's n |  |  |  |  |  |  |  |

STA-6 flow-monitoring sites and stage-monitoring stations are listed in Table 3. Table 3 indicates the flow combinations, site identifiers (site i.d.s) and start dates of the monitoring stations. Station source and preferred flow dbkeys (database keys or alphanumeric identifiers) are also given in this table. Initially the outflow stations were established in such a way that G354 was treated as one flow station with three culvert barrels, as was G393. One reason for handling G354 and G393 as one flow station with three controls was that all structure parameters used for all of them were similar and the same pair of headwater and tailwater stages was used. In addition, all three culverts delivered water from the same cell to the same discharge canal with identical inlet and outlet conditions. Thus it was deemed logical to establish one flow station with three controls in the interest of reducing data- processing costs. Later, it was decided to treat each culvert as a separate flow station because of the distance between adjacent culverts.

Table 3. STA6 Flow Monitoring Sites and Stage Stations

| Site | Station Flow Combination | Site ID | Start Date | Source dbkey | Preferred dbkey |
| :---: | :---: | :---: | :---: | :---: | :---: |
| G600 | G600 P | 62647341 | 29-OCT-1997 | G6531 | GG955 |
|  | G600+H |  | 31-OCT-1997 | G6528 |  |
|  | G600+T |  | 29-OCT-1997 | G6529 |  |
|  | G600+P1 |  | 29-OCT-1997 |  |  |
|  | G600+P2 |  | 29-OCT-1997 |  |  |
|  | G600+P4 |  | 29-OCT-1997 |  |  |
|  | G600+P5 |  | 29-OCT-1997 |  |  |
| G601 | G601 | 63547341 | 30-NOV-1998 | J5566 |  |
|  | G352S+H |  | 17-DEC-1997 |  |  |
|  | G352S+T |  | 17-DEC-1997 |  |  |
| G602 | G602 | 63547342 | 30-NOV-1998 | J5567 |  |
|  | G352S+H |  | 17-DEC-1997 |  |  |
|  | G352S+T |  | 17-DEC-1997 |  |  |
| G603 | G603 | 63647341 | 30-NOV-1998 | J5568 |  |
|  | G392S+H |  | 17-DEC-1997 |  |  |
|  | G392S+T |  | 17-DEC-1997 |  |  |
| G605 | G605+Q |  | 24-NOV-1997 | GA119 | H3143 |
|  | G605+ (stage) |  | 24-NOV-1997 | GA118 |  |
| G606 | G606+Q |  | 24-NOV-1997 | GA116 | H3144 |
|  | G606+(stage) |  | 24-NOV-1997 | GA115 |  |
| G354 | G354 C | 63147352 | 12-DEC-1997 | J0939 | MC958 |
|  | G354C+H |  | 12-DEC-1997 |  |  |
|  | G354C+T |  | 12-DEC-1997 |  |  |
|  | G354A@1 |  | 01-DEC-1997 |  |  |
|  | G354B@1 |  | 01-DEC-1997 |  |  |
|  | G354C@1 |  | 01-DEC-1997 |  |  |
| G393 | G393 C | 60148343 | 12-DEC-1997 | J5569 | MC959 |
|  | G393+H |  | 12-DEC-1997 |  |  |
|  | G393+T |  | 12-DEC-1997 |  |  |
|  | G393A@1 |  | 01-DEC-1997 |  |  |
|  | G393B@1 |  | 01-DEC-1997 |  |  |
|  | G393C@1 |  | 01-DEC-1997 |  |  |
| G354+G393 |  |  | 01-DEC-1997 | JI252 |  |
| STA6OUT | STA6OUT |  |  |  | HD889 |
| G607 | G607 C | 60148341 | 13-MAY-1997 | G7750 |  |
|  | G607+H |  | 13-MAY-1997 |  |  |
|  | G607+T |  | 13-MAY-1997 |  |  |
|  | G607@(1to6) |  | 13-MAY-1997 |  |  |

### 10.0 EVALUATION OF FLOW ESTIMATES

A period of record (October 1 through 31, 2000) was selected to evaluate the ratings implemented for inflow and outflow structures for STA-6. The Flow program was used to generate instantaneous flows for the selected period. Figure 8 shows instantaneous flows through all inflow and outflow structures of STA6. The cumulative flows for the period are shown in Fig. 9.

STA6 Flows
—G600 pump cfs - G601 weir cfs - G603 weir cfs - G354 culvert cfs - G393 culvert cfs


Figure 8. STA-6 Instantaneous Discharges of October 2000

In general the results were very good as far as flow estimates are concerned. The estimates of cumulative flow for G354 and G393 (the outflow weirs) compared very well with the corresponding

## STA6 Cumulative Flows for 10/2000



Figure 9. STA-6 Cumulative Flows of October 2000
inflows through G600 pumps. The cumulative inflow through the G600 pumps was estimated at 12,700 acft for the period. The estimate of the corresponding combined cumulative outflow through G354 and G393 was $12,300 \mathrm{ac}$-ft, i.e. 97 percent of G 600 inflow. The three-percent difference can be attributed to losses through net evapotranspiration, seepage and estimation errors.

The attenuation and translation effects of the cells (providing storage) can be observed in Fig. 8. The outflow peak is reduced in magnitude and shifted forward in time when compared to the inflows. The outflow discharge curve is smoother and flatter than that of the inflow. The behavior is expected of reservoirs (detention facilities). The pulse-like discharges from G600 are routed through the cells to generate a smoother and flatter receding limb of the outflow hydrograph.

The discharges through the inflow weirs (G601, G602 and G603) show a few negative values, implying flow from the treatment cells back into the supply canal (reverse flow). Under normal operating conditions, backflow from the treatment cells to the inflow canal is not a likely scenario. It is a result of negative head differential, i.e. the headwater being less than the tailwater. The scenario is not consistent with the fact that G604 is closed and thus there is no flow through this bypass structure. There is no backflow through G600, which implies that there is no discharge from the supply canal into the sugarcane farms.

The relation between the headwater and tailwater of a control structure determines the sign of the resulting computed flow. When the headwater is higher than the tailwater, the flow is positive; otherwise it is negative. The instances where the headwater is lower than the tailwater at the inflow weirs of STA- 6 may be due to some errors in the reference elevations. The reference elevations related to G601, G602 and G603 need to be tied to a benchmark. If both tailwater and headwater elevations are tied to the same benchmark, the effect of reference elevation errors will be minimized.

In a few instances the headwater and tailwater stages at the inflow trapezoidal weirs did not appear realistic. In those instances, headwater readings were lower than the tailwater readings, and thus the flow estimates were negative, indicating reverse flow. The stage readings seem to be erroneous. The combined cumulative inflow through the trapezoidal weirs G601, G602 and G603 estimated for the period was 10,900 ac-ft, i.e. 86 percent of the estimated inflow through G600. The 14 -percent difference between $G 600$ estimates and the combined flows of G601, G602 and G603 is partly due to the negative head differentials, which generated negative flows at the three inflow weirs, and partly due to seepage and estimation errors. The negative flows do not seem warranted by the design criteria or the operation plan. The actual operation of those structures did not indicate any possibilities of reverse flow.

Flow pulses shown in Fig. 9 match exactly with stage variations indicated in Fig. 10. This is not unexpected, because discharge is a function of stage. The accuracy of computed flow is dependent upon the accuracy of the stages. Any error in the stage values affects the error in flow exponentially. This is clear from the equations used to determine flow. Flow equations for all conditions are given as power functions of head differential (powers of H greater than 1.0).


Figure 10. Inflow and Outflow Stages of Cell 3

### 11.0 CONCLUSIONS AND RECOMMENDATIONS

Procedures have been developed to monitor inflow and outflow at STA-6 Section 1. The criteria and steps to be followed for computing flows into STA- 6 cells through the inflow weirs have been presented in this report. A method is presented that enables the computation of flow through the weir box and culvert combination structures at G354 and G393 in order to monitor outflows from the respective treatment cells.

The flow conditions most likely to prevail at the inflow and outflow stations have been considered. For most coefficients, default values have been suggested for use in the absence of calibration results. However, streamgauging activities need to be planned and carried out to obtain adequate calibration data from the inflow and outflow stations. Adequate discharge measurements (preferably 30 or more for each station) will facilitate rating analyses to determine appropriate discharge coefficients. Streamgauging activities need to be provided for in such a way as to enable independent discharge measurements for G354 and G393. This may require operating one of these two stations at a time when the measurements are taking place. Discharge measurements need to be made for the inflow stations in such a way as to determine inflows to Cell 5 separately from inflows to Cell 3. This may require simultaneous measurements using two crews.
"As-built" crest elevations of the inflow and outflow weirs have been used in the flow computation equations. For the inflow Weir 3 the "as-built" crest elevation is slightly higher than the design crest elevation ( 14.3 ft NGVD as designed versus 14.2 ft NGVD as built).

The criteria, equations and algorithms developed and presented in this report will significantly improve flow monitoring through STA-6 Section 1. The methodologies presented here can, with slight modifications, be used for flow monitoring at similar stations in new stormwater treatment areas when they come on line.

The equations used for flow computation at STA-6 structures are theoretical, and default values have been adopted for discharge coefficients. There is good correlation between inflows from G600 and outflows through G354 and G393 (correlation coefficient $=0.99$ ). The flows through G601, G602 and G603 are slightly different from G600 inflows, as well as the outflows through G354 and G393. There is some room for improvement of the weir inflow estimates. It is also possible to gain some improvement on the overall accuracy of flow computation at STA- 6 structures. Thus, it is imperative that extensive streamgauging be conducted at STA-6. It is necessary to acquire adequate streamgauging data in order to verify and/or improve accuracy of flow estimates at STA- 6 structures.

Some input data showed unlikely stage relations between the headwater and tailwater stages of G603 (G352S+H and G352S+T). On a few occasions it was observed that the headwater stages were lower than the tailwater stages, resulting in negative flows. This is possibly caused by incompatible reference elevations of headwater and tailwater. It is thus imperative that the reference elevations of those stages be investigated. If the reference elevations of the headwater and the tailwater differ, the correct values must be used to improve the accuracy of the flow estimates.

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## APPENDIX I: STA-6 INFLOW, INTERIOR AND OUTFLOW STAGES FOR OCTOBER 2000

G392S+H = Inflow headwater stage in supply canal (for G601 and G602), G392S+T = Inflow tailwater stage in Cell 3 (for G601 and G602), G393S+H = Outflow headwater stage inside Cell 3 (for G393), G393 $+\mathrm{T}=$ Outflow tailwater stage in discharge canal, G393 CE $=$ Weir crest elevation of G393 (weir-culvert combination structure), Hinflow = Head difference across inflow weirs (G601 and G602), Houtflow = Head difference across outflow (G393)

| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001001 | 0 | 1 | 14.41 | 14.28 | 14.27 | 12.82 | 14 | 0.13 | 0.01 |
| 20001001 | 15 | 1 | 14.4 | 14.28 | 14.26 | 12.82 | 14 | 0.12 | 0.02 |
| 20001001 | 30 | 1 | 14.4 | 14.28 | 14.26 | 12.82 | 14 | 0.12 | 0.02 |
| 20001001 | 45 | 1 | 14.39 | 14.28 | 14.26 | 12.82 | 14 | 0.11 | 0.02 |
| 20001001 | 100 | 1 | 14.39 | 14.28 | 14.26 | 12.82 | 14 | 0.11 | 0.02 |
| 20001001 | 115 | 1 | 14.39 | 14.28 | 14.26 | 12.82 | 14 | 0.11 | 0.02 |
| 20001001 | 130 | 1 | 14.38 | 14.28 | 14.26 | 12.82 | 14 | 0.1 | 0.02 |
| 20001001 | 145 | 1 | 14.38 | 14.28 | 14.26 | 12.82 | 14 | 0.1 | 0.02 |
| 20001001 | 200 | 1 | 14.38 | 14.27 | 14.26 | 12.82 | 14 | 0.11 | 0.01 |
| 20001001 | 215 | 1 | 14.37 | 14.27 | 14.26 | 12.82 | 14 | 0.1 | 0.01 |
| 20001001 | 230 | 1 | 14.37 | 14.27 | 14.25 | 12.82 | 14 | 0.1 | 0.02 |
| 20001001 | 245 | 1 | 14.37 | 14.27 | 14.25 | 12.82 | 14 | 0.1 | 0.02 |
| 20001001 | 300 | 1 | 14.37 | 14.27 | 14.25 | 12.82 | 14 | 0.1 | 0.02 |
| 20001001 | 315 | 1 | 14.36 | 14.27 | 14.25 | 12.82 | 14 | 0.09 | 0.02 |
| 20001001 | 330 | 1 | 14.36 | 14.27 | 14.25 | 12.82 | 14 | 0.09 | 0.02 |
| 20001001 | 345 | 1 | 14.36 | 14.26 | 14.25 | 12.82 | 14 | 0.1 | 0.01 |
| 20001001 | 400 | 1 | 14.35 | 14.26 | 14.25 | 12.82 | 14 | 0.09 | 0.01 |
| 20001001 | 415 | 1 | 14.35 | 14.26 | 14.25 | 12.82 | 14 | 0.09 | 0.01 |
| 20001001 | 430 | 1 | 14.35 | 14.26 | 14.25 | 12.82 | 14 | 0.09 | 0.01 |
| 20001001 | 445 | 1 | 14.34 | 14.26 | 14.24 | 12.82 | 14 | 0.08 | 0.02 |
| 20001001 | 500 | 1 | 14.34 | 14.26 | 14.24 | 12.82 | 14 | 0.08 | 0.02 |
| 20001001 | 515 | 1 | 14.34 | 14.26 | 14.24 | 12.82 | 14 | 0.08 | 0.02 |
| 20001001 | 530 | 1 | 14.34 | 14.26 | 14.24 | 12.82 | 14 | 0.08 | 0.02 |
| 20001001 | 545 | 1 | 14.33 | 14.26 | 14.24 | 12.82 | 14 | 0.07 | 0.02 |
| 20001001 | 600 | 1 | 14.33 | 14.25 | 14.24 | 12.82 | 14 | 0.08 | 0.01 |
| 20001001 | 615 | 1 | 14.33 | 14.25 | 14.24 | 12.82 | 14 | 0.08 | 0.01 |
| 20001001 | 630 | 1 | 14.32 | 14.25 | 14.24 | 12.82 | 14 | 0.07 | 0.01 |
| 20001001 | 645 | 1 | 14.32 | 14.25 | 14.24 | 12.82 | 14 | 0.07 | 0.01 |
| 20001001 | 700 | 1 | 14.32 | 14.25 | 14.23 | 12.82 | 14 | 0.07 | 0.02 |
| 20001001 | 715 | 1 | 14.32 | 14.25 | 14.23 | 12.82 | 14 | 0.07 | 0.02 |
| 20001001 | 730 | 1 | 14.31 | 14.25 | 14.23 | 12.82 | 14 | 0.06 | 0.02 |
| 20001001 | 745 | 1 | 14.31 | 14.25 | 14.23 | 12.82 | 14 | 0.06 | 0.02 |
| 20001001 | 800 | 1 | 14.31 | 14.24 | 14.23 | 12.81 | 14 | 0.07 | 0.01 |
| 20001001 | 815 | 1 | 14.48 | 14.24 | 14.23 | 12.81 | 14 | 0.24 | 0.01 |
| 20001001 | 830 | 1 | 14.63 | 14.25 | 14.23 | 12.82 | 14 | 0.38 | 0.02 |
| 20001001 | 845 | 1 | 14.74 | 14.26 | 14.23 | 12.81 | 14 | 0.48 | 0.03 |
| 20001001 | 900 | 1 | 14.83 | 14.27 | 14.23 | 12.81 | 14 | 0.56 | 0.04 |
| 20001001 | 915 | 1 | 14.89 | 14.29 | 14.23 | 12.81 | 14 | 0.6 | 0.06 |
| 20001001 | 930 | 1 | 14.95 | 14.31 | 14.22 | 12.81 | 14 | 0.64 | 0.09 |
| 20001001 | 945 | 1 | 15.02 | 14.34 | 14.22 | 12.81 | 14 | 0.68 | 0.12 |
| 20001001 | 1000 | 1 | 15.07 | 14.36 | 14.22 | 12.81 | 14 | 0.71 | 0.14 |
| 20001001 | 1015 | 1 | 15.12 | 14.39 | 14.22 | 12.81 | 14 | 0.73 | 0.17 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001001 | 1030 | 1 | 15.16 | 14.41 | 14.22 | 12.81 | 14 | 0.75 | 0.19 |
| 20001001 | 1045 | 1 | 15.21 | 14.44 | 14.22 | 12.81 | 14 | 0.77 | 0.22 |
| 20001001 | 1100 | 1 | 15.25 | 14.46 | 14.22 | 12.81 | 14 | 0.79 | 0.24 |
| 20001001 | 1115 | 1 | 15.28 | 14.48 | 14.22 | 12.81 | 14 | 0.8 | 0.26 |
| 20001001 | 1130 | 1 | 15.31 | 14.5 | 14.22 | 12.8 | 14 | 0.81 | 0.28 |
| 20001001 | 1145 | 1 | 15.34 | 14.52 | 14.22 | 12.8 | 14 | 0.82 | 0.3 |
| 20001001 | 1200 | 1 | 15.37 | 14.53 | 14.22 | 12.8 | 14 | 0.84 | 0.31 |
| 20001001 | 1215 | 1 | 15.39 | 14.55 | 14.22 | 12.8 | 14 | 0.84 | 0.33 |
| 20001001 | 1230 | 1 | 15.41 | 14.56 | 14.22 | 12.8 | 14 | 0.85 | 0.34 |
| 20001001 | 1245 | 1 | 15.43 | 14.57 | 14.22 | 12.8 | 14 | 0.86 | 0.35 |
| 20001001 | 1300 | 1 | 15.44 | 14.59 | 14.23 | 12.8 | 14 | 0.85 | 0.36 |
| 20001001 | 1315 | 1 | 15.45 | 14.6 | 14.23 | 12.8 | 14 | 0.85 | 0.37 |
| 20001001 | 1330 | 1 | 15.46 | 14.61 | 14.23 | 12.79 | 14 | 0.85 | 0.38 |
| 20001001 | 1345 | 1 | 15.47 | 14.61 | 14.23 | 12.79 | 14 | 0.86 | 0.38 |
| 20001001 | 1400 | 1 | 15.46 | 14.62 | 14.23 | 12.79 | 14 | 0.84 | 0.39 |
| 20001001 | 1415 | 1 | 15.38 | 14.58 | 14.24 | 12.79 | 14 | 0.8 | 0.34 |
| 20001001 | 1430 | 1 | 15.3 | 14.55 | 14.24 | 12.79 | 14 | 0.75 | 0.31 |
| 20001001 | 1445 | 1 | 15.23 | 14.52 | 14.24 | 12.79 | 14 | 0.71 | 0.28 |
| 20001001 | 1500 | 1 | 15.18 | 14.5 | 14.24 | 12.79 | 14 | 0.68 | 0.26 |
| 20001001 | 1515 | 1 | 15.14 | 14.48 | 14.25 | 12.79 | 14 | 0.66 | 0.23 |
| 20001001 | 1530 | 1 | 15.09 | 14.46 | 14.25 | 12.79 | 14 | 0.63 | 0.21 |
| 20001001 | 1545 | 1 | 15.06 | 14.44 | 14.25 | 12.79 | 14 | 0.62 | 0.19 |
| 20001001 | 1600 | 1 | 15.02 | 14.42 | 14.25 | 12.79 | 14 | 0.6 | 0.17 |
| 20001001 | 1615 | 1 | 14.99 | 14.41 | 14.26 | 12.78 | 14 | 0.58 | 0.15 |
| 20001001 | 1630 | 1 | 14.96 | 14.39 | 14.26 | 12.78 | 14 | 0.57 | 0.13 |
| 20001001 | 1645 | 1 | 14.93 | 14.38 | 14.26 | 12.78 | 14 | 0.55 | 0.12 |
| 20001001 | 1700 | 1 | 14.9 | 14.37 | 14.26 | 12.78 | 14 | 0.53 | 0.11 |
| 20001001 | 1715 | 1 | 14.88 | 14.36 | 14.26 | 12.78 | 14 | 0.52 | 0.1 |
| 20001001 | 1730 | 1 | 14.85 | 14.35 | 14.27 | 12.78 | 14 | 0.5 | 0.08 |
| 20001001 | 1745 | 1 | 14.83 | 14.35 | 14.27 | 12.78 | 14 | 0.48 | 0.08 |
| 20001001 | 1800 | 1 | 14.81 | 14.34 | 14.27 | 12.78 | 14 | 0.47 | 0.07 |
| 20001001 | 1815 | 1 | 14.79 | 14.33 | 14.27 | 12.78 | 14 | 0.46 | 0.06 |
| 20001001 | 1830 | 1 | 14.78 | 14.33 | 14.27 | 12.78 | 14 | 0.45 | 0.06 |
| 20001001 | 1845 | 1 | 14.76 | 14.32 | 14.27 | 12.78 | 14 | 0.44 | 0.05 |
| 20001001 | 1900 | 1 | 14.74 | 14.32 | 14.27 | 12.78 | 14 | 0.42 | 0.05 |
| 20001001 | 1915 | 1 | 14.73 | 14.32 | 14.27 | 12.78 | 14 | 0.41 | 0.05 |
| 20001001 | 1930 | 1 | 14.71 | 14.31 | 14.27 | 12.78 | 14 | 0.4 | 0.04 |
| 20001001 | 1945 | 1 | 14.7 | 14.31 | 14.27 | 12.78 | 14 | 0.39 | 0.04 |
| 20001001 | 2000 | 1 | 14.68 | 14.31 | 14.27 | 12.78 | 14 | 0.37 | 0.04 |
| 20001001 | 2015 | 1 | 14.67 | 14.3 | 14.27 | 12.78 | 14 | 0.37 | 0.03 |
| 20001001 | 2030 | 1 | 14.66 | 14.3 | 14.27 | 12.78 | 14 | 0.36 | 0.03 |
| 20001001 | 2045 | 1 | 14.65 | 14.3 | 14.27 | 12.78 | 14 | 0.35 | 0.03 |
| 20001001 | 2100 | 1 | 14.64 | 14.3 | 14.27 | 12.77 | 14 | 0.34 | 0.03 |
| 20001001 | 2115 | 1 | 14.63 | 14.3 | 14.27 | 12.78 | 14 | 0.33 | 0.03 |
| 20001001 | 2130 | 1 | 14.62 | 14.29 | 14.27 | 12.78 | 14 | 0.33 | 0.02 |
| 20001001 | 2145 | 1 | 14.61 | 14.29 | 14.27 | 12.78 | 14 | 0.32 | 0.02 |
| 20001001 | 2200 | 1 | 14.6 | 14.29 | 14.27 | 12.78 | 14 | 0.31 | 0.02 |
| 20001001 | 2215 | 1 | 14.59 | 14.29 | 14.26 | 12.78 | 14 | 0.3 | 0.03 |
| 20001001 | 2230 | 1 | 14.58 | 14.29 | 14.26 | 12.78 | 14 | 0.29 | 0.03 |
| 20001001 | 2245 | 1 | 14.57 | 14.28 | 14.26 | 12.77 | 14 | 0.29 | 0.02 |
| 20001001 | 2300 | 1 | 14.57 | 14.28 | 14.26 | 12.77 | 14 | 0.29 | 0.02 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001001 | 2315 | 1 | 14.56 | 14.28 | 14.26 | 12.77 | 14 | 0.28 | 0.02 |
| 20001001 | 2330 | 1 | 14.55 | 14.28 | 14.26 | 12.77 | 14 | 0.27 | 0.02 |
| 20001001 | 2345 | 1 | 14.54 | 14.28 | 14.26 | 12.77 | 14 | 0.26 | 0.02 |
| 20001002 | 0 | 2 | 14.54 | 14.28 | 14.26 | 12.77 | 14 | 0.26 | 0.02 |
| 20001002 | 15 | 2 | 14.53 | 14.28 | 14.26 | 12.77 | 14 | 0.25 | 0.02 |
| 20001002 | 30 | 2 | 14.52 | 14.27 | 14.26 | 12.77 | 14 | 0.25 | 0.01 |
| 20001002 | 45 | 2 | 14.52 | 14.27 | 14.25 | 12.77 | 14 | 0.25 | 0.02 |
| 20001002 | 100 | 2 | 14.51 | 14.27 | 14.25 | 12.77 | 14 | 0.24 | 0.02 |
| 20001002 | 115 | 2 | 14.5 | 14.27 | 14.25 | 12.77 | 14 | 0.23 | 0.02 |
| 20001002 | 130 | 2 | 14.5 | 14.27 | 14.25 | 12.77 | 14 | 0.23 | 0.02 |
| 20001002 | 145 | 2 | 14.49 | 14.27 | 14.25 | 12.77 | 14 | 0.22 | 0.02 |
| 20001002 | 200 | 2 | 14.49 | 14.27 | 14.25 | 12.77 | 14 | 0.22 | 0.02 |
| 20001002 | 215 | 2 | 14.48 | 14.27 | 14.25 | 12.77 | 14 | 0.21 | 0.02 |
| 20001002 | 230 | 2 | 14.48 | 14.26 | 14.25 | 12.77 | 14 | 0.22 | 0.01 |
| 20001002 | 245 | 2 | 14.47 | 14.26 | 14.25 | 12.77 | 14 | 0.21 | 0.01 |
| 20001002 | 300 | 2 | 14.47 | 14.26 | 14.25 | 12.77 | 14 | 0.21 | 0.01 |
| 20001002 | 315 | 2 | 14.46 | 14.26 | 14.24 | 12.77 | 14 | 0.2 | 0.02 |
| 20001002 | 330 | 2 | 14.46 | 14.26 | 14.24 | 12.77 | 14 | 0.2 | 0.02 |
| 20001002 | 345 | 2 | 14.45 | 14.26 | 14.24 | 12.77 | 14 | 0.19 | 0.02 |
| 20001002 | 400 | 2 | 14.45 | 14.26 | 14.24 | 12.77 | 14 | 0.19 | 0.02 |
| 20001002 | 415 | 2 | 14.44 | 14.26 | 14.24 | 12.77 | 14 | 0.18 | 0.02 |
| 20001002 | 430 | 2 | 14.44 | 14.25 | 14.24 | 12.77 | 14 | 0.19 | 0.01 |
| 20001002 | 445 | 2 | 14.43 | 14.25 | 14.24 | 12.77 | 14 | 0.18 | 0.01 |
| 20001002 | 500 | 2 | 14.43 | 14.25 | 14.24 | 12.77 | 14 | 0.18 | 0.01 |
| 20001002 | 515 | 2 | 14.42 | 14.25 | 14.24 | 12.77 | 14 | 0.17 | 0.01 |
| 20001002 | 530 | 2 | 14.42 | 14.25 | 14.23 | 12.77 | 14 | 0.17 | 0.02 |
| 20001002 | 545 | 2 | 14.42 | 14.25 | 14.23 | 12.77 | 14 | 0.17 | 0.02 |
| 20001002 | 600 | 2 | 14.41 | 14.25 | 14.23 | 12.77 | 14 | 0.16 | 0.02 |
| 20001002 | 615 | 2 | 14.41 | 14.25 | 14.23 | 12.77 | 14 | 0.16 | 0.02 |
| 20001002 | 630 | 2 | 14.4 | 14.25 | 14.23 | 12.77 | 14 | 0.15 | 0.02 |
| 20001002 | 645 | 2 | 14.4 | 14.24 | 14.23 | 12.77 | 14 | 0.16 | 0.01 |
| 20001002 | 700 | 2 | 14.4 | 14.24 | 14.23 | 12.77 | 14 | 0.16 | 0.01 |
| 20001002 | 715 | 2 | 14.39 | 14.24 | 14.23 | 12.77 | 14 | 0.15 | 0.01 |
| 20001002 | 730 | 2 | 14.39 | 14.24 | 14.23 | 12.77 | 14 | 0.15 | 0.01 |
| 20001002 | 745 | 2 | 14.39 | 14.24 | 14.23 | 12.77 | 14 | 0.15 | 0.01 |
| 20001002 | 800 | 2 | 14.38 | 14.24 | 14.22 | 12.77 | 14 | 0.14 | 0.02 |
| 20001002 | 815 | 2 | 14.38 | 14.24 | 14.22 | 12.77 | 14 | 0.14 | 0.02 |
| 20001002 | 830 | 2 | 14.38 | 14.24 | 14.22 | 12.77 | 14 | 0.14 | 0.02 |
| 20001002 | 845 | 2 | 14.37 | 14.23 | 14.22 | 12.77 | 14 | 0.14 | 0.01 |
| 20001002 | 900 | 2 | 14.37 | 14.23 | 14.22 | 12.77 | 14 | 0.14 | 0.01 |
| 20001002 | 915 | 2 | 14.37 | 14.23 | 14.22 | 12.77 | 14 | 0.14 | 0.01 |
| 20001002 | 930 | 2 | 14.36 | 14.23 | 14.22 | 12.77 | 14 | 0.13 | 0.01 |
| 20001002 | 945 | 2 | 14.36 | 14.23 | 14.22 | 12.77 | 14 | 0.13 | 0.01 |
| 20001002 | 1000 | 2 | 14.36 | 14.23 | 14.22 | 12.77 | 14 | 0.13 | 0.01 |
| 20001002 | 1015 | 2 | 14.35 | 14.23 | 14.22 | 12.77 | 14 | 0.12 | 0.01 |
| 20001002 | 1030 | 2 | 14.35 | 14.23 | 14.21 | 12.77 | 14 | 0.12 | 0.02 |
| 20001002 | 1045 | 2 | 14.35 | 14.23 | 14.21 | 12.77 | 14 | 0.12 | 0.02 |
| 20001002 | 1100 | 2 | 14.34 | 14.23 | 14.21 | 12.77 | 14 | 0.11 | 0.02 |
| 20001002 | 1115 | 2 | 14.34 | 14.22 | 14.21 | 12.77 | 14 | 0.12 | 0.01 |
| 20001002 | 1130 | 2 | 14.34 | 14.22 | 14.21 | 12.77 | 14 | 0.12 | 0.01 |
| 20001002 | 1145 | 2 | 14.34 | 14.22 | 14.21 | 12.77 | 14 | 0.12 | 0.01 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001002 | 1200 | 2 | 14.33 | 14.22 | 14.21 | 12.76 | 14 | 0.11 | 0.01 |
| 20001002 | 1215 | 2 | 14.34 | 14.24 | 14.22 | 12.77 | 14 | 0.1 | 0.02 |
| 20001002 | 1230 | 2 | 14.34 | 14.23 | 14.22 | 12.76 | 14 | 0.11 | 0.01 |
| 20001002 | 1245 | 2 | 14.34 | 14.23 | 14.22 | 12.76 | 14 | 0.11 | 0.01 |
| 20001002 | 1300 | 2 | 14.34 | 14.23 | 14.21 | 12.75 | 14 | 0.11 | 0.02 |
| 20001002 | 1315 | 2 | 14.34 | 14.23 | 14.21 | 12.75 | 14 | 0.11 | 0.02 |
| 20001002 | 1330 | 2 | 14.33 | 14.23 | 14.21 | 12.77 | 14 | 0.1 | 0.02 |
| 20001002 | 1345 | 2 | 14.35 | 14.24 | 14.21 | 12.79 | 14 | 0.11 | 0.03 |
| 20001002 | 1400 | 2 | 14.35 | 14.24 | 14.22 | 12.79 | 14 | 0.11 | 0.02 |
| 20001002 | 1415 | 2 | 14.35 | 14.24 | 14.22 | 12.77 | 14 | 0.11 | 0.02 |
| 20001002 | 1430 | 2 | 14.34 | 14.23 | 14.22 | 12.77 | 14 | 0.11 | 0.01 |
| 20001002 | 1445 | 2 | 14.34 | 14.23 | 14.22 | 12.76 | 14 | 0.11 | 0.01 |
| 20001002 | 1500 | 2 | 14.34 | 14.23 | 14.22 | 12.77 | 14 | 0.11 | 0.01 |
| 20001002 | 1515 | 2 | 14.33 | 14.23 | 14.22 | 12.77 | 14 | 0.1 | 0.01 |
| 20001002 | 1530 | 2 | 14.33 | 14.23 | 14.22 | 12.78 | 14 | 0.1 | 0.01 |
| 20001002 | 1545 | 2 | 14.33 | 14.23 | 14.21 | 12.78 | 14 | 0.1 | 0.02 |
| 20001002 | 1600 | 2 | 14.33 | 14.23 | 14.21 | 12.78 | 14 | 0.1 | 0.02 |
| 20001002 | 1615 | 2 | 14.33 | 14.23 | 14.21 | 12.79 | 14 | 0.1 | 0.02 |
| 20001002 | 1630 | 2 | 14.32 | 14.22 | 14.21 | 12.78 | 14 | 0.1 | 0.01 |
| 20001002 | 1645 | 2 | 14.32 | 14.22 | 14.21 | 12.77 | 14 | 0.1 | 0.01 |
| 20001002 | 1700 | 2 | 14.32 | 14.22 | 14.21 | 12.77 | 14 | 0.1 | 0.01 |
| 20001002 | 1715 | 2 | 14.32 | 14.22 | 14.21 | 12.77 | 14 | 0.1 | 0.01 |
| 20001002 | 1730 | 2 | 14.31 | 14.22 | 14.21 | 12.78 | 14 | 0.09 | 0.01 |
| 20001002 | 1745 | 2 | 14.31 | 14.22 | 14.21 | 12.78 | 14 | 0.09 | 0.01 |
| 20001002 | 1800 | 2 | 14.31 | 14.22 | 14.21 | 12.78 | 14 | 0.09 | 0.01 |
| 20001002 | 1815 | 2 | 14.31 | 14.22 | 14.21 | 12.77 | 14 | 0.09 | 0.01 |
| 20001002 | 1830 | 2 | 14.3 | 14.22 | 14.2 | 12.77 | 14 | 0.08 | 0.02 |
| 20001002 | 1845 | 2 | 14.3 | 14.21 | 14.2 | 12.78 | 14 | 0.09 | 0.01 |
| 20001002 | 1900 | 2 | 14.3 | 14.21 | 14.2 | 12.78 | 14 | 0.09 | 0.01 |
| 20001002 | 1915 | 2 | 14.3 | 14.21 | 14.2 | 12.78 | 14 | 0.09 | 0.01 |
| 20001002 | 1930 | 2 | 14.3 | 14.21 | 14.2 | 12.77 | 14 | 0.09 | 0.01 |
| 20001002 | 1945 | 2 | 14.3 | 14.21 | 14.2 | 12.77 | 14 | 0.09 | 0.01 |
| 20001002 | 2000 | 2 | 14.3 | 14.21 | 14.2 | 12.77 | 14 | 0.09 | 0.01 |
| 20001002 | 2015 | 2 | 14.29 | 14.21 | 14.2 | 12.77 | 14 | 0.08 | 0.01 |
| 20001002 | 2030 | 2 | 14.29 | 14.21 | 14.2 | 12.77 | 14 | 0.08 | 0.01 |
| 20001002 | 2045 | 2 | 14.29 | 14.21 | 14.2 | 12.77 | 14 | 0.08 | 0.01 |
| 20001002 | 2100 | 2 | 14.29 | 14.21 | 14.2 | 12.77 | 14 | 0.08 | 0.01 |
| 20001002 | 2115 | 2 | 14.28 | 14.21 | 14.2 | 12.77 | 14 | 0.07 | 0.01 |
| 20001002 | 2130 | 2 | 14.28 | 14.21 | 14.2 | 12.77 | 14 | 0.07 | 0.01 |
| 20001002 | 2145 | 2 | 14.28 | 14.21 | 14.2 | 12.76 | 14 | 0.07 | 0.01 |
| 20001002 | 2200 | 2 | 14.28 | 14.2 | 14.2 | 12.76 | 14 | 0.08 | 0 |
| 20001002 | 2215 | 2 | 14.27 | 14.2 | 14.19 | 12.76 | 14 | 0.07 | 0.01 |
| 20001002 | 2230 | 2 | 14.27 | 14.2 | 14.19 | 12.76 | 14 | 0.07 | 0.01 |
| 20001002 | 2245 | 2 | 14.27 | 14.2 | 14.19 | 12.76 | 14 | 0.07 | 0.01 |
| 20001002 | 2300 | 2 | 14.27 | 14.2 | 14.19 | 12.76 | 14 | 0.07 | 0.01 |
| 20001002 | 2315 | 2 | 14.27 | 14.2 | 14.19 | 12.76 | 14 | 0.07 | 0.01 |
| 20001002 | 2330 | 2 | 14.26 | 14.2 | 14.19 | 12.75 | 14 | 0.06 | 0.01 |
| 20001002 | 2345 | 2 | 14.26 | 14.2 | 14.19 | 12.76 | 14 | 0.06 | 0.01 |
| 20001003 | 0 | 3 | 14.26 | 14.2 | 14.19 | 12.76 | 14 | 0.06 | 0.01 |
| 20001003 | 15 | 3 | 14.26 | 14.2 | 14.19 | 12.76 | 14 | 0.06 | 0.01 |
| 20001003 | 30 | 3 | 14.26 | 14.2 | 14.19 | 12.76 | 14 | 0.06 | 0.01 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001003 | 45 | 3 | 14.25 | 14.19 | 14.19 | 12.76 | 14 | 0.06 | 0 |
| 20001003 | 100 | 3 | 14.25 | 14.19 | 14.19 | 12.76 | 14 | 0.06 | 0 |
| 20001003 | 115 | 3 | 14.25 | 14.19 | 14.19 | 12.76 | 14 | 0.06 | 0 |
| 20001003 | 130 | 3 | 14.25 | 14.19 | 14.18 | 12.76 | 14 | 0.06 | 0.01 |
| 20001003 | 145 | 3 | 14.25 | 14.19 | 14.18 | 12.76 | 14 | 0.06 | 0.01 |
| 20001003 | 200 | 3 | 14.24 | 14.19 | 14.18 | 12.75 | 14 | 0.05 | 0.01 |
| 20001003 | 215 | 3 | 14.24 | 14.19 | 14.18 | 12.75 | 14 | 0.05 | 0.01 |
| 20001003 | 230 | 3 | 14.24 | 14.19 | 14.18 | 12.75 | 14 | 0.05 | 0.01 |
| 20001003 | 245 | 3 | 14.24 | 14.19 | 14.18 | 12.75 | 14 | 0.05 | 0.01 |
| 20001003 | 300 | 3 | 14.23 | 14.19 | 14.18 | 12.75 | 14 | 0.04 | 0.01 |
| 20001003 | 315 | 3 | 14.23 | 14.19 | 14.18 | 12.75 | 14 | 0.04 | 0.01 |
| 20001003 | 330 | 3 | 14.23 | 14.19 | 14.18 | 12.75 | 14 | 0.04 | 0.01 |
| 20001003 | 345 | 3 | 14.23 | 14.18 | 14.18 | 12.75 | 14 | 0.05 | 0 |
| 20001003 | 400 | 3 | 14.23 | 14.18 | 14.18 | 12.75 | 14 | 0.05 | 0 |
| 20001003 | 415 | 3 | 14.22 | 14.18 | 14.18 | 12.74 | 14 | 0.04 | 0 |
| 20001003 | 430 | 3 | 14.22 | 14.18 | 14.18 | 12.74 | 14 | 0.04 | 0 |
| 20001003 | 445 | 3 | 14.22 | 14.18 | 14.17 | 12.74 | 14 | 0.04 | 0.01 |
| 20001003 | 500 | 3 | 14.22 | 14.18 | 14.17 | 12.74 | 14 | 0.04 | 0.01 |
| 20001003 | 515 | 3 | 14.22 | 14.18 | 14.17 | 12.74 | 14 | 0.04 | 0.01 |
| 20001003 | 530 | 3 | 14.21 | 14.18 | 14.17 | 12.74 | 14 | 0.03 | 0.01 |
| 20001003 | 545 | 3 | 14.21 | 14.18 | 14.17 | 12.74 | 14 | 0.03 | 0.01 |
| 20001003 | 600 | 3 | 14.21 | 14.18 | 14.17 | 12.74 | 14 | 0.03 | 0.01 |
| 20001003 | 615 | 3 | 14.21 | 14.18 | 14.17 | 12.74 | 14 | 0.03 | 0.01 |
| 20001003 | 630 | 3 | 14.21 | 14.18 | 14.17 | 12.74 | 14 | 0.03 | 0.01 |
| 20001003 | 645 | 3 | 14.2 | 14.18 | 14.17 | 12.74 | 14 | 0.02 | 0.01 |
| 20001003 | 700 | 3 | 14.2 | 14.17 | 14.17 | 12.74 | 14 | 0.03 | 0 |
| 20001003 | 715 | 3 | 14.2 | 14.17 | 14.17 | 12.74 | 14 | 0.03 | 0 |
| 20001003 | 730 | 3 | 14.2 | 14.17 | 14.17 | 12.74 | 14 | 0.03 | 0 |
| 20001003 | 745 | 3 | 14.43 | 14.17 | 14.17 | 12.74 | 14 | 0.26 | 0 |
| 20001003 | 800 | 3 | 14.64 | 14.18 | 14.17 | 12.73 | 14 | 0.46 | 0.01 |
| 20001003 | 815 | 3 | 14.79 | 14.21 | 14.17 | 12.73 | 14 | 0.58 | 0.04 |
| 20001003 | 830 | 3 | 14.92 | 14.24 | 14.17 | 12.73 | 14 | 0.68 | 0.07 |
| 20001003 | 845 | 3 | 15 | 14.28 | 14.17 | 12.73 | 14 | 0.72 | 0.11 |
| 20001003 | 900 | 3 | 15.08 | 14.32 | 14.17 | 12.73 | 14 | 0.76 | 0.15 |
| 20001003 | 915 | 3 | 15.14 | 14.36 | 14.16 | 12.73 | 14 | 0.78 | 0.2 |
| 20001003 | 930 | 3 | 15.2 | 14.4 | 14.16 | 12.73 | 14 | 0.8 | 0.24 |
| 20001003 | 945 | 3 | 15.27 | 14.43 | 14.16 | 12.73 | 14 | 0.84 | 0.27 |
| 20001003 | 1000 | 3 | 15.32 | 14.47 | 14.16 | 12.73 | 14 | 0.85 | 0.31 |
| 20001003 | 1015 | 3 | 15.37 | 14.5 | 14.17 | 12.72 | 14 | 0.87 | 0.33 |
| 20001003 | 1030 | 3 | 15.42 | 14.53 | 14.17 | 12.72 | 14 | 0.89 | 0.36 |
| 20001003 | 1045 | 3 | 15.45 | 14.56 | 14.17 | 12.73 | 14 | 0.89 | 0.39 |
| 20001003 | 1100 | 3 | 15.49 | 14.58 | 14.17 | 12.73 | 14 | 0.91 | 0.41 |
| 20001003 | 1115 | 3 | 15.52 | 14.61 | 14.18 | 12.74 | 14 | 0.91 | 0.43 |
| 20001003 | 1130 | 3 | 15.55 | 14.63 | 14.18 | 12.74 | 14 | 0.92 | 0.45 |
| 20001003 | 1145 | 3 | 15.58 | 14.65 | 14.18 | 12.74 | 14 | 0.93 | 0.47 |
| 20001003 | 1200 | 3 | 15.59 | 14.66 | 14.18 | 12.73 | 14 | 0.93 | 0.48 |
| 20001003 | 1215 | 3 | 15.61 | 14.67 | 14.19 | 12.72 | 14 | 0.94 | 0.48 |
| 20001003 | 1230 | 3 | 15.63 | 14.69 | 14.19 | 12.72 | 14 | 0.94 | 0.5 |
| 20001003 | 1245 | 3 | 15.64 | 14.7 | 14.19 | 12.72 | 14 | 0.94 | 0.51 |
| 20001003 | 1300 | 3 | 15.65 | 14.71 | 14.2 | 12.73 | 14 | 0.94 | 0.51 |
| 20001003 | 1315 | 3 | 15.66 | 14.73 | 14.21 | 12.74 | 14 | 0.93 | 0.52 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001003 | 1330 | 3 | 15.67 | 14.74 | 14.21 | 12.75 | 14 | 0.93 | 0.53 |
| 20001003 | 1345 | 3 | 15.68 | 14.74 | 14.22 | 12.75 | 14 | 0.94 | 0.52 |
| 20001003 | 1400 | 3 | 15.69 | 14.75 | 14.22 | 12.75 | 14 | 0.94 | 0.53 |
| 20001003 | 1415 | 3 | 15.7 | 14.76 | 14.23 | 12.75 | 14 | 0.94 | 0.53 |
| 20001003 | 1430 | 3 | 15.7 | 14.77 | 14.24 | 12.75 | 14 | 0.93 | 0.53 |
| 20001003 | 1445 | 3 | 15.71 | 14.78 | 14.24 | 12.76 | 14 | 0.93 | 0.54 |
| 20001003 | 1500 | 3 | 15.72 | 14.79 | 14.25 | 12.76 | 14 | 0.93 | 0.54 |
| 20001003 | 1515 | 3 | 15.72 | 14.79 | 14.26 | 12.76 | 14 | 0.93 | 0.53 |
| 20001003 | 1530 | 3 | 15.73 | 14.8 | 14.26 | 12.76 | 14 | 0.93 | 0.54 |
| 20001003 | 1545 | 3 | 15.73 | 14.81 | 14.27 | 12.77 | 14 | 0.92 | 0.54 |
| 20001003 | 1600 | 3 | 15.73 | 14.81 | 14.28 | 12.77 | 14 | 0.92 | 0.53 |
| 20001003 | 1615 | 3 | 15.74 | 14.82 | 14.29 | 12.78 | 14 | 0.92 | 0.53 |
| 20001003 | 1630 | 3 | 15.74 | 14.83 | 14.3 | 12.79 | 14 | 0.91 | 0.53 |
| 20001003 | 1645 | 3 | 15.74 | 14.83 | 14.31 | 12.79 | 14 | 0.91 | 0.52 |
| 20001003 | 1700 | 3 | 15.74 | 14.84 | 14.31 | 12.8 | 14 | 0.9 | 0.53 |
| 20001003 | 1715 | 3 | 15.74 | 14.84 | 14.32 | 12.8 | 14 | 0.9 | 0.52 |
| 20001003 | 1730 | 3 | 15.74 | 14.84 | 14.33 | 12.8 | 14 | 0.9 | 0.51 |
| 20001003 | 1745 | 3 | 15.73 | 14.85 | 14.34 | 12.81 | 14 | 0.88 | 0.51 |
| 20001003 | 1800 | 3 | 15.73 | 14.85 | 14.34 | 12.81 | 14 | 0.88 | 0.51 |
| 20001003 | 1815 | 3 | 15.73 | 14.85 | 14.35 | 12.82 | 14 | 0.88 | 0.5 |
| 20001003 | 1830 | 3 | 15.73 | 14.85 | 14.36 | 12.81 | 14 | 0.88 | 0.49 |
| 20001003 | 1845 | 3 | 15.73 | 14.85 | 14.37 | 12.82 | 14 | 0.88 | 0.48 |
| 20001003 | 1900 | 3 | 15.73 | 14.86 | 14.39 | 12.84 | 14 | 0.87 | 0.47 |
| 20001003 | 1915 | 3 | 15.73 | 14.87 | 14.4 | 12.86 | 14 | 0.86 | 0.47 |
| 20001003 | 1930 | 3 | 15.73 | 14.87 | 14.41 | 12.87 | 14 | 0.86 | 0.46 |
| 20001003 | 1945 | 3 | 15.72 | 14.87 | 14.41 | 12.86 | 14 | 0.85 | 0.46 |
| 20001003 | 2000 | 3 | 15.72 | 14.87 | 14.42 | 12.86 | 14 | 0.85 | 0.45 |
| 20001003 | 2015 | 3 | 15.72 | 14.87 | 14.42 | 12.86 | 14 | 0.85 | 0.45 |
| 20001003 | 2030 | 3 | 15.71 | 14.87 | 14.43 | 12.88 | 14 | 0.84 | 0.44 |
| 20001003 | 2045 | 3 | 15.72 | 14.88 | 14.44 | 12.88 | 14 | 0.84 | 0.44 |
| 20001003 | 2100 | 3 | 15.74 | 14.91 | 14.46 | 12.92 | 14 | 0.83 | 0.45 |
| 20001003 | 2115 | 3 | 15.73 | 14.91 | 14.47 | 12.93 | 14 | 0.82 | 0.44 |
| 20001003 | 2130 | 3 | 15.74 | 14.92 | 14.49 | 12.94 | 14 | 0.82 | 0.43 |
| 20001003 | 2145 | 3 | 15.73 | 14.92 | 14.5 | 12.95 | 14 | 0.81 | 0.42 |
| 20001003 | 2200 | 3 | 15.73 | 14.92 | 14.51 | 12.94 | 14 | 0.81 | 0.41 |
| 20001003 | 2215 | 3 | 15.73 | 14.92 | 14.51 | 12.95 | 14 | 0.81 | 0.41 |
| 20001003 | 2230 | 3 | 15.72 | 14.93 | 14.51 | 12.96 | 14 | 0.79 | 0.42 |
| 20001003 | 2245 | 3 | 15.72 | 14.93 | 14.52 | 12.96 | 14 | 0.79 | 0.41 |
| 20001003 | 2300 | 3 | 15.72 | 14.93 | 14.53 | 12.97 | 14 | 0.79 | 0.4 |
| 20001003 | 2315 | 3 | 15.72 | 14.94 | 14.53 | 12.98 | 14 | 0.78 | 0.41 |
| 20001003 | 2330 | 3 | 15.72 | 14.94 | 14.54 | 12.98 | 14 | 0.78 | 0.4 |
| 20001003 | 2345 | 3 | 15.71 | 14.94 | 14.54 | 12.99 | 14 | 0.77 | 0.4 |
| 20001004 | 0 | 4 | 15.71 | 14.94 | 14.55 | 12.99 | 14 | 0.77 | 0.39 |
| 20001004 | 15 | 4 | 15.71 | 14.94 | 14.55 | 12.99 | 14 | 0.77 | 0.39 |
| 20001004 | 30 | 4 | 15.7 | 14.94 | 14.56 | 13 | 14 | 0.76 | 0.38 |
| 20001004 | 45 | 4 | 15.71 | 14.95 | 14.58 | 13.02 | 14 | 0.76 | 0.37 |
| 20001004 | 100 | 4 | 15.71 | 14.95 | 14.59 | 13.05 | 14 | 0.76 | 0.36 |
| 20001004 | 115 | 4 | 15.71 | 14.96 | 14.6 | 13.07 | 14 | 0.75 | 0.36 |
| 20001004 | 130 | 4 | 15.74 | 15.03 | 14.62 | 13.14 | 14 | 0.71 | 0.41 |
| 20001004 | 145 | 4 | 15.81 | 15.1 | 14.68 | 13.23 | 14 | 0.71 | 0.42 |
| 20001004 | 200 | 4 | 15.87 | 15.17 | 14.72 | 13.29 | 14 | 0.7 | 0.45 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001004 | 215 | 4 | 15.88 | 15.18 | 14.74 | 13.3 | 14 | 0.7 | 0.44 |
| 20001004 | 230 | 4 | 15.93 | 15.26 | 14.81 | 13.36 | 14 | 0.67 | 0.45 |
| 20001004 | 245 | 4 | 15.93 | 15.29 | 14.85 | 13.41 | 14 | 0.64 | 0.44 |
| 20001004 | 300 | 4 | 15.95 | 15.33 | 14.87 | 13.46 | 14 | 0.62 | 0.46 |
| 20001004 | 315 | 4 | 15.96 | 15.35 | 14.89 | 13.49 | 14 | 0.61 | 0.46 |
| 20001004 | 330 | 4 | 15.97 | 15.38 | 14.92 | 13.52 | 14 | 0.59 | 0.46 |
| 20001004 | 345 | 4 | 16.03 | 15.43 | 14.96 | 13.61 | 14 | 0.6 | 0.47 |
| 20001004 | 400 | 4 | 16.05 | 15.47 | 15.03 | 13.71 | 14 | 0.58 | 0.44 |
| 20001004 | 415 | 4 | 16.03 | 15.48 | 15.05 | 13.78 | 14 | 0.55 | 0.43 |
| 20001004 | 430 | 4 | 16.06 | 15.54 | 15.09 | 13.83 | 14 | 0.52 | 0.45 |
| 20001004 | 445 | 4 | 16.12 | 15.62 | 15.16 | 13.94 | 14 | 0.5 | 0.46 |
| 20001004 | 500 | 4 | 16.15 | 15.68 | 15.25 | 14.05 | 14 | 0.47 | 0.43 |
| 20001004 | 515 | 4 | 16.14 | 15.7 | 15.31 | 14.11 | 14 | 0.44 | 0.39 |
| 20001004 | 530 | 4 | 16.14 | 15.73 | 15.36 | 14.17 | 14 | 0.41 | 0.37 |
| 20001004 | 545 | 4 | 16.12 | 15.74 | 15.37 | 14.2 | 14 | 0.38 | 0.37 |
| 20001004 | 600 | 4 | 16.13 | 15.79 | 15.42 | 14.24 | 14 | 0.34 | 0.37 |
| 20001004 | 615 | 4 | 16.12 | 15.8 | 15.44 | 14.28 | 14 | 0.32 | 0.36 |
| 20001004 | 630 | 4 | 16.1 | 15.81 | 15.46 | 14.29 | 14 | 0.29 | 0.35 |
| 20001004 | 645 | 4 | 16.08 | 15.81 | 15.47 | 14.3 | 14 | 0.27 | 0.34 |
| 20001004 | 700 | 4 | 16.07 | 15.81 | 15.48 | 14.31 | 14 | 0.26 | 0.33 |
| 20001004 | 715 | 4 | 16.07 | 15.83 | 15.51 | 14.33 | 14 | 0.24 | 0.32 |
| 20001004 | 730 | 4 | 16.05 | 15.83 | 15.51 | 14.34 | 14 | 0.22 | 0.32 |
| 20001004 | 745 | 4 | 16.04 | 15.83 | 15.52 | 14.34 | 14 | 0.21 | 0.31 |
| 20001004 | 800 | 4 | 16.06 | 15.86 | 15.52 | 14.35 | 14 | 0.2 | 0.34 |
| 20001004 | 815 | 4 | 16.06 | 15.87 | 15.55 | 14.39 | 14 | 0.19 | 0.32 |
| 20001004 | 830 | 4 | 16.07 | 15.88 | 15.56 | 14.4 | 14 | 0.19 | 0.32 |
| 20001004 | 845 | 4 | 16.06 | 15.88 | 15.58 | 14.4 | 14 | 0.18 | 0.3 |
| 20001004 | 900 | 4 | 16.1 | 15.93 | 15.61 | 14.44 | 14 | 0.17 | 0.32 |
| 20001004 | 915 | 4 | 16.13 | 15.97 | 15.65 | 14.49 | 14 | 0.16 | 0.32 |
| 20001004 | 930 | 4 | 16.14 | 16 | 15.68 | 14.52 | 14 | 0.14 | 0.32 |
| 20001004 | 945 | 4 | 16.15 | 16.01 | 15.7 | 14.54 | 14 | 0.14 | 0.31 |
| 20001004 | 1000 | 4 | 16.14 | 16.01 | 15.71 | 14.54 | 14 | 0.13 | 0.3 |
| 20001004 | 1015 | 4 | 16.13 | 16.01 | 15.72 | 14.54 | 14 | 0.12 | 0.29 |
| 20001004 | 1030 | 4 | 16.12 | 16 | 15.73 | 14.53 | 14 | 0.12 | 0.27 |
| 20001004 | 1045 | 4 | 16.11 | 15.99 | 15.73 | 14.53 | 14 | 0.12 | 0.26 |
| 20001004 | 1100 | 4 | 16.09 | 15.99 | 15.73 | 14.52 | 14 | 0.1 | 0.26 |
| 20001004 | 1115 | 4 | 16.09 | 15.99 | 15.73 | 14.52 | 14 | 0.1 | 0.26 |
| 20001004 | 1130 | 4 | 16.09 | 15.98 | 15.73 | 14.51 | 14 | 0.11 | 0.25 |
| 20001004 | 1145 | 4 | 16.09 | 15.99 | 15.73 | 14.51 | 14 | 0.1 | 0.26 |
| 20001004 | 1200 | 4 | 16.09 | 15.99 | 15.73 | 14.5 | 14 | 0.1 | 0.26 |
| 20001004 | 1215 | 4 | 16.08 | 15.98 | 15.73 | 14.5 | 14 | 0.1 | 0.25 |
| 20001004 | 1230 | 4 | 16.08 | 15.98 | 15.73 | 14.49 | 14 | 0.1 | 0.25 |
| 20001004 | 1245 | 4 | 16.07 | 15.98 | 15.73 | 14.48 | 14 | 0.09 | 0.25 |
| 20001004 | 1300 | 4 | 16.07 | 15.97 | 15.73 | 14.47 | 14 | 0.1 | 0.24 |
| 20001004 | 1315 | 4 | 16.07 | 15.97 | 15.73 | 14.47 | 14 | 0.1 | 0.24 |
| 20001004 | 1330 | 4 | 16.06 | 15.97 | 15.73 | 14.46 | 14 | 0.09 | 0.24 |
| 20001004 | 1345 | 4 | 16.06 | 15.97 | 15.72 | 14.46 | 14 | 0.09 | 0.25 |
| 20001004 | 1400 | 4 | 16.06 | 15.96 | 15.72 | 14.45 | 14 | 0.1 | 0.24 |
| 20001004 | 1415 | 4 | 16.06 | 15.96 | 15.72 | 14.44 | 14 | 0.1 | 0.24 |
| 20001004 | 1430 | 4 | 16.05 | 15.96 | 15.71 | 14.44 | 14 | 0.09 | 0.25 |
| 20001004 | 1445 | 4 | 16.05 | 15.96 | 15.71 | 14.43 | 14 | 0.09 | 0.25 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001004 | 1500 | 4 | 16.05 | 15.95 | 15.71 | 14.42 | 14 | 0.1 | 0.24 |
| 20001004 | 1515 | 4 | 16.05 | 15.95 | 15.7 | 14.42 | 14 | 0.1 | 0.25 |
| 20001004 | 1530 | 4 | 16.05 | 15.95 | 15.7 | 14.41 | 14 | 0.1 | 0.25 |
| 20001004 | 1545 | 4 | 16.05 | 15.95 | 15.7 | 14.41 | 14 | 0.1 | 0.25 |
| 20001004 | 1600 | 4 | 16.05 | 15.95 | 15.7 | 14.41 | 14 | 0.1 | 0.25 |
| 20001004 | 1615 | 4 | 16.05 | 15.94 | 15.69 | 14.4 | 14 | 0.11 | 0.25 |
| 20001004 | 1630 | 4 | 16.05 | 15.94 | 15.69 | 14.4 | 14 | 0.11 | 0.25 |
| 20001004 | 1645 | 4 | 16.03 | 15.93 | 15.69 | 14.4 | 14 | 0.1 | 0.24 |
| 20001004 | 1700 | 4 | 16.03 | 15.93 | 15.69 | 14.4 | 14 | 0.1 | 0.24 |
| 20001004 | 1715 | 4 | 16.05 | 15.94 | 15.69 | 14.39 | 14 | 0.11 | 0.25 |
| 20001004 | 1730 | 4 | 16.05 | 15.94 | 15.68 | 14.39 | 14 | 0.11 | 0.26 |
| 20001004 | 1745 | 4 | 16.05 | 15.94 | 15.68 | 14.39 | 14 | 0.11 | 0.26 |
| 20001004 | 1800 | 4 | 16.05 | 15.94 | 15.68 | 14.4 | 14 | 0.11 | 0.26 |
| 20001004 | 1815 | 4 | 16.05 | 15.93 | 15.68 | 14.4 | 14 | 0.12 | 0.25 |
| 20001004 | 1830 | 4 | 16.05 | 15.93 | 15.67 | 14.4 | 14 | 0.12 | 0.26 |
| 20001004 | 1845 | 4 | 16.05 | 15.93 | 15.67 | 14.4 | 14 | 0.12 | 0.26 |
| 20001004 | 1900 | 4 | 16.05 | 15.93 | 15.67 | 14.4 | 14 | 0.12 | 0.26 |
| 20001004 | 1915 | 4 | 16.05 | 15.93 | 15.67 | 14.4 | 14 | 0.12 | 0.26 |
| 20001004 | 1930 | 4 | 16.05 | 15.93 | 15.67 | 14.4 | 14 | 0.12 | 0.26 |
| 20001004 | 1945 | 4 | 16.05 | 15.93 | 15.67 | 14.41 | 14 | 0.12 | 0.26 |
| 20001004 | 2000 | 4 | 16.05 | 15.93 | 15.66 | 14.41 | 14 | 0.12 | 0.27 |
| 20001004 | 2015 | 4 | 16.05 | 15.93 | 15.66 | 14.41 | 14 | 0.12 | 0.27 |
| 20001004 | 2030 | 4 | 16.05 | 15.92 | 15.66 | 14.42 | 14 | 0.13 | 0.26 |
| 20001004 | 2045 | 4 | 16.05 | 15.92 | 15.66 | 14.42 | 14 | 0.13 | 0.26 |
| 20001004 | 2100 | 4 | 16.04 | 15.92 | 15.66 | 14.42 | 14 | 0.12 | 0.26 |
| 20001004 | 2115 | 4 | 16.04 | 15.92 | 15.66 | 14.42 | 14 | 0.12 | 0.26 |
| 20001004 | 2130 | 4 | 16.04 | 15.92 | 15.66 | 14.42 | 14 | 0.12 | 0.26 |
| 20001004 | 2145 | 4 | 16.04 | 15.92 | 15.66 | 14.42 | 14 | 0.12 | 0.26 |
| 20001004 | 2200 | 4 | 16.04 | 15.92 | 15.65 | 14.42 | 14 | 0.12 | 0.27 |
| 20001004 | 2215 | 4 | 16.04 | 15.91 | 15.65 | 14.42 | 14 | 0.13 | 0.26 |
| 20001004 | 2230 | 4 | 16.04 | 15.91 | 15.65 | 14.42 | 14 | 0.13 | 0.26 |
| 20001004 | 2245 | 4 | 16.04 | 15.91 | 15.65 | 14.42 | 14 | 0.13 | 0.26 |
| 20001004 | 2300 | 4 | 16.04 | 15.91 | 15.65 | 14.42 | 14 | 0.13 | 0.26 |
| 20001004 | 2315 | 4 | 16.04 | 15.91 | 15.65 | 14.42 | 14 | 0.13 | 0.26 |
| 20001004 | 2330 | 4 | 16.03 | 15.91 | 15.65 | 14.42 | 14 | 0.12 | 0.26 |
| 20001004 | 2345 | 4 | 16.03 | 15.91 | 15.65 | 14.42 | 14 | 0.12 | 0.26 |
| 20001005 | 0 |  | 16.03 | 15.9 | 15.64 | 14.42 | 14 | 0.13 | 0.26 |
| 20001005 | 15 | 5 | 16.03 | 15.9 | 15.64 | 14.42 | 14 | 0.13 | 0.26 |
| 20001005 | 30 | 5 | 16.03 | 15.9 | 15.64 | 14.42 | 14 | 0.13 | 0.26 |
| 20001005 | 45 | 5 | 16.03 | 15.9 | 15.64 | 14.42 | 14 | 0.13 | 0.26 |
| 20001005 | 100 | 5 | 16.03 | 15.9 | 15.64 | 14.42 | 14 | 0.13 | 0.26 |
| 20001005 | 115 | 5 | 16.03 | 15.9 | 15.64 | 14.42 | 14 | 0.13 | 0.26 |
| 20001005 | 130 | 5 | 16.03 | 15.9 | 15.64 | 14.41 | 14 | 0.13 | 0.26 |
| 20001005 | 145 | 5 | 16.03 | 15.9 | 15.63 | 14.41 | 14 | 0.13 | 0.27 |
| 20001005 | 200 | 5 | 16.03 | 15.89 | 15.63 | 14.41 | 14 | 0.14 | 0.26 |
| 20001005 | 215 | 5 | 16.03 | 15.89 | 15.63 | 14.41 | 14 | 0.14 | 0.26 |
| 20001005 | 230 | 5 | 16.02 | 15.89 | 15.63 | 14.41 | 14 | 0.13 | 0.26 |
| 20001005 | 245 | 5 | 16.02 | 15.89 | 15.63 | 14.41 | 14 | 0.13 | 0.26 |
| 20001005 | 300 | 5 | 16.02 | 15.89 | 15.63 | 14.41 | 14 | 0.13 | 0.26 |
| 20001005 | 315 | 5 | 16.02 | 15.89 | 15.63 | 14.41 | 14 | 0.13 | 0.26 |
| 20001005 | 330 | 5 | 16.02 | 15.89 | 15.63 | 14.41 | 14 | 0.13 | 0.26 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001005 | 345 | 5 | 16.02 | 15.89 | 15.62 | 14.41 | 14 | 0.13 | 0.27 |
| 20001005 | 400 | 5 | 16.02 | 15.89 | 15.62 | 14.41 | 14 | 0.13 | 0.27 |
| 20001005 | 415 | 5 | 16.02 | 15.88 | 15.62 | 14.41 | 14 | 0.14 | 0.26 |
| 20001005 | 430 | 5 | 16.02 | 15.88 | 15.62 | 14.4 | 14 | 0.14 | 0.26 |
| 20001005 | 445 | 5 | 16.02 | 15.88 | 15.62 | 14.4 | 14 | 0.14 | 0.26 |
| 20001005 | 500 | 5 | 16.02 | 15.88 | 15.62 | 14.4 | 14 | 0.14 | 0.26 |
| 20001005 | 515 | 5 | 16.02 | 15.88 | 15.62 | 14.4 | 14 | 0.14 | 0.26 |
| 20001005 | 530 | 5 | 16.01 | 15.88 | 15.61 | 14.4 | 14 | 0.13 | 0.27 |
| 20001005 | 545 | 5 | 16.01 | 15.88 | 15.61 | 14.4 | 14 | 0.13 | 0.27 |
| 20001005 | 600 | 5 | 16.01 | 15.88 | 15.61 | 14.4 | 14 | 0.13 | 0.27 |
| 20001005 | 615 | 5 | 16.01 | 15.88 | 15.61 | 14.4 | 14 | 0.13 | 0.27 |
| 20001005 | 630 | 5 | 16.01 | 15.88 | 15.61 | 14.4 | 14 | 0.13 | 0.27 |
| 20001005 | 645 | 5 | 16.01 | 15.88 | 15.61 | 14.39 | 14 | 0.13 | 0.27 |
| 20001005 | 700 | 5 | 16.01 | 15.87 | 15.61 | 14.39 | 14 | 0.14 | 0.26 |
| 20001005 | 715 | 5 | 16.01 | 15.87 | 15.61 | 14.39 | 14 | 0.14 | 0.26 |
| 20001005 | 730 | 5 | 16.01 | 15.87 | 15.6 | 14.39 | 14 | 0.14 | 0.27 |
| 20001005 | 745 | 5 | 16.01 | 15.87 | 15.6 | 14.39 | 14 | 0.14 | 0.27 |
| 20001005 | 800 | 5 | 16.01 | 15.87 | 15.6 | 14.39 | 14 | 0.14 | 0.27 |
| 20001005 | 815 | 5 | 16.01 | 15.87 | 15.6 | 14.39 | 14 | 0.14 | 0.27 |
| 20001005 | 830 | 5 | 16.01 | 15.87 | 15.6 | 14.39 | 14 | 0.14 | 0.27 |
| 20001005 | 845 | 5 | 16.01 | 15.87 | 15.6 | 14.39 | 14 | 0.14 | 0.27 |
| 20001005 | 900 | 5 | 16.01 | 15.87 | 15.6 | 14.39 | 14 | 0.14 | 0.27 |
| 20001005 | 915 | 5 | 16.01 | 15.87 | 15.6 | 14.38 | 14 | 0.14 | 0.27 |
| 20001005 | 930 | 5 | 16 | 15.86 | 15.6 | 14.38 | 14 | 0.14 | 0.26 |
| 20001005 | 945 | 5 | 16 | 15.86 | 15.6 | 14.38 | 14 | 0.14 | 0.26 |
| 20001005 | 1000 | 5 | 16 | 15.86 | 15.59 | 14.38 | 14 | 0.14 | 0.27 |
| 20001005 | 1015 | 5 | 16 | 15.86 | 15.59 | 14.38 | 14 | 0.14 | 0.27 |
| 20001005 | 1030 | 5 | 16 | 15.86 | 15.59 | 14.37 | 14 | 0.14 | 0.27 |
| 20001005 | 1045 | 5 | 16 | 15.86 | 15.59 | 14.37 | 14 | 0.14 | 0.27 |
| 20001005 | 1100 | 5 | 16 | 15.86 | 15.59 | 14.37 | 14 | 0.14 | 0.27 |
| 20001005 | 1115 | 5 | 16 | 15.86 | 15.59 | 14.36 | 14 | 0.14 | 0.27 |
| 20001005 | 1130 | 5 | 15.97 | 15.85 | 15.59 | 14.35 | 14 | 0.12 | 0.26 |
| 20001005 | 1145 | 5 | 15.99 | 15.85 | 15.59 | 14.35 | 14 | 0.14 | 0.26 |
| 20001005 | 1200 | 5 | 16 | 15.85 | 15.58 | 14.34 | 14 | 0.15 | 0.27 |
| 20001005 | 1215 | 5 | 15.99 | 15.85 | 15.58 | 14.33 | 14 | 0.14 | 0.27 |
| 20001005 | 1230 | 5 | 15.99 | 15.85 | 15.58 | 14.32 | 14 | 0.14 | 0.27 |
| 20001005 | 1245 | 5 | 15.99 | 15.85 | 15.58 | 14.31 | 14 | 0.14 | 0.27 |
| 20001005 | 1300 | 5 | 15.99 | 15.85 | 15.58 | 14.31 | 14 | 0.14 | 0.27 |
| 20001005 | 1315 | 5 | 15.99 | 15.85 | 15.58 | 14.3 | 14 | 0.14 | 0.27 |
| 20001005 | 1330 | 5 | 15.99 | 15.85 | 15.57 | 14.29 | 14 | 0.14 | 0.28 |
| 20001005 | 1345 | 5 | 15.99 | 15.85 | 15.57 | 14.29 | 14 | 0.14 | 0.28 |
| 20001005 | 1400 | 5 | 15.99 | 15.85 | 15.57 | 14.28 | 14 | 0.14 | 0.28 |
| 20001005 | 1415 | 5 | 15.99 | 15.84 | 15.57 | 14.28 | 14 | 0.15 | 0.27 |
| 20001005 | 1430 | 5 | 15.99 | 15.84 | 15.57 | 14.27 | 14 | 0.15 | 0.27 |
| 20001005 | 1445 | 5 | 15.99 | 15.84 | 15.57 | 14.27 | 14 | 0.15 | 0.27 |
| 20001005 | 1500 | 5 | 15.99 | 15.84 | 15.56 | 14.27 | 14 | 0.15 | 0.28 |
| 20001005 | 1515 | 5 | 15.99 | 15.84 | 15.56 | 14.27 | 14 | 0.15 | 0.28 |
| 20001005 | 1530 | 5 | 15.99 | 15.84 | 15.56 | 14.26 | 14 | 0.15 | 0.28 |
| 20001005 | 1545 | 5 | 15.99 | 15.84 | 15.56 | 14.26 | 14 | 0.15 | 0.28 |
| 20001005 | 1600 | 5 | 15.99 | 15.84 | 15.56 | 14.25 | 14 | 0.15 | 0.28 |
| 20001005 | 1615 | 5 | 15.99 | 15.84 | 15.56 | 14.25 | 14 | 0.15 | 0.28 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001005 | 1630 | 5 | 15.99 | 15.84 | 15.55 | 14.24 | 14 | 0.15 | 0.29 |
| 20001005 | 1645 | 5 | 15.99 | 15.83 | 15.55 | 14.24 | 14 | 0.16 | 0.28 |
| 20001005 | 1700 | 5 | 15.99 | 15.83 | 15.55 | 14.24 | 14 | 0.16 | 0.28 |
| 20001005 | 1715 | 5 | 15.96 | 15.83 | 15.55 | 14.24 | 14 | 0.13 | 0.28 |
| 20001005 | 1730 | 5 | 15.97 | 15.83 | 15.55 | 14.23 | 14 | 0.14 | 0.28 |
| 20001005 | 1745 | 5 | 15.97 | 15.82 | 15.55 | 14.23 | 14 | 0.15 | 0.27 |
| 20001005 | 1800 | 5 | 15.97 | 15.82 | 15.55 | 14.23 | 14 | 0.15 | 0.27 |
| 20001005 | 1815 | 5 | 15.86 | 15.8 | 15.54 | 14.23 | 14 | 0.06 | 0.26 |
| 20001005 | 1830 | 5 | 15.97 | 15.82 | 15.54 | 14.22 | 14 | 0.15 | 0.28 |
| 20001005 | 1845 | 5 | 16.01 | 15.82 | 15.54 | 14.22 | 14 | 0.19 | 0.28 |
| 20001005 | 1900 | 5 | 16.01 | 15.83 | 15.54 | 14.22 | 14 | 0.18 | 0.29 |
| 20001005 | 1915 | 5 | 16.03 | 15.83 | 15.54 | 14.22 | 14 | 0.2 | 0.29 |
| 20001005 | 1930 | 5 | 16.05 | 15.84 | 15.54 | 14.22 | 14 | 0.21 | 0.3 |
| 20001005 | 1945 | 5 | 16.06 | 15.85 | 15.54 | 14.22 | 14 | 0.21 | 0.31 |
| 20001005 | 2000 | 5 | 16.07 | 15.85 | 15.54 | 14.21 | 14 | 0.22 | 0.31 |
| 20001005 | 2015 | 5 | 16.08 | 15.85 | 15.54 | 14.21 | 14 | 0.23 | 0.31 |
| 20001005 | 2030 | 5 | 16.08 | 15.86 | 15.54 | 14.21 | 14 | 0.22 | 0.32 |
| 20001005 | 2045 | 5 | 16.09 | 15.86 | 15.54 | 14.21 | 14 | 0.23 | 0.32 |
| 20001005 | 2100 | 5 | 16.09 | 15.86 | 15.54 | 14.21 | 14 | 0.23 | 0.32 |
| 20001005 | 2115 | 5 | 16.09 | 15.87 | 15.54 | 14.21 | 14 | 0.22 | 0.33 |
| 20001005 | 2130 | 5 | 16.1 | 15.87 | 15.54 | 14.21 | 14 | 0.23 | 0.33 |
| 20001005 | 2145 | 5 | 16.1 | 15.87 | 15.54 | 14.2 | 14 | 0.23 | 0.33 |
| 20001005 | 2200 | 5 | 16.1 | 15.87 | 15.54 | 14.2 | 14 | 0.23 | 0.33 |
| 20001005 | 2215 | 5 | 16.09 | 15.87 | 15.54 | 14.2 | 14 | 0.22 | 0.33 |
| 20001005 | 2230 | 5 | 16.09 | 15.87 | 15.54 | 14.2 | 14 | 0.22 | 0.33 |
| 20001005 | 2245 | 5 | 16.09 | 15.87 | 15.54 | 14.2 | 14 | 0.22 | 0.33 |
| 20001005 | 2300 | 5 | 16.09 | 15.87 | 15.54 | 14.2 | 14 | 0.22 | 0.33 |
| 20001005 | 2315 | 5 | 16.09 | 15.87 | 15.54 | 14.2 | 14 | 0.22 | 0.33 |
| 20001005 | 2330 | 5 | 16.09 | 15.87 | 15.55 | 14.2 | 14 | 0.22 | 0.32 |
| 20001005 | 2345 | 5 | 16.09 | 15.87 | 15.55 | 14.19 | 14 | 0.22 | 0.32 |
| 20001006 | 0 | 6 | 16.09 | 15.87 | 15.55 | 14.2 | 14 | 0.22 | 0.32 |
| 20001006 | 15 | 6 | 16.09 | 15.87 | 15.55 | 14.19 | 14 | 0.22 | 0.32 |
| 20001006 | 30 | 6 | 16.09 | 15.88 | 15.55 | 14.19 | 14 | 0.21 | 0.33 |
| 20001006 | 45 | 6 | 16.09 | 15.88 | 15.55 | 14.19 | 14 | 0.21 | 0.33 |
| 20001006 | 100 | 6 | 16.09 | 15.88 | 15.55 | 14.19 | 14 | 0.21 | 0.33 |
| 20001006 | 115 | 6 | 16.09 | 15.88 | 15.55 | 14.19 | 14 | 0.21 | 0.33 |
| 20001006 | 130 | 6 | 16.09 | 15.88 | 15.55 | 14.19 | 14 | 0.21 | 0.33 |
| 20001006 | 145 | 6 | 16.09 | 15.88 | 15.55 | 14.19 | 14 | 0.21 | 0.33 |
| 20001006 | 200 | 6 | 16.09 | 15.88 | 15.55 | 14.19 | 14 | 0.21 | 0.33 |
| 20001006 | 215 | 6 | 16.09 | 15.88 | 15.56 | 14.19 | 14 | 0.21 | 0.32 |
| 20001006 | 230 | 6 | 16.09 | 15.88 | 15.56 | 14.19 | 14 | 0.21 | 0.32 |
| 20001006 | 245 | 6 | 16.09 | 15.88 | 15.56 | 14.19 | 14 | 0.21 | 0.32 |
| 20001006 | 300 | 6 | 16.09 | 15.88 | 15.56 | 14.19 | 14 | 0.21 | 0.32 |
| 20001006 | 315 | 6 | 16.08 | 15.88 | 15.56 | 14.19 | 14 | 0.2 | 0.32 |
| 20001006 | 330 | 6 | 16.09 | 15.88 | 15.56 | 14.19 | 14 | 0.21 | 0.32 |
| 20001006 | 345 | 6 | 16.08 | 15.88 | 15.56 | 14.19 | 14 | 0.2 | 0.32 |
| 20001006 | 400 | 6 | 16.09 | 15.88 | 15.56 | 14.19 | 14 | 0.21 | 0.32 |
| 20001006 | 415 | 6 | 16.09 | 15.88 | 15.56 | 14.19 | 14 | 0.21 | 0.32 |
| 20001006 | 430 | 6 | 16.09 | 15.89 | 15.56 | 14.19 | 14 | 0.2 | 0.33 |
| 20001006 | 445 | 6 | 16.09 | 15.89 | 15.56 | 14.18 | 14 | 0.2 | 0.33 |
| 20001006 | 500 | 6 | 16.09 | 15.89 | 15.56 | 14.18 | 14 | 0.2 | 0.33 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001006 | 515 | 6 | 16.09 | 15.89 | 15.56 | 14.18 | 14 | 0.2 | 0.33 |
| 20001006 | 530 | 6 | 16.09 | 15.89 | 15.56 | 14.18 | 14 | 0.2 | 0.33 |
| 20001006 | 545 | 6 | 16.09 | 15.89 | 15.56 | 14.18 | 14 | 0.2 | 0.33 |
| 20001006 | 600 | 6 | 16.09 | 15.89 | 15.56 | 14.18 | 14 | 0.2 | 0.33 |
| 20001006 | 615 | 6 | 16.09 | 15.89 | 15.57 | 14.18 | 14 | 0.2 | 0.32 |
| 20001006 | 630 | 6 | 16.09 | 15.89 | 15.57 | 14.18 | 14 | 0.2 | 0.32 |
| 20001006 | 645 | 6 | 16.09 | 15.89 | 15.57 | 14.18 | 14 | 0.2 | 0.32 |
| 20001006 | 700 | 6 | 16.09 | 15.89 | 15.57 | 14.18 | 14 | 0.2 | 0.32 |
| 20001006 | 715 | 6 | 16.09 | 15.89 | 15.57 | 14.18 | 14 | 0.2 | 0.32 |
| 20001006 | 730 | 6 | 16.09 | 15.89 | 15.57 | 14.18 | 14 | 0.2 | 0.32 |
| 20001006 | 745 | 6 | 16.09 | 15.89 | 15.57 | 14.18 | 14 | 0.2 | 0.32 |
| 20001006 | 800 | 6 | 16.09 | 15.89 | 15.57 | 14.18 | 14 | 0.2 | 0.32 |
| 20001006 | 815 | 6 | 16.09 | 15.9 | 15.57 | 14.18 | 14 | 0.19 | 0.33 |
| 20001006 | 830 | 6 | 16.09 | 15.9 | 15.57 | 14.18 | 14 | 0.19 | 0.33 |
| 20001006 | 845 | 6 | 16.09 | 15.9 | 15.57 | 14.18 | 14 | 0.19 | 0.33 |
| 20001006 | 900 | 6 | 16.09 | 15.9 | 15.57 | 14.18 | 14 | 0.19 | 0.33 |
| 20001006 | 915 | 6 | 16.09 | 15.9 | 15.57 | 14.18 | 14 | 0.19 | 0.33 |
| 20001006 | 930 | 6 | 16.08 | 15.9 | 15.57 | 14.18 | 14 | 0.18 | 0.33 |
| 20001006 | 945 | 6 | 16.08 | 15.9 | 15.57 | 14.18 | 14 | 0.18 | 0.33 |
| 20001006 | 1000 | 6 | 16.07 | 15.89 | 15.57 | 14.17 | 14 | 0.18 | 0.32 |
| 20001006 | 1015 | 6 | 16.08 | 15.9 | 15.57 | 14.17 | 14 | 0.18 | 0.33 |
| 20001006 | 1030 | 6 | 16.09 | 15.9 | 15.57 | 14.17 | 14 | 0.19 | 0.33 |
| 20001006 | 1045 | 6 | 16.09 | 15.9 | 15.57 | 14.17 | 14 | 0.19 | 0.33 |
| 20001006 | 1100 | 6 | 16.09 | 15.9 | 15.57 | 14.17 | 14 | 0.19 | 0.33 |
| 20001006 | 1115 | 6 | 16.1 | 15.9 | 15.57 | 14.17 | 14 | 0.2 | 0.33 |
| 20001006 | 1130 | 6 | 16.1 | 15.9 | 15.57 | 14.17 | 14 | 0.2 | 0.33 |
| 20001006 | 1145 | 6 | 16.1 | 15.9 | 15.57 | 14.17 | 14 | 0.2 | 0.33 |
| 20001006 | 1200 | 6 | 16.1 | 15.9 | 15.57 | 14.17 | 14 | 0.2 | 0.33 |
| 20001006 | 1215 | 6 | 16.1 | 15.91 | 15.57 | 14.16 | 14 | 0.19 | 0.34 |
| 20001006 | 1230 | 6 | 16.1 | 15.91 | 15.57 | 14.16 | 14 | 0.19 | 0.34 |
| 20001006 | 1245 | 6 | 16.1 | 15.91 | 15.57 | 14.16 | 14 | 0.19 | 0.34 |
| 20001006 | 1300 | 6 | 16.1 | 15.91 | 15.57 | 14.16 | 14 | 0.19 | 0.34 |
| 20001006 | 1315 | 6 | 16.1 | 15.91 | 15.58 | 14.16 | 14 | 0.19 | 0.33 |
| 20001006 | 1330 | 6 | 16.1 | 15.91 | 15.58 | 14.16 | 14 | 0.19 | 0.33 |
| 20001006 | 1345 | 6 | 16.1 | 15.91 | 15.58 | 14.16 | 14 | 0.19 | 0.33 |
| 20001006 | 1400 | 6 | 16.07 | 15.9 | 15.58 | 14.16 | 14 | 0.17 | 0.32 |
| 20001006 | 1415 | 6 | 16.06 | 15.89 | 15.58 | 14.16 | 14 | 0.17 | 0.31 |
| 20001006 | 1430 | 6 | 16.01 | 15.88 | 15.58 | 14.16 | 14 | 0.13 | 0.3 |
| 20001006 | 1445 | 6 | 16.02 | 15.88 | 15.58 | 14.16 | 14 | 0.14 | 0.3 |
| 20001006 | 1500 | 6 | 16.06 | 15.88 | 15.58 | 14.16 | 14 | 0.18 | 0.3 |
| 20001006 | 1515 | 6 | 16.05 | 15.88 | 15.58 | 14.15 | 14 | 0.17 | 0.3 |
| 20001006 | 1530 | 6 | 16.06 | 15.88 | 15.57 | 14.15 | 14 | 0.18 | 0.31 |
| 20001006 | 1545 | 6 | 16.06 | 15.89 | 15.57 | 14.15 | 14 | 0.17 | 0.32 |
| 20001006 | 1600 | 6 | 16.06 | 15.89 | 15.57 | 14.15 | 14 | 0.17 | 0.32 |
| 20001006 | 1615 | 6 | 16.07 | 15.89 | 15.58 | 14.16 | 14 | 0.18 | 0.31 |
| 20001006 | 1630 | 6 | 16.06 | 15.89 | 15.57 | 14.16 | 14 | 0.17 | 0.32 |
| 20001006 | 1645 | 6 | 16.07 | 15.89 | 15.57 | 14.16 | 14 | 0.18 | 0.32 |
| 20001006 | 1700 | 6 | 16.05 | 15.89 | 15.57 | 14.16 | 14 | 0.16 | 0.32 |
| 20001006 | 1715 | 6 | 16.05 | 15.89 | 15.57 | 14.16 | 14 | 0.16 | 0.32 |
| 20001006 | 1730 | 6 | 16.06 | 15.89 | 15.57 | 14.16 | 14 | 0.17 | 0.32 |
| 20001006 | 1745 | 6 | 16.11 | 15.93 | 15.58 | 14.19 | 14 | 0.18 | 0.35 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001006 | 1800 | 6 | 16.15 | 15.96 | 15.61 | 14.24 | 14 | 0.19 | 0.35 |
| 20001006 | 1815 | 6 | 16.13 | 15.96 | 15.62 | 14.25 | 14 | 0.17 | 0.34 |
| 20001006 | 1830 | 6 | 16.13 | 15.96 | 15.62 | 14.25 | 14 | 0.17 | 0.34 |
| 20001006 | 1845 | 6 | 16.13 | 15.96 | 15.63 | 14.25 | 14 | 0.17 | 0.33 |
| 20001006 | 1900 | 6 | 16.12 | 15.96 | 15.63 | 14.25 | 14 | 0.16 | 0.33 |
| 20001006 | 1915 | 6 | 16.13 | 15.96 | 15.63 | 14.24 | 14 | 0.17 | 0.33 |
| 20001006 | 1930 | 6 | 16.12 | 15.96 | 15.63 | 14.24 | 14 | 0.16 | 0.33 |
| 20001006 | 1945 | 6 | 16.12 | 15.96 | 15.63 | 14.24 | 14 | 0.16 | 0.33 |
| 20001006 | 2000 | 6 | 16.12 | 15.96 | 15.63 | 14.24 | 14 | 0.16 | 0.33 |
| 20001006 | 2015 | 6 | 16.12 | 15.96 | 15.63 | 14.24 | 14 | 0.16 | 0.33 |
| 20001006 | 2030 | 6 | 16.12 | 15.96 | 15.63 | 14.24 | 14 | 0.16 | 0.33 |
| 20001006 | 2045 | 6 | 16.12 | 15.96 | 15.63 | 14.24 | 14 | 0.16 | 0.33 |
| 20001006 | 2100 | 6 | 16.12 | 15.96 | 15.63 | 14.24 | 14 | 0.16 | 0.33 |
| 20001006 | 2115 | 6 | 16.12 | 15.96 | 15.63 | 14.24 | 14 | 0.16 | 0.33 |
| 20001006 | 2130 | 6 | 16.12 | 15.96 | 15.63 | 14.24 | 14 | 0.16 | 0.33 |
| 20001006 | 2145 | 6 | 16.12 | 15.96 | 15.63 | 14.24 | 14 | 0.16 | 0.33 |
| 20001006 | 2200 | 6 | 16.12 | 15.96 | 15.63 | 14.24 | 14 | 0.16 | 0.33 |
| 20001006 | 2215 | 6 | 16.12 | 15.96 | 15.63 | 14.24 | 14 | 0.16 | 0.33 |
| 20001006 | 2230 | 6 | 16.12 | 15.96 | 15.63 | 14.23 | 14 | 0.16 | 0.33 |
| 20001006 | 2245 | 6 | 16.12 | 15.96 | 15.63 | 14.23 | 14 | 0.16 | 0.33 |
| 20001006 | 2300 | 6 | 16.12 | 15.96 | 15.63 | 14.23 | 14 | 0.16 | 0.33 |
| 20001006 | 2315 | 6 | 16.12 | 15.96 | 15.63 | 14.23 | 14 | 0.16 | 0.33 |
| 20001006 | 2330 | 6 | 16.12 | 15.96 | 15.63 | 14.23 | 14 | 0.16 | 0.33 |
| 20001006 | 2345 | 6 | 16.12 | 15.96 | 15.63 | 14.23 | 14 | 0.16 | 0.33 |
| 20001007 | 0 | 7 | 16.12 | 15.96 | 15.63 | 14.23 | 14 | 0.16 | 0.33 |
| 20001007 | 15 | 7 | 16.12 | 15.96 | 15.63 | 14.23 | 14 | 0.16 | 0.33 |
| 20001007 | 30 | 7 | 16.12 | 15.96 | 15.63 | 14.23 | 14 | 0.16 | 0.33 |
| 20001007 | 45 | 7 | 16.12 | 15.96 | 15.63 | 14.23 | 14 | 0.16 | 0.33 |
| 20001007 | 100 | 7 | 16.12 | 15.96 | 15.63 | 14.23 | 14 | 0.16 | 0.33 |
| 20001007 | 115 | 7 | 16.12 | 15.96 | 15.63 | 14.23 | 14 | 0.16 | 0.33 |
| 20001007 | 130 | 7 | 16.12 | 15.96 | 15.63 | 14.23 | 14 | 0.16 | 0.33 |
| 20001007 | 145 | 7 | 16.12 | 15.96 | 15.63 | 14.23 | 14 | 0.16 | 0.33 |
| 20001007 | 200 | 7 | 16.12 | 15.96 | 15.63 | 14.22 | 14 | 0.16 | 0.33 |
| 20001007 | 215 | 7 | 16.11 | 15.96 | 15.63 | 14.22 | 14 | 0.15 | 0.33 |
| 20001007 | 230 | 7 | 16.12 | 15.96 | 15.63 | 14.22 | 14 | 0.16 | 0.33 |
| 20001007 | 245 | 7 | 16.11 | 15.96 | 15.63 | 14.22 | 14 | 0.15 | 0.33 |
| 20001007 | 300 | 7 | 16.12 | 15.96 | 15.63 | 14.22 | 14 | 0.16 | 0.33 |
| 20001007 | 315 | 7 | 16.11 | 15.96 | 15.63 | 14.22 | 14 | 0.15 | 0.33 |
| 20001007 | 330 | 7 | 16.11 | 15.96 | 15.63 | 14.22 | 14 | 0.15 | 0.33 |
| 20001007 | 345 | 7 | 16.11 | 15.96 | 15.63 | 14.22 | 14 | 0.15 | 0.33 |
| 20001007 | 400 | 7 | 16.11 | 15.96 | 15.63 | 14.22 | 14 | 0.15 | 0.33 |
| 20001007 | 415 | 7 | 16.12 | 15.96 | 15.63 | 14.22 | 14 | 0.16 | 0.33 |
| 20001007 | 430 | 7 | 16.12 | 15.96 | 15.63 | 14.22 | 14 | 0.16 | 0.33 |
| 20001007 | 445 | 7 | 16.12 | 15.96 | 15.63 | 14.22 | 14 | 0.16 | 0.33 |
| 20001007 | 500 | 7 | 16.11 | 15.96 | 15.63 | 14.22 | 14 | 0.15 | 0.33 |
| 20001007 | 515 | 7 | 16.12 | 15.96 | 15.63 | 14.22 | 14 | 0.16 | 0.33 |
| 20001007 | 530 | 7 | 16.11 | 15.96 | 15.63 | 14.22 | 14 | 0.15 | 0.33 |
| 20001007 | 545 | 7 | 16.11 | 15.96 | 15.63 | 14.22 | 14 | 0.15 | 0.33 |
| 20001007 | 600 | 7 | 16.11 | 15.96 | 15.63 | 14.22 | 14 | 0.15 | 0.33 |
| 20001007 | 615 | 7 | 16.11 | 15.96 | 15.63 | 14.21 | 14 | 0.15 | 0.33 |
| 20001007 | 630 | 7 | 16.11 | 15.96 | 15.63 | 14.21 | 14 | 0.15 | 0.33 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001007 | 645 | 7 | 16.11 | 15.96 | 15.63 | 14.21 | 14 | 0.15 | 0.33 |
| 20001007 | 700 | 7 | 16.11 | 15.96 | 15.63 | 14.21 | 14 | 0.15 | 0.33 |
| 20001007 | 715 | 7 | 16.11 | 15.96 | 15.63 | 14.21 | 14 | 0.15 | 0.33 |
| 20001007 | 730 | 7 | 16.12 | 15.96 | 15.63 | 14.21 | 14 | 0.16 | 0.33 |
| 20001007 | 745 | 7 | 16.12 | 15.96 | 15.63 | 14.21 | 14 | 0.16 | 0.33 |
| 20001007 | 800 | 7 | 16.12 | 15.96 | 15.63 | 14.21 | 14 | 0.16 | 0.33 |
| 20001007 | 815 | 7 | 16.12 | 15.96 | 15.63 | 14.21 | 14 | 0.16 | 0.33 |
| 20001007 | 830 | 7 | 16.12 | 15.96 | 15.63 | 14.21 | 14 | 0.16 | 0.33 |
| 20001007 | 845 | 7 | 16.12 | 15.96 | 15.63 | 14.21 | 14 | 0.16 | 0.33 |
| 20001007 | 900 | 7 | 16.12 | 15.96 | 15.63 | 14.21 | 14 | 0.16 | 0.33 |
| 20001007 | 915 | 7 | 16.11 | 15.96 | 15.63 | 14.21 | 14 | 0.15 | 0.33 |
| 20001007 | 930 | 7 | 16.12 | 15.96 | 15.63 | 14.21 | 14 | 0.16 | 0.33 |
| 20001007 | 945 | 7 | 16.12 | 15.96 | 15.63 | 14.21 | 14 | 0.16 | 0.33 |
| 20001007 | 1000 | 7 | 16.1 | 15.96 | 15.63 | 14.2 | 14 | 0.14 | 0.33 |
| 20001007 | 1015 | 7 | 16.12 | 15.96 | 15.63 | 14.2 | 14 | 0.16 | 0.33 |
| 20001007 | 1030 | 7 | 16.12 | 15.96 | 15.63 | 14.2 | 14 | 0.16 | 0.33 |
| 20001007 | 1045 | 7 | 16.12 | 15.96 | 15.63 | 14.2 | 14 | 0.16 | 0.33 |
| 20001007 | 1100 | 7 | 16.12 | 15.96 | 15.63 | 14.2 | 14 | 0.16 | 0.33 |
| 20001007 | 1115 | 7 | 16.13 | 15.96 | 15.63 | 14.19 | 14 | 0.17 | 0.33 |
| 20001007 | 1130 | 7 | 16.13 | 15.96 | 15.63 | 14.19 | 14 | 0.17 | 0.33 |
| 20001007 | 1145 | 7 | 16.13 | 15.96 | 15.63 | 14.19 | 14 | 0.17 | 0.33 |
| 20001007 | 1200 | 7 | 16.13 | 15.97 | 15.63 | 14.19 | 14 | 0.16 | 0.34 |
| 20001007 | 1215 | 7 | 16.13 | 15.97 | 15.63 | 14.19 | 14 | 0.16 | 0.34 |
| 20001007 | 1230 | 7 | 16.13 | 15.97 | 15.63 | 14.19 | 14 | 0.16 | 0.34 |
| 20001007 | 1245 | 7 | 16.13 | 15.97 | 15.63 | 14.18 | 14 | 0.16 | 0.34 |
| 20001007 | 1300 | 7 | 16.13 | 15.97 | 15.62 | 14.18 | 14 | 0.16 | 0.35 |
| 20001007 | 1315 | 7 | 16.13 | 15.97 | 15.62 | 14.18 | 14 | 0.16 | 0.35 |
| 20001007 | 1330 | 7 | 16.13 | 15.97 | 15.62 | 14.18 | 14 | 0.16 | 0.35 |
| 20001007 | 1345 | 7 | 16.13 | 15.97 | 15.62 | 14.18 | 14 | 0.16 | 0.35 |
| 20001007 | 1400 | 7 | 16.13 | 15.97 | 15.62 | 14.18 | 14 | 0.16 | 0.35 |
| 20001007 | 1415 | 7 | 16.13 | 15.97 | 15.62 | 14.18 | 14 | 0.16 | 0.35 |
| 20001007 | 1430 | 7 | 16.13 | 15.97 | 15.62 | 14.17 | 14 | 0.16 | 0.35 |
| 20001007 | 1445 | 7 | 16.13 | 15.97 | 15.62 | 14.17 | 14 | 0.16 | 0.35 |
| 20001007 | 1500 | 7 | 16.13 | 15.97 | 15.62 | 14.17 | 14 | 0.16 | 0.35 |
| 20001007 | 1515 | 7 | 16.13 | 15.97 | 15.62 | 14.17 | 14 | 0.16 | 0.35 |
| 20001007 | 1530 | 7 | 16.13 | 15.97 | 15.62 | 14.17 | 14 | 0.16 | 0.35 |
| 20001007 | 1545 | 7 | 16.13 | 15.97 | 15.62 | 14.17 | 14 | 0.16 | 0.35 |
| 20001007 | 1600 | 7 | 16.13 | 15.97 | 15.62 | 14.17 | 14 | 0.16 | 0.35 |
| 20001007 | 1615 | 7 | 16.13 | 15.97 | 15.62 | 14.17 | 14 | 0.16 | 0.35 |
| 20001007 | 1630 | 7 | 16.13 | 15.97 | 15.62 | 14.17 | 14 | 0.16 | 0.35 |
| 20001007 | 1645 | 7 | 16.13 | 15.96 | 15.62 | 14.17 | 14 | 0.17 | 0.34 |
| 20001007 | 1700 | 7 | 16.13 | 15.96 | 15.62 | 14.17 | 14 | 0.17 | 0.34 |
| 20001007 | 1715 | 7 | 16.13 | 15.97 | 15.62 | 14.17 | 14 | 0.16 | 0.35 |
| 20001007 | 1730 | 7 | 16.11 | 15.96 | 15.62 | 14.17 | 14 | 0.15 | 0.34 |
| 20001007 | 1745 | 7 | 16.07 | 15.95 | 15.62 | 14.17 | 14 | 0.12 | 0.33 |
| 20001007 | 1800 | 7 | 16.06 | 15.94 | 15.62 | 14.17 | 14 | 0.12 | 0.32 |
| 20001007 | 1815 | 7 | 16.05 | 15.93 | 15.62 | 14.17 | 14 | 0.12 | 0.31 |
| 20001007 | 1830 | 7 | 16.03 | 15.92 | 15.62 | 14.17 | 14 | 0.11 | 0.3 |
| 20001007 | 1845 | 7 | 16.03 | 15.92 | 15.62 | 14.17 | 14 | 0.11 | 0.3 |
| 20001007 | 1900 | 7 | 16.02 | 15.91 | 15.62 | 14.17 | 14 | 0.11 | 0.29 |
| 20001007 | 1915 | 7 | 16.01 | 15.91 | 15.62 | 14.17 | 14 | 0.1 | 0.29 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001007 | 1930 | 7 | 16 | 15.9 | 15.62 | 14.17 | 14 | 0.1 | 0.28 |
| 20001007 | 1945 | 7 | 16 | 15.9 | 15.61 | 14.17 | 14 | 0.1 | 0.29 |
| 20001007 | 2000 | 7 | 15.99 | 15.9 | 15.61 | 14.17 | 14 | 0.09 | 0.29 |
| 20001007 | 2015 | 7 | 15.99 | 15.89 | 15.61 | 14.17 | 14 | 0.1 | 0.28 |
| 20001007 | 2030 | 7 | 15.99 | 15.89 | 15.61 | 14.17 | 14 | 0.1 | 0.28 |
| 20001007 | 2045 | 7 | 15.98 | 15.89 | 15.6 | 14.17 | 14 | 0.09 | 0.29 |
| 20001007 | 2100 | 7 | 15.98 | 15.88 | 15.6 | 14.17 | 14 | 0.1 | 0.28 |
| 20001007 | 2115 | 7 | 15.98 | 15.88 | 15.6 | 14.17 | 14 | 0.1 | 0.28 |
| 20001007 | 2130 | 7 | 15.98 | 15.88 | 15.6 | 14.17 | 14 | 0.1 | 0.28 |
| 20001007 | 2145 | 7 | 15.97 | 15.88 | 15.59 | 14.17 | 14 | 0.09 | 0.29 |
| 20001007 | 2200 | 7 | 15.97 | 15.87 | 15.59 | 14.17 | 14 | 0.1 | 0.28 |
| 20001007 | 2215 | 7 | 15.97 | 15.87 | 15.59 | 14.17 | 14 | 0.1 | 0.28 |
| 20001007 | 2230 | 7 | 15.97 | 15.87 | 15.59 | 14.17 | 14 | 0.1 | 0.28 |
| 20001007 | 2245 | 7 | 15.97 | 15.87 | 15.58 | 14.17 | 14 | 0.1 | 0.29 |
| 20001007 | 2300 | 7 | 15.97 | 15.86 | 15.58 | 14.17 | 14 | 0.11 | 0.28 |
| 20001007 | 2315 | 7 | 15.96 | 15.86 | 15.58 | 14.16 | 14 | 0.1 | 0.28 |
| 20001007 | 2330 | 7 | 15.96 | 15.86 | 15.57 | 14.16 | 14 | 0.1 | 0.29 |
| 20001007 | 2345 | 7 | 15.96 | 15.86 | 15.57 | 14.16 | 14 | 0.1 | 0.29 |
| 20001008 | 0 | 8 | 15.96 | 15.85 | 15.57 | 14.16 | 14 | 0.11 | 0.28 |
| 20001008 | 15 | 8 | 15.96 | 15.85 | 15.57 | 14.16 | 14 | 0.11 | 0.28 |
| 20001008 | 30 | 8 | 15.96 | 15.85 | 15.56 | 14.16 | 14 | 0.11 | 0.29 |
| 20001008 | 45 | 8 | 15.96 | 15.85 | 15.56 | 14.16 | 14 | 0.11 | 0.29 |
| 20001008 | 100 | 8 | 15.96 | 15.84 | 15.56 | 14.15 | 14 | 0.12 | 0.28 |
| 20001008 | 115 | 8 | 15.96 | 15.84 | 15.56 | 14.15 | 14 | 0.12 | 0.28 |
| 20001008 | 130 | 8 | 15.95 | 15.84 | 15.55 | 14.15 | 14 | 0.11 | 0.29 |
| 20001008 | 145 | 8 | 15.95 | 15.84 | 15.55 | 14.15 | 14 | 0.11 | 0.29 |
| 20001008 | 200 | 8 | 15.95 | 15.84 | 15.55 | 14.15 | 14 | 0.11 | 0.29 |
| 20001008 | 215 | 8 | 15.95 | 15.83 | 15.54 | 14.14 | 14 | 0.12 | 0.29 |
| 20001008 | 230 | 8 | 15.95 | 15.83 | 15.54 | 14.14 | 14 | 0.12 | 0.29 |
| 20001008 | 245 | 8 | 15.95 | 15.83 | 15.54 | 14.14 | 14 | 0.12 | 0.29 |
| 20001008 | 300 | 8 | 15.95 | 15.83 | 15.54 | 14.14 | 14 | 0.12 | 0.29 |
| 20001008 | 315 | 8 | 15.95 | 15.83 | 15.53 | 14.14 | 14 | 0.12 | 0.3 |
| 20001008 | 330 | 8 | 15.95 | 15.82 | 15.53 | 14.14 | 14 | 0.13 | 0.29 |
| 20001008 | 345 | 8 | 15.95 | 15.82 | 15.53 | 14.13 | 14 | 0.13 | 0.29 |
| 20001008 | 400 | 8 | 15.95 | 15.82 | 15.53 | 14.13 | 14 | 0.13 | 0.29 |
| 20001008 | 415 | 8 | 15.94 | 15.82 | 15.53 | 14.13 | 14 | 0.12 | 0.29 |
| 20001008 | 430 | 8 | 15.94 | 15.82 | 15.52 | 14.13 | 14 | 0.12 | 0.3 |
| 20001008 | 445 | 8 | 15.94 | 15.82 | 15.52 | 14.13 | 14 | 0.12 | 0.3 |
| 20001008 | 500 | 8 | 15.94 | 15.81 | 15.52 | 14.13 | 14 | 0.13 | 0.29 |
| 20001008 | 515 | 8 | 15.94 | 15.81 | 15.52 | 14.13 | 14 | 0.13 | 0.29 |
| 20001008 | 530 | 8 | 15.94 | 15.81 | 15.51 | 14.12 | 14 | 0.13 | 0.3 |
| 20001008 | 545 | 8 | 15.94 | 15.81 | 15.51 | 14.12 | 14 | 0.13 | 0.3 |
| 20001008 | 600 | 8 | 15.94 | 15.81 | 15.51 | 14.12 | 14 | 0.13 | 0.3 |
| 20001008 | 615 | 8 | 15.94 | 15.81 | 15.51 | 14.12 | 14 | 0.13 | 0.3 |
| 20001008 | 630 | 8 | 15.94 | 15.81 | 15.5 | 14.12 | 14 | 0.13 | 0.31 |
| 20001008 | 645 | 8 | 15.94 | 15.8 | 15.5 | 14.12 | 14 | 0.14 | 0.3 |
| 20001008 | 700 | 8 | 15.94 | 15.8 | 15.5 | 14.12 | 14 | 0.14 | 0.3 |
| 20001008 | 715 | 8 | 15.94 | 15.8 | 15.5 | 14.11 | 14 | 0.14 | 0.3 |
| 20001008 | 730 | 8 | 15.94 | 15.8 | 15.5 | 14.11 | 14 | 0.14 | 0.3 |
| 20001008 | 745 | 8 | 15.94 | 15.8 | 15.49 | 14.11 | 14 | 0.14 | 0.31 |
| 20001008 | 800 | 8 | 15.94 | 15.8 | 15.49 | 14.11 | 14 | 0.14 | 0.31 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001008 | 815 | 8 | 15.94 | 15.8 | 15.49 | 14.1 | 14 | 0.14 | 0.31 |
| 20001008 | 830 | 8 | 15.94 | 15.79 | 15.49 | 14.1 | 14 | 0.15 | 0.3 |
| 20001008 | 845 | 8 | 15.94 | 15.79 | 15.49 | 14.1 | 14 | 0.15 | 0.3 |
| 20001008 | 900 | 8 | 15.94 | 15.79 | 15.48 | 14.1 | 14 | 0.15 | 0.31 |
| 20001008 | 915 | 8 | 15.94 | 15.79 | 15.48 | 14.1 | 14 | 0.15 | 0.31 |
| 20001008 | 930 | 8 | 15.92 | 15.78 | 15.48 | 14.09 | 14 | 0.14 | 0.3 |
| 20001008 | 945 | 8 | 15.93 | 15.79 | 15.48 | 14.09 | 14 | 0.14 | 0.31 |
| 20001008 | 1000 | 8 | 15.94 | 15.79 | 15.48 | 14.09 | 14 | 0.15 | 0.31 |
| 20001008 | 1015 | 8 | 15.94 | 15.79 | 15.48 | 14.09 | 14 | 0.15 | 0.31 |
| 20001008 | 1030 | 8 | 15.95 | 15.79 | 15.47 | 14.08 | 14 | 0.16 | 0.32 |
| 20001008 | 1045 | 8 | 15.95 | 15.79 | 15.47 | 14.08 | 14 | 0.16 | 0.32 |
| 20001008 | 1100 | 8 | 15.95 | 15.79 | 15.47 | 14.08 | 14 | 0.16 | 0.32 |
| 20001008 | 1115 | 8 | 15.95 | 15.79 | 15.47 | 14.08 | 14 | 0.16 | 0.32 |
| 20001008 | 1130 | 8 | 15.99 | 15.79 | 15.47 | 14.07 | 14 | 0.2 | 0.32 |
| 20001008 | 1145 | 8 | 16.02 | 15.8 | 15.46 | 14.07 | 14 | 0.22 | 0.34 |
| 20001008 | 1200 | 8 | 16.03 | 15.81 | 15.46 | 14.07 | 14 | 0.22 | 0.35 |
| 20001008 | 1215 | 8 | 16.05 | 15.81 | 15.46 | 14.06 | 14 | 0.24 | 0.35 |
| 20001008 | 1230 | 8 | 16.06 | 15.82 | 15.46 | 14.06 | 14 | 0.24 | 0.36 |
| 20001008 | 1245 | 8 | 16.07 | 15.83 | 15.46 | 14.05 | 14 | 0.24 | 0.37 |
| 20001008 | 1300 | 8 | 16.08 | 15.83 | 15.46 | 14.05 | 14 | 0.25 | 0.37 |
| 20001008 | 1315 | 8 | 16.09 | 15.84 | 15.46 | 14.05 | 14 | 0.25 | 0.38 |
| 20001008 | 1330 | 8 | 16.09 | 15.84 | 15.46 | 14.04 | 14 | 0.25 | 0.38 |
| 20001008 | 1345 | 8 | 16.1 | 15.84 | 15.46 | 14.04 | 14 | 0.26 | 0.38 |
| 20001008 | 1400 | 8 | 16.1 | 15.84 | 15.46 | 14.04 | 14 | 0.26 | 0.38 |
| 20001008 | 1415 | 8 | 16.11 | 15.85 | 15.46 | 14.03 | 14 | 0.26 | 0.39 |
| 20001008 | 1430 | 8 | 16.07 | 15.84 | 15.46 | 14.03 | 14 | 0.23 | 0.38 |
| 20001008 | 1445 | 8 | 16.06 | 15.83 | 15.46 | 14.03 | 14 | 0.23 | 0.37 |
| 20001008 | 1500 | 8 | 16.04 | 15.83 | 15.46 | 14.03 | 14 | 0.21 | 0.37 |
| 20001008 | 1515 | 8 | 16.03 | 15.82 | 15.46 | 14.03 | 14 | 0.21 | 0.36 |
| 20001008 | 1530 | 8 | 16.02 | 15.82 | 15.46 | 14.02 | 14 | 0.2 | 0.36 |
| 20001008 | 1545 | 8 | 16.01 | 15.82 | 15.46 | 14.02 | 14 | 0.19 | 0.36 |
| 20001008 | 1600 | 8 | 16 | 15.81 | 15.46 | 14.02 | 14 | 0.19 | 0.35 |
| 20001008 | 1615 | 8 | 15.99 | 15.81 | 15.46 | 14.02 | 14 | 0.18 | 0.35 |
| 20001008 | 1630 | 8 | 15.99 | 15.81 | 15.47 | 14.02 | 14 | 0.18 | 0.34 |
| 20001008 | 1645 | 8 | 15.98 | 15.81 | 15.46 | 14.02 | 14 | 0.17 | 0.35 |
| 20001008 | 1700 | 8 | 15.98 | 15.8 | 15.46 | 14.02 | 14 | 0.18 | 0.34 |
| 20001008 | 1715 | 8 | 15.97 | 15.8 | 15.46 | 14.02 | 14 | 0.17 | 0.34 |
| 20001008 | 1730 | 8 | 15.97 | 15.8 | 15.46 | 14.02 | 14 | 0.17 | 0.34 |
| 20001008 | 1745 | 8 | 15.96 | 15.79 | 15.46 | 14.02 | 14 | 0.17 | 0.33 |
| 20001008 | 1800 | 8 | 15.95 | 15.79 | 15.46 | 14.02 | 14 | 0.16 | 0.33 |
| 20001008 | 1815 | 8 | 15.95 | 15.79 | 15.46 | 14.01 | 14 | 0.16 | 0.33 |
| 20001008 | 1830 | 8 | 15.95 | 15.79 | 15.46 | 14.02 | 14 | 0.16 | 0.33 |
| 20001008 | 1845 | 8 | 15.94 | 15.78 | 15.46 | 14.01 | 14 | 0.16 | 0.32 |
| 20001008 | 1900 | 8 | 15.94 | 15.78 | 15.46 | 14.01 | 14 | 0.16 | 0.32 |
| 20001008 | 1915 | 8 | 15.94 | 15.78 | 15.46 | 14.01 | 14 | 0.16 | 0.32 |
| 20001008 | 1930 | 8 | 15.94 | 15.78 | 15.46 | 14.01 | 14 | 0.16 | 0.32 |
| 20001008 | 1945 | 8 | 15.94 | 15.78 | 15.45 | 14.01 | 14 | 0.16 | 0.33 |
| 20001008 | 2000 | 8 | 15.94 | 15.78 | 15.45 | 14.01 | 14 | 0.16 | 0.33 |
| 20001008 | 2015 | 8 | 15.94 | 15.78 | 15.45 | 14.01 | 14 | 0.16 | 0.33 |
| 20001008 | 2030 | 8 | 15.93 | 15.77 | 15.45 | 14.01 | 14 | 0.16 | 0.32 |
| 20001008 | 2045 | 8 | 15.93 | 15.77 | 15.45 | 14.01 | 14 | 0.16 | 0.32 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001008 | 2100 | 8 | 15.93 | 15.77 | 15.45 | 14.01 | 14 | 0.16 | 0.32 |
| 20001008 | 2115 | 8 | 15.93 | 15.77 | 15.44 | 14.01 | 14 | 0.16 | 0.33 |
| 20001008 | 2130 | 8 | 15.93 | 15.77 | 15.44 | 14.01 | 14 | 0.16 | 0.33 |
| 20001008 | 2145 | 8 | 15.93 | 15.77 | 15.44 | 14.01 | 14 | 0.16 | 0.33 |
| 20001008 | 2200 | 8 | 15.93 | 15.77 | 15.44 | 14.01 | 14 | 0.16 | 0.33 |
| 20001008 | 2215 | 8 | 15.93 | 15.76 | 15.44 | 14.01 | 14 | 0.17 | 0.32 |
| 20001008 | 2230 | 8 | 15.93 | 15.76 | 15.44 | 14.01 | 14 | 0.17 | 0.32 |
| 20001008 | 2245 | 8 | 15.93 | 15.76 | 15.44 | 14.01 | 14 | 0.17 | 0.32 |
| 20001008 | 2300 | 8 | 15.93 | 15.76 | 15.43 | 14.01 | 14 | 0.17 | 0.33 |
| 20001008 | 2315 | 8 | 15.93 | 15.76 | 15.43 | 14.01 | 14 | 0.17 | 0.33 |
| 20001008 | 2330 | 8 | 15.93 | 15.76 | 15.43 | 14.01 | 14 | 0.17 | 0.33 |
| 20001008 | 2345 | 8 | 15.93 | 15.76 | 15.43 | 14 | 14 | 0.17 | 0.33 |
| 20001009 | 0 | 9 | 15.93 | 15.76 | 15.43 | 14 | 14 | 0.17 | 0.33 |
| 20001009 | 15 | 9 | 15.93 | 15.76 | 15.43 | 14 | 14 | 0.17 | 0.33 |
| 20001009 | 30 | 9 | 15.93 | 15.75 | 15.42 | 14 | 14 | 0.18 | 0.33 |
| 20001009 | 45 | 9 | 15.93 | 15.75 | 15.42 | 14 | 14 | 0.18 | 0.33 |
| 20001009 | 100 | 9 | 15.92 | 15.75 | 15.42 | 14 | 14 | 0.17 | 0.33 |
| 20001009 | 115 | 9 | 15.92 | 15.75 | 15.42 | 14 | 14 | 0.17 | 0.33 |
| 20001009 | 130 | 9 | 15.92 | 15.75 | 15.42 | 14 | 14 | 0.17 | 0.33 |
| 20001009 | 145 | 9 | 15.92 | 15.75 | 15.42 | 14 | 14 | 0.17 | 0.33 |
| 20001009 | 200 | 9 | 15.92 | 15.75 | 15.41 | 14 | 14 | 0.17 | 0.34 |
| 20001009 | 215 | 9 | 15.92 | 15.75 | 15.41 | 14 | 14 | 0.17 | 0.34 |
| 20001009 | 230 | 9 | 15.92 | 15.75 | 15.41 | 13.99 | 14 | 0.17 | 0.34 |
| 20001009 | 245 | 9 | 15.92 | 15.75 | 15.41 | 13.99 | 14 | 0.17 | 0.34 |
| 20001009 | 300 | 9 | 15.92 | 15.75 | 15.41 | 13.99 | 14 | 0.17 | 0.34 |
| 20001009 | 315 | 9 | 15.92 | 15.74 | 15.41 | 13.99 | 14 | 0.18 | 0.33 |
| 20001009 | 330 | 9 | 15.92 | 15.74 | 15.41 | 13.99 | 14 | 0.18 | 0.33 |
| 20001009 | 345 | 9 | 15.92 | 15.74 | 15.41 | 13.99 | 14 | 0.18 | 0.33 |
| 20001009 | 400 | 9 | 15.92 | 15.74 | 15.4 | 13.99 | 14 | 0.18 | 0.34 |
| 20001009 | 415 | 9 | 15.92 | 15.74 | 15.4 | 13.99 | 14 | 0.18 | 0.34 |
| 20001009 | 430 | 9 | 15.92 | 15.74 | 15.4 | 13.99 | 14 | 0.18 | 0.34 |
| 20001009 | 445 | 9 | 15.92 | 15.74 | 15.4 | 13.99 | 14 | 0.18 | 0.34 |
| 20001009 | 500 | 9 | 15.92 | 15.74 | 15.4 | 13.99 | 14 | 0.18 | 0.34 |
| 20001009 | 515 | 9 | 15.92 | 15.74 | 15.39 | 13.98 | 14 | 0.18 | 0.35 |
| 20001009 | 530 | 9 | 15.92 | 15.74 | 15.39 | 13.98 | 14 | 0.18 | 0.35 |
| 20001009 | 545 | 9 | 15.92 | 15.74 | 15.39 | 13.98 | 14 | 0.18 | 0.35 |
| 20001009 | 600 | 9 | 15.92 | 15.74 | 15.39 | 13.97 | 14 | 0.18 | 0.35 |
| 20001009 | 615 | 9 | 15.92 | 15.74 | 15.39 | 13.97 | 14 | 0.18 | 0.35 |
| 20001009 | 630 | 9 | 15.92 | 15.74 | 15.39 | 13.97 | 14 | 0.18 | 0.35 |
| 20001009 | 645 | 9 | 15.92 | 15.73 | 15.39 | 13.97 | 14 | 0.19 | 0.34 |
| 20001009 | 700 | 9 | 15.92 | 15.73 | 15.38 | 13.96 | 14 | 0.19 | 0.35 |
| 20001009 | 715 | 9 | 15.92 | 15.73 | 15.38 | 13.96 | 14 | 0.19 | 0.35 |
| 20001009 | 730 | 9 | 15.92 | 15.73 | 15.38 | 13.96 | 14 | 0.19 | 0.35 |
| 20001009 | 745 | 9 | 15.92 | 15.73 | 15.38 | 13.96 | 14 | 0.19 | 0.35 |
| 20001009 | 800 | 9 | 15.92 | 15.73 | 15.38 | 13.96 | 14 | 0.19 | 0.35 |
| 20001009 | 815 | 9 | 15.92 | 15.73 | 15.38 | 13.96 | 14 | 0.19 | 0.35 |
| 20001009 | 830 | 9 | 15.92 | 15.73 | 15.38 | 13.96 | 14 | 0.19 | 0.35 |
| 20001009 | 845 | 9 | 15.92 | 15.73 | 15.38 | 13.96 | 14 | 0.19 | 0.35 |
| 20001009 | 900 | 9 | 15.92 | 15.73 | 15.37 | 13.96 | 14 | 0.19 | 0.36 |
| 20001009 | 915 | 9 | 15.92 | 15.73 | 15.37 | 13.96 | 14 | 0.19 | 0.36 |
| 20001009 | 930 | 9 | 15.92 | 15.73 | 15.37 | 13.95 | 14 | 0.19 | 0.36 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001009 | 945 | 9 | 15.92 | 15.72 | 15.37 | 13.95 | 14 | 0.2 | 0.35 |
| 20001009 | 1000 | 9 | 15.9 | 15.72 | 15.37 | 13.95 | 14 | 0.18 | 0.35 |
| 20001009 | 1015 | 9 | 15.79 | 15.7 | 15.37 | 13.95 | 14 | 0.09 | 0.33 |
| 20001009 | 1030 | 9 | 15.74 | 15.67 | 15.37 | 13.95 | 14 | 0.07 | 0.3 |
| 20001009 | 1045 | 9 | 15.81 | 15.68 | 15.36 | 13.95 | 14 | 0.13 | 0.32 |
| 20001009 | 1100 | 9 | 15.88 | 15.7 | 15.36 | 13.94 | 14 | 0.18 | 0.34 |
| 20001009 | 1115 | 9 | 15.88 | 15.7 | 15.36 | 13.94 | 14 | 0.18 | 0.34 |
| 20001009 | 1130 | 9 | 15.92 | 15.71 | 15.36 | 13.94 | 14 | 0.21 | 0.35 |
| 20001009 | 1145 | 9 | 15.93 | 15.72 | 15.35 | 13.93 | 14 | 0.21 | 0.37 |
| 20001009 | 1200 | 9 | 15.94 | 15.72 | 15.35 | 13.93 | 14 | 0.22 | 0.37 |
| 20001009 | 1215 | 9 | 15.96 | 15.73 | 15.35 | 13.93 | 14 | 0.23 | 0.38 |
| 20001009 | 1230 | 9 | 15.97 | 15.73 | 15.35 | 13.93 | 14 | 0.24 | 0.38 |
| 20001009 | 1245 | 9 | 15.98 | 15.73 | 15.35 | 13.93 | 14 | 0.25 | 0.38 |
| 20001009 | 1300 | 9 | 15.99 | 15.74 | 15.35 | 13.93 | 14 | 0.25 | 0.39 |
| 20001009 | 1315 | 9 | 15.99 | 15.74 | 15.35 | 13.93 | 14 | 0.25 | 0.39 |
| 20001009 | 1330 | 9 | 15.97 | 15.74 | 15.34 | 13.93 | 14 | 0.23 | 0.4 |
| 20001009 | 1345 | 9 | 15.97 | 15.74 | 15.34 | 13.92 | 14 | 0.23 | 0.4 |
| 20001009 | 1400 | 9 | 15.97 | 15.74 | 15.34 | 13.92 | 14 | 0.23 | 0.4 |
| 20001009 | 1415 | 9 | 15.97 | 15.74 | 15.34 | 13.95 | 14 | 0.23 | 0.4 |
| 20001009 | 1430 | 9 | 15.98 | 15.74 | 15.34 | 13.96 | 14 | 0.24 | 0.4 |
| 20001009 | 1445 | 9 | 16.01 | 15.75 | 15.34 | 13.97 | 14 | 0.26 | 0.41 |
| 20001009 | 1500 | 9 | 16.03 | 15.76 | 15.34 | 13.95 | 14 | 0.27 | 0.42 |
| 20001009 | 1515 | 9 | 16.04 | 15.76 | 15.34 | 13.95 | 14 | 0.28 | 0.42 |
| 20001009 | 1530 | 9 | 16.05 | 15.77 | 15.34 | 13.94 | 14 | 0.28 | 0.43 |
| 20001009 | 1545 | 9 | 16.06 | 15.77 | 15.34 | 13.94 | 14 | 0.29 | 0.43 |
| 20001009 | 1600 | 9 | 16.07 | 15.78 | 15.35 | 13.94 | 14 | 0.29 | 0.43 |
| 20001009 | 1615 | 9 | 16.07 | 15.78 | 15.35 | 13.93 | 14 | 0.29 | 0.43 |
| 20001009 | 1630 | 9 | 16.07 | 15.79 | 15.35 | 13.93 | 14 | 0.28 | 0.44 |
| 20001009 | 1645 | 9 | 16.08 | 15.79 | 15.35 | 13.93 | 14 | 0.29 | 0.44 |
| 20001009 | 1700 | 9 | 16.09 | 15.79 | 15.35 | 13.92 | 14 | 0.3 | 0.44 |
| 20001009 | 1715 | 9 | 16.09 | 15.79 | 15.35 | 13.92 | 14 | 0.3 | 0.44 |
| 20001009 | 1730 | 9 | 16.09 | 15.8 | 15.35 | 13.92 | 14 | 0.29 | 0.45 |
| 20001009 | 1745 | 9 | 16.09 | 15.8 | 15.35 | 13.91 | 14 | 0.29 | 0.45 |
| 20001009 | 1800 | 9 | 16.08 | 15.8 | 15.36 | 13.92 | 14 | 0.28 | 0.44 |
| 20001009 | 1815 | 9 | 16.09 | 15.8 | 15.36 | 13.92 | 14 | 0.29 | 0.44 |
| 20001009 | 1830 | 9 | 16.09 | 15.8 | 15.36 | 13.92 | 14 | 0.29 | 0.44 |
| 20001009 | 1845 | 9 | 16.09 | 15.8 | 15.36 | 13.92 | 14 | 0.29 | 0.44 |
| 20001009 | 1900 | 9 | 16.09 | 15.8 | 15.37 | 13.92 | 14 | 0.29 | 0.43 |
| 20001009 | 1915 | 9 | 16.09 | 15.8 | 15.37 | 13.91 | 14 | 0.29 | 0.43 |
| 20001009 | 1930 | 9 | 16.09 | 15.81 | 15.37 | 13.92 | 14 | 0.28 | 0.44 |
| 20001009 | 1945 | 9 | 16.09 | 15.81 | 15.37 | 13.92 | 14 | 0.28 | 0.44 |
| 20001009 | 2000 | 9 | 16.09 | 15.81 | 15.37 | 13.92 | 14 | 0.28 | 0.44 |
| 20001009 | 2015 | 9 | 16.09 | 15.81 | 15.38 | 13.92 | 14 | 0.28 | 0.43 |
| 20001009 | 2030 | 9 | 16.09 | 15.81 | 15.38 | 13.92 | 14 | 0.28 | 0.43 |
| 20001009 | 2045 | 9 | 16.09 | 15.81 | 15.38 | 13.92 | 14 | 0.28 | 0.43 |
| 20001009 | 2100 | 9 | 16.09 | 15.82 | 15.38 | 13.92 | 14 | 0.27 | 0.44 |
| 20001009 | 2115 | 9 | 16.1 | 15.82 | 15.39 | 13.92 | 14 | 0.28 | 0.43 |
| 20001009 | 2130 | 9 | 16.09 | 15.82 | 15.39 | 13.92 | 14 | 0.27 | 0.43 |
| 20001009 | 2145 | 9 | 16.09 | 15.82 | 15.39 | 13.92 | 14 | 0.27 | 0.43 |
| 20001009 | 2200 | 9 | 16.09 | 15.82 | 15.39 | 13.92 | 14 | 0.27 | 0.43 |
| 20001009 | 2215 | 9 | 16.09 | 15.82 | 15.39 | 13.92 | 14 | 0.27 | 0.43 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001009 | 2230 | 9 | 16.1 | 15.82 | 15.4 | 13.92 | 14 | 0.28 | 0.42 |
| 20001009 | 2245 | 9 | 16.09 | 15.83 | 15.4 | 13.92 | 14 | 0.26 | 0.43 |
| 20001009 | 2300 | 9 | 16.09 | 15.83 | 15.4 | 13.92 | 14 | 0.26 | 0.43 |
| 20001009 | 2315 | 9 | 16.09 | 15.83 | 15.4 | 13.92 | 14 | 0.26 | 0.43 |
| 20001009 | 2330 | 9 | 16.1 | 15.83 | 15.4 | 13.92 | 14 | 0.27 | 0.43 |
| 20001009 | 2345 | 9 | 16.1 | 15.83 | 15.41 | 13.92 | 14 | 0.27 | 0.42 |
| 20001010 | 0 | 10 | 16.1 | 15.83 | 15.41 | 13.93 | 14 | 0.27 | 0.42 |
| 20001010 | 15 | 10 | 16.1 | 15.83 | 15.41 | 13.93 | 14 | 0.27 | 0.42 |
| 20001010 | 30 | 10 | 16.1 | 15.83 | 15.41 | 13.93 | 14 | 0.27 | 0.42 |
| 20001010 | 45 | 10 | 16.1 | 15.84 | 15.41 | 13.93 | 14 | 0.26 | 0.43 |
| 20001010 | 100 | 10 | 16.1 | 15.84 | 15.41 | 13.93 | 14 | 0.26 | 0.43 |
| 20001010 | 115 | 10 | 16.1 | 15.84 | 15.42 | 13.93 | 14 | 0.26 | 0.42 |
| 20001010 | 130 | 10 | 16.1 | 15.84 | 15.42 | 13.93 | 14 | 0.26 | 0.42 |
| 20001010 | 145 | 10 | 16.1 | 15.84 | 15.42 | 13.93 | 14 | 0.26 | 0.42 |
| 20001010 | 200 | 10 | 16.1 | 15.85 | 15.42 | 13.93 | 14 | 0.25 | 0.43 |
| 20001010 | 215 | 10 | 16.1 | 15.85 | 15.42 | 13.93 | 14 | 0.25 | 0.43 |
| 20001010 | 230 | 10 | 16.1 | 15.85 | 15.42 | 13.93 | 14 | 0.25 | 0.43 |
| 20001010 | 245 | 10 | 16.1 | 15.85 | 15.43 | 13.93 | 14 | 0.25 | 0.42 |
| 20001010 | 300 | 10 | 16.1 | 15.85 | 15.43 | 13.93 | 14 | 0.25 | 0.42 |
| 20001010 | 315 | 10 | 16.1 | 15.85 | 15.43 | 13.93 | 14 | 0.25 | 0.42 |
| 20001010 | 330 | 10 | 16.1 | 15.85 | 15.43 | 13.94 | 14 | 0.25 | 0.42 |
| 20001010 | 345 | 10 | 16.1 | 15.85 | 15.43 | 13.94 | 14 | 0.25 | 0.42 |
| 20001010 | 400 | 10 | 16.1 | 15.85 | 15.43 | 13.94 | 14 | 0.25 | 0.42 |
| 20001010 | 415 | 10 | 16.1 | 15.86 | 15.44 | 13.94 | 14 | 0.24 | 0.42 |
| 20001010 | 430 | 10 | 16.1 | 15.86 | 15.44 | 13.94 | 14 | 0.24 | 0.42 |
| 20001010 | 445 | 10 | 16.1 | 15.86 | 15.44 | 13.94 | 14 | 0.24 | 0.42 |
| 20001010 | 500 | 10 | 16.1 | 15.86 | 15.44 | 13.94 | 14 | 0.24 | 0.42 |
| 20001010 | 515 | 10 | 16.1 | 15.86 | 15.44 | 13.94 | 14 | 0.24 | 0.42 |
| 20001010 | 530 | 10 | 16.1 | 15.86 | 15.44 | 13.94 | 14 | 0.24 | 0.42 |
| 20001010 | 545 | 10 | 16.1 | 15.86 | 15.45 | 13.94 | 14 | 0.24 | 0.41 |
| 20001010 | 600 | 10 | 16.1 | 15.86 | 15.45 | 13.94 | 14 | 0.24 | 0.41 |
| 20001010 | 615 | 10 | 16.1 | 15.87 | 15.45 | 13.94 | 14 | 0.23 | 0.42 |
| 20001010 | 630 | 10 | 16.1 | 15.87 | 15.45 | 13.94 | 14 | 0.23 | 0.42 |
| 20001010 | 645 | 10 | 16.1 | 15.87 | 15.45 | 13.95 | 14 | 0.23 | 0.42 |
| 20001010 | 700 | 10 | 16.1 | 15.87 | 15.45 | 13.95 | 14 | 0.23 | 0.42 |
| 20001010 | 715 | 10 | 16.1 | 15.87 | 15.45 | 13.95 | 14 | 0.23 | 0.42 |
| 20001010 | 730 | 10 | 16.1 | 15.87 | 15.45 | 13.95 | 14 | 0.23 | 0.42 |
| 20001010 | 745 | 10 | 16.1 | 15.87 | 15.46 | 13.95 | 14 | 0.23 | 0.41 |
| 20001010 | 800 | 10 | 16.1 | 15.87 | 15.46 | 13.95 | 14 | 0.23 | 0.41 |
| 20001010 | 815 | 10 | 16.1 | 15.88 | 15.46 | 13.95 | 14 | 0.22 | 0.42 |
| 20001010 | 830 | 10 | 16.1 | 15.88 | 15.46 | 13.95 | 14 | 0.22 | 0.42 |
| 20001010 | 845 | 10 | 16.1 | 15.88 | 15.46 | 13.95 | 14 | 0.22 | 0.42 |
| 20001010 | 900 | 10 | 16.1 | 15.88 | 15.46 | 13.95 | 14 | 0.22 | 0.42 |
| 20001010 | 915 | 10 | 16.1 | 15.88 | 15.46 | 13.95 | 14 | 0.22 | 0.42 |
| 20001010 | 930 | 10 | 16.1 | 15.88 | 15.46 | 13.95 | 14 | 0.22 | 0.42 |
| 20001010 | 945 | 10 | 16.1 | 15.88 | 15.46 | 13.95 | 14 | 0.22 | 0.42 |
| 20001010 | 1000 | 10 | 16.1 | 15.88 | 15.46 | 13.95 | 14 | 0.22 | 0.42 |
| 20001010 | 1015 | 10 | 16.1 | 15.88 | 15.46 | 13.95 | 14 | 0.22 | 0.42 |
| 20001010 | 1030 | 10 | 16.1 | 15.88 | 15.47 | 13.96 | 14 | 0.22 | 0.41 |
| 20001010 | 1045 | 10 | 16.1 | 15.89 | 15.47 | 13.96 | 14 | 0.21 | 0.42 |
| 20001010 | 1100 | 10 | 16.1 | 15.89 | 15.47 | 13.96 | 14 | 0.21 | 0.42 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE | Hinflow | Houtflow |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20001010 | 1115 | 10 | 16.1 | 15.89 | 15.47 | 13.96 | 14 | 0.21 | 0.42 |
| 20001010 | 1130 | 10 | 16.1 | 15.89 | 15.47 | 13.96 | 14 | 0.21 | 0.42 |
| 20001010 | 1145 | 10 | 16.1 | 15.89 | 15.47 | 13.96 | 14 | 0.21 | 0.42 |
| 20001010 | 1200 | 10 | 16.1 | 15.89 | 15.47 | 13.96 | 14 | 0.21 | 0.42 |
| 20001010 | 1215 | 10 | 16.1 | 15.89 | 15.47 | 13.96 | 14 | 0.21 | 0.42 |
| 20001010 | 1230 | 10 | 16.1 | 15.89 | 15.47 | 13.96 | 14 | 0.21 | 0.42 |
| 20001010 | 1245 | 10 | 16.1 | 15.89 | 15.48 | 13.96 | 14 | 0.21 | 0.41 |
| 20001010 | 1300 | 10 | 16.1 | 15.89 | 15.48 | 13.96 | 14 | 0.21 | 0.41 |
| 20001010 | 1315 | 10 | 16.1 | 15.89 | 15.48 | 13.96 | 14 | 0.21 | 0.41 |
| 20001010 | 1330 | 10 | 16.1 | 15.89 | 15.48 | 13.96 | 14 | 0.21 | 0.41 |
| 20001010 | 1345 | 10 | 16.1 | 15.89 | 15.48 | 13.96 | 14 | 0.21 | 0.41 |
| 20001010 | 1400 | 10 | 16.1 | 15.9 | 15.48 | 13.97 | 14 | 0.2 | 0.42 |
| 20001010 | 1415 | 10 | 16.1 | 15.9 | 15.48 | 13.97 | 14 | 0.2 | 0.42 |
| 20001010 | 1430 | 10 | 16.1 | 15.9 | 15.48 | 13.97 | 14 | 0.2 | 0.42 |
| 20001010 | 1445 | 10 | 16.1 | 15.9 | 15.48 | 13.97 | 14 | 0.2 | 0.42 |
| 20001010 | 1500 | 10 | 16.1 | 15.9 | 15.48 | 13.97 | 14 | 0.2 | 0.42 |
| 20001010 | 1515 | 10 | 16.1 | 15.9 | 15.48 | 13.97 | 14 | 0.2 | 0.42 |
| 20001010 | 1530 | 10 | 16.09 | 15.89 | 15.48 | 13.97 | 14 | 0.2 | 0.41 |
| 20001010 | 1545 | 10 | 16.09 | 15.9 | 15.48 | 13.97 | 14 | 0.19 | 0.42 |
| 20001010 | 1600 | 10 | 16.1 | 15.9 | 15.48 | 13.97 | 14 | 0.2 | 0.42 |
| 20001010 | 1615 | 10 | 16.1 | 15.9 | 15.48 | 13.97 | 14 | 0.2 | 0.42 |
| 20001010 | 1630 | 10 | 16.1 | 15.9 | 15.48 | 13.97 | 14 | 0.2 | 0.42 |
| 20001010 | 1645 | 10 | 16.1 | 15.9 | 15.48 | 13.97 | 14 | 0.2 | 0.42 |
| 20001010 | 1700 | 10 | 16.11 | 15.9 | 15.49 | 13.97 | 14 | 0.21 | 0.41 |
| 20001010 | 1715 | 10 | 16.11 | 15.9 | 15.49 | 13.97 | 14 | 0.21 | 0.41 |
| 20001010 | 1730 | 10 | 16.11 | 15.9 | 15.49 | 13.97 | 14 | 0.21 | 0.41 |
| 20001010 | 1745 | 10 | 16.11 | 15.91 | 15.49 | 13.97 | 14 | 0.2 | 0.42 |
| 20001010 | 1800 | 10 | 16.11 | 15.91 | 15.49 | 13.97 | 14 | 0.2 | 0.42 |
| 20001010 | 1815 | 10 | 16.09 | 15.9 | 15.49 | 13.97 | 14 | 0.19 | 0.41 |
| 20001010 | 1830 | 10 | 16.1 | 15.9 | 15.49 | 13.97 | 14 | 0.2 | 0.41 |
| 20001010 | 1845 | 10 | 16.11 | 15.91 | 15.49 | 13.97 | 14 | 0.2 | 0.42 |
| 20001010 | 1900 | 10 | 16.1 | 15.91 | 15.49 | 13.97 | 14 | 0.19 | 0.42 |
| 20001010 | 1915 | 10 | 16.11 | 15.91 | 15.5 | 13.97 | 14 | 0.2 | 0.41 |
| 20001010 | 1930 | 10 | 16.11 | 15.91 | 15.5 | 13.97 | 14 | 0.2 | 0.41 |
| 20001010 | 1945 | 10 | 16.11 | 15.91 | 15.5 | 13.97 | 14 | 0.2 | 0.41 |
| 20001010 | 2000 | 10 | 16.11 | 15.91 | 15.5 | 13.97 | 14 | 0.2 | 0.41 |
| 20001010 | 2015 | 10 | 16.11 | 15.91 | 15.5 | 13.97 | 14 | 0.2 | 0.41 |
| 20001010 | 2030 | 10 | 16.11 | 15.91 | 15.5 | 13.97 | 14 | 0.2 | 0.41 |
| 20001010 | 2045 | 10 | 16.11 | 15.91 | 15.5 | 13.97 | 14 | 0.2 | 0.41 |
| 20001010 | 2100 | 10 | 16.11 | 15.91 | 15.5 | 13.97 | 14 | 0.2 | 0.41 |
| 20001010 | 2115 | 10 | 16.11 | 15.91 | 15.5 | 13.97 | 14 | 0.2 | 0.41 |
| 20001010 | 2130 | 10 | 16.11 | 15.91 | 15.5 | 13.97 | 14 | 0.2 | 0.41 |
| 20001010 | 2145 | 10 | 16.11 | 15.92 | 15.5 | 13.98 | 14 | 0.19 | 0.42 |
| 20001010 | 2200 | 10 | 16.11 | 15.92 | 15.5 | 13.98 | 14 | 0.19 | 0.42 |
| 20001010 | 2215 | 10 | 16.11 | 15.92 | 15.5 | 13.98 | 14 | 0.19 | 0.42 |
| 20001010 | 2230 | 10 | 16.11 | 15.92 | 15.5 | 13.98 | 14 | 0.19 | 0.42 |
| 20001010 | 2245 | 10 | 16.11 | 15.92 | 15.51 | 13.98 | 14 | 0.19 | 0.41 |
| 20001010 | 2300 | 10 | 16.11 | 15.92 | 15.51 | 13.98 | 14 | 0.19 | 0.41 |
| 20001010 | 2315 | 10 | 16.11 | 15.92 | 15.51 | 13.98 | 14 | 0.19 | 0.41 |
| 20001010 | 2330 | 10 | 16.11 | 15.92 | 15.51 | 13.98 | 14 | 0.19 | 0.41 |
| 20001010 | 2345 | 10 | 16.11 | 15.92 | 15.51 | 13.98 | 14 | 0.19 | 0.41 |


| Date | Hrs | Day | G392S+H | G392S+T | G393+H | G393+T | G393CE Hinflow | Houtflow |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 20001011 | 0 | 11 | 16.11 | 15.92 | 15.51 | 13.98 | 14 | 0.19 | 0.41 |
| 20001011 | 15 | 11 | 16.11 | 15.92 | 15.51 | 13.98 | 14 | 0.19 | 0.41 |
| 20001011 | 30 | 11 | 16.11 | 15.92 | 15.51 | 13.99 | 14 | 0.19 | 0.41 |

## APPENDIX II: STA-6 INFLOWS AND OUTFLOWS THROUGH CELL 5 FOR OCTOBER 2000

| Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G601 } \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \text { G602 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G603 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G354 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G393 } \\ \text { cfs } \end{gathered}$ | Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G601-3 } \\ \text { cfs } \end{gathered}$ | $\begin{aligned} & \text { G393+G354 } \\ & \text { Cfs } \end{aligned}$ | $\begin{gathered} \text { G600 } \\ \text { ac-ft } \end{gathered}$ | $\begin{gathered} \text { G601-3 } \\ \mathrm{ac}-\mathrm{ft} \end{gathered}$ | $\begin{gathered} \text { G393+G354 } \\ \text { ac-ft } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.0 | 4.5 | 4.5 | 4.2 | 20.1 | 12.5 | 1 | 0.0 | 0.1 | 0.3 | 0.0 | 0.3 | 0.7 |
|  | 0.0 | 4.5 | 4.5 | 3.9 | 20.1 | 11.8 | 1 | 0.0 | 0.3 | 0.7 | 0.0 | 0.5 | 1.3 |
|  | 0.0 | 4.2 | 4.2 | 3.9 | 20.1 | 11.8 | 1 | 0.0 | 0.4 | 1.0 | 0.0 | 0.8 | 2.0 |
|  | 0.0 | 4.3 | 4.3 | 3.5 | 20.1 | 11.8 | 1 | 0.0 | 0.5 | 1.3 | 0.0 | 1.0 | 2.6 |
|  | 0.0 | 4.3 | 4.3 | 3.5 | 20.1 | 11.8 | 1 | 0.0 | 0.7 | 1.7 | 0.0 | 1.3 | 3.3 |
|  | 0.0 | 4.3 | 4.3 | 3.5 | 20.1 | 11.8 | 1 | 0.0 | 0.8 | 2.0 | 0.0 | 1.5 | 4.0 |
|  | 0.0 | 4.1 | 4.1 | 3.2 | 20.1 | 11.8 | 1 | 0.0 | 0.9 | 2.3 | 0.0 | 1.8 | 4.6 |
|  | 0.0 | 4.1 | 4.1 | 3.2 | 18.5 | 11.8 | 1 | 0.0 | 1.0 | 2.6 | 0.0 | 2.0 | 5.2 |
|  | 0.0 | 3.8 | 3.8 | 3.3 | 18.5 | 11.8 | 1 | 0.0 | 1.1 | 3.0 | 0.0 | 2.2 | 5.9 |
|  | 0.0 | 3.8 | 3.8 | 3.0 | 18.5 | 11.8 | 1 | 0.0 | 1.2 | 3.3 | 0.0 | 2.5 | 6.5 |
|  | 0.0 | 4.0 | 4.0 | 3.0 | 18.5 | 11.1 | 1 | 0.0 | 1.4 | 3.6 | 0.0 | 2.7 | 7.1 |
|  | 0.0 | 3.6 | 3.6 | 3.0 | 18.5 | 11.1 | 1 | 0.0 | 1.5 | 3.9 | 0.0 | 2.9 | 7.7 |
|  | 0.0 | 3.6 | 3.6 | 3.0 | 18.5 | 11.1 | 1 | 0.0 | 1.6 | 4.2 | 0.0 | 3.1 | 8.3 |
|  | 0.0 | 3.8 | 3.8 | 2.7 | 18.5 | 11.1 | 1 | 0.0 | 1.7 | 4.5 | 0.0 | 3.3 | 8.9 |
|  | 0.0 | 3.4 | 3.4 | 2.7 | 18.5 | 11.1 | 1 | 0.0 | 1.8 | 4.8 | 0.0 | 3.5 | 9.6 |
|  | 0.0 | 3.4 | 3.4 | 2.7 | 18.5 | 11.1 | 1 | 0.0 | 1.9 | 5.1 | 0.0 | 3.7 | 10.2 |
|  | 0.0 | 3.4 | 3.4 | 2.4 | 18.5 | 11.1 | 1 | 0.0 | 2.0 | 5.4 | 0.0 | 3.9 | 10.8 |
|  | 0.0 | 3.6 | 3.6 | 2.4 | 18.5 | 11.1 | 1 | 0.0 | 2.1 | 5.7 | 0.0 | 4.1 | 11.4 |
|  | 0.0 | 3.3 | 3.3 | 2.4 | 17.0 | 11.1 | 1 | 0.0 | 2.2 | 6.0 | 0.0 | 4.3 | 12.0 |
|  | 0.0 | 3.3 | 3.3 | 2.2 | 17.0 | 10.4 | 1 | 0.0 | 2.3 | 6.3 | 0.0 | 4.5 | 12.5 |
|  | 0.0 | 3.3 | 3.3 | 2.2 | 17.0 | 10.4 | 1 | 0.0 | 2.3 | 6.6 | 0.0 | 4.7 | 13.1 |
|  | 0.0 | 3.4 | 3.4 | 2.2 | 17.0 | 10.4 | 1 | 0.0 | 2.4 | 6.9 | 0.0 | 4.8 | 13.7 |
|  | 0.0 | 3.1 | 3.1 | 2.2 | 17.0 | 10.4 | 1 | 0.0 | 2.5 | 7.2 | 0.0 | 5.0 | 14.2 |
|  | 0.0 | 3.1 | 3.1 | 1.9 | 17.0 | 10.4 | 1 | 0.0 | 2.6 | 7.5 | 0.0 | 5.2 | 14.8 |
|  | 0.0 | 3.1 | 3.1 | 2.0 | 17.0 | 10.4 | 1 | 0.0 | 2.7 | 7.7 | 0.0 | 5.4 | 15.4 |
|  | 0.0 | 2.9 | 2.9 | 2.0 | 17.0 | 10.4 | 1 | 0.0 | 2.8 | 8.0 | 0.0 | 5.5 | 15.9 |
|  | 0.0 | 2.9 | 2.9 | 1.7 | 17.0 | 10.4 | 1 | 0.0 | 2.9 | 8.3 | 0.0 | 5.7 | 16.5 |
|  | 0.0 | 2.9 | 2.9 | 1.7 | 17.0 | 10.4 | 1 | 0.0 | 2.9 | 8.6 | 0.0 | 5.8 | 17.1 |
|  | 0.0 | 2.7 | 2.7 | 1.7 | 15.5 | 9.8 | 1 | 0.0 | 3.0 | 8.9 | 0.0 | 6.0 | 17.6 |
|  | 0.0 | 2.8 | 2.8 | 1.7 | 15.5 | 9.8 | 1 | 0.0 | 3.1 | 9.1 | 0.0 | 6.1 | 18.1 |
|  | 0.0 | 2.8 | 2.8 | 1.5 | 15.5 | 9.8 | 1 | 0.0 | 3.2 | 9.4 | 0.0 | 6.3 | 18.6 |
|  | 0.0 | 2.8 | 2.8 | 1.5 | 15.5 | 9.8 | 1 | 0.0 | 3.2 | 9.7 | 0.0 | 6.4 | 19.2 |
|  | 305.0 | 6.2 | 6.2 | 1.5 | 15.5 | 9.8 | 1 | 3.2 | 3.4 | 9.9 | 6.3 | 6.7 | 19.7 |
|  | 295.0 | 8.0 | 8.0 | 7.3 | 15.5 | 9.8 | 1 | 6.3 | 3.6 | 10.2 | 12.4 | 7.2 | 20.2 |
|  | 284.6 | 15.2 | 15.2 | 15.0 | 15.5 | 9.8 | 1 | 9.2 | 4.1 | 10.5 | 18.3 | 8.1 | 20.7 |
|  | 286.7 | 19.6 | 19.6 | 22.3 | 15.5 | 9.8 | 1 | 12.2 | 4.7 | 10.7 | 24.2 | 9.4 | 21.3 |
|  | 286.2 | 23.9 | 23.9 | 29.2 | 15.5 | 9.8 | 1 | 15.2 | 5.5 | 11.0 | 30.1 | 11.0 | 21.8 |
|  | 278.7 | 28.5 | 28.5 | 34.1 | 15.5 | 9.8 | 1 | 18.1 | 6.5 | 11.2 | 35.9 | 12.9 | 22.3 |
|  | 277.8 | 30.5 | 30.5 | 39.5 | 14.1 | 9.2 | 1 | 21.0 | 7.5 | 11.5 | 41.6 | 14.9 | 22.8 |
|  | 272.9 | 35.6 | 35.6 | 46.1 | 14.1 | 9.2 | 1 | 23.8 | 8.8 | 11.7 | 47.3 | 17.4 | 23.3 |
|  | 273.5 | 36.7 | 36.7 | 51.2 | 14.1 | 9.2 | 1 | 26.7 | 10.1 | 12.0 | 52.9 | 19.9 | 23.7 |
|  | 269.5 | 41.1 | 41.1 | 56.4 | 14.1 | 9.2 | 1 | 29.5 | 11.5 | 12.2 | 58.5 | 22.8 | 24.2 |
|  | 274.9 | 44.4 | 44.4 | 60.8 | 14.1 | 9.2 | 1 | 32.3 | 13.1 | 12.5 | 64.2 | 25.9 | 24.7 |
|  | 276.3 | 46.3 | 46.3 | 66.5 | 14.1 | 9.2 | 1 | 35.2 | 14.7 | 12.7 | 69.9 | 29.2 | 25.2 |
|  | 272.3 | 48.8 | 48.8 | 71.2 | 14.1 | 9.2 | 1 | 38.1 | 16.5 | 12.9 | 75.5 | 32.7 | 25.7 |
|  | 273.8 | 52.1 | 52.1 | 74.8 | 14.1 | 9.2 | 1 | 40.9 | 18.3 | 13.2 | 81.1 | 36.4 | 26.1 |


| Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \mathrm{G} 601 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \mathrm{G} 602 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \text { G603 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G354 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \mathrm{G} 393 \\ \mathrm{cfs} \end{gathered}$ | Day | $\begin{gathered} \mathrm{G} 600 \\ \mathrm{cfs} \end{gathered}$ | G601-3 <br> cfs | $\begin{aligned} & \mathrm{G} 393+\mathrm{G} 354 \\ & \text { Cfs } \end{aligned}$ | G600 $\mathrm{ac}-\mathrm{ft}$ | G601-3 $\mathrm{ac}-\mathrm{ft}$ | $\begin{gathered} \mathrm{G} 393+\mathrm{G} 354 \\ \mathrm{ac}-\mathrm{ft} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 266.1 | 54.1 | 54.1 | 78.5 | 14.1 | 9.2 | 1 | 43.7 | 20.3 | 13.4 | 86.6 | 40.2 | 26.6 |
|  | 264.4 | 56.6 | 56.6 | 82.3 | 12.7 | 9.2 | 1 | 46.4 | 22.3 | 13.6 | 92.1 | 44.3 | 27.1 |
|  | 261.0 | 58.0 | 58.0 | 86.4 | 12.7 | 9.2 | 1 | 49.2 | 24.4 | 13.9 | 97.5 | 48.4 | 27.5 |
|  | 260.1 | 60.5 | 60.5 | 88.8 | 12.7 | 9.2 | 1 | 51.9 | 26.6 | 14.1 | 102.9 | 52.8 | 28.0 |
|  | 259.0 | 60.8 | 60.8 | 91.6 | 12.7 | 9.2 | 1 | 54.6 | 28.8 | 14.3 | 108.2 | 57.2 | 28.4 |
|  | 255.1 | 62.7 | 62.7 | 94.4 | 12.7 | 9.2 | 1 | 57.2 | 31.1 | 14.6 | 113.5 | 61.7 | 28.9 |
|  | 254.7 | 63.4 | 63.4 | 95.3 | 12.7 | 9.8 | 1 | 59.9 | 33.4 | 14.8 | 118.8 | 66.3 | 29.3 |
|  | 256.3 | 65.3 | 65.3 | 96.6 | 12.7 | 9.8 | 1 | 62.5 | 35.8 | 15.0 | 124.1 | 71.0 | 29.8 |
|  | 252.9 | 66.0 | 66.0 | 97.9 | 12.7 | 9.8 | 1 | 65.2 | 38.2 | 15.3 | 129.3 | 75.8 | 30.3 |
|  | 254.8 | 66.8 | 66.8 | 99.5 | 12.7 | 9.8 | 1 | 67.8 | 40.6 | 15.5 | 134.5 | 80.6 | 30.7 |
|  | 0.0 | 55.7 | 55.7 | 97.6 | 12.7 | 9.8 | 1 | 67.8 | 42.8 | 15.7 | 134.5 | 84.9 | 31.2 |
|  | 0.0 | 56.9 | 56.9 | 86.5 | 12.7 | 10.4 | 1 | 67.8 | 44.9 | 16.0 | 134.5 | 89.0 | 31.7 |
|  | 0.0 | 45.6 | 45.6 | 75.8 | 12.7 | 10.4 | 1 | 67.8 | 46.6 | 16.2 | 134.5 | 92.5 | 32.2 |
|  | 0.0 | 43.3 | 43.3 | 67.2 | 12.7 | 10.4 | 1 | 67.8 | 48.2 | 16.5 | 134.5 | 95.6 | 32.6 |
|  | 0.0 | 40.1 | 40.1 | 61.3 | 12.7 | 10.4 | 1 | 67.8 | 49.7 | 16.7 | 134.5 | 98.6 | 33.1 |
|  | 0.0 | 35.1 | 35.1 | 56.9 | 12.7 | 11.1 | 1 | 67.8 | 51.0 | 16.9 | 134.5 | 101.2 | 33.6 |
|  | 0.0 | 34.1 | 34.1 | 51.6 | 12.7 | 11.1 | 1 | 67.8 | 52.3 | 17.2 | 134.5 | 103.7 | 34.1 |
|  | 0.0 | 30.9 | 30.9 | 48.7 | 12.7 | 11.1 | 1 | 67.8 | 53.4 | 17.4 | 134.5 | 106.0 | 34.6 |
|  | 0.0 | 29.1 | 29.1 | 44.8 | 12.7 | 11.1 | 1 | 67.8 | 54.5 | 17.7 | 134.5 | 108.1 | 35.1 |
|  | 0.0 | 27.3 | 27.3 | 41.9 | 12.7 | 11.8 | 1 | 67.8 | 55.5 | 17.9 | 134.5 | 110.1 | 35.6 |
|  | 0.0 | 25.7 | 25.7 | 39.3 | 12.7 | 11.8 | 1 | 67.8 | 56.4 | 18.2 | 134.5 | 112.0 | 36.1 |
|  | 0.0 | 24.0 | 24.0 | 36.6 | 12.7 | 11.8 | 1 | 67.8 | 57.3 | 18.5 | 134.5 | 113.7 | 36.6 |
|  | 0.0 | 22.4 | 22.4 | 34.0 | 12.7 | 11.8 | 1 | 67.8 | 58.1 | 18.7 | 134.5 | 115.3 | 37.1 |
|  | 0.0 | 21.6 | 21.6 | 32.3 | 12.7 | 11.8 | 1 | 67.8 | 58.9 | 19.0 | 134.5 | 116.9 | 37.6 |
|  | 0.0 | 20.5 | 20.5 | 29.9 | 12.7 | 12.5 | 1 | 67.8 | 59.7 | 19.2 | 134.5 | 118.4 | 38.1 |
|  | 0.0 | 19.1 | 19.1 | 28.2 | 12.7 | 12.5 | 1 | 67.8 | 60.4 | 19.5 | 134.5 | 119.7 | 38.7 |
|  | 0.0 | 18.7 | 18.7 | 26.7 | 12.7 | 12.5 | 1 | 67.8 | 61.0 | 19.7 | 134.5 | 121.1 | 39.2 |
|  | 0.0 | 17.3 | 17.3 | 25.3 | 12.7 | 12.5 | 1 | 67.8 | 61.7 | 20.0 | 134.5 | 122.3 | 39.7 |
|  | 0.0 | 16.9 | 16.9 | 24.5 | 12.7 | 12.5 | 1 | 67.8 | 62.3 | 20.3 | 134.5 | 123.5 | 40.2 |
|  | 0.0 | 15.9 | 15.9 | 23.1 | 12.7 | 12.5 | 1 | 67.8 | 62.8 | 20.5 | 134.5 | 124.6 | 40.7 |
|  | 0.0 | 15.0 | 15.0 | 21.6 | 12.7 | 12.5 | 1 | 67.8 | 63.4 | 20.8 | 134.5 | 125.7 | 41.3 |
|  | 0.0 | 14.6 | 14.6 | 20.9 | 12.7 | 12.5 | 1 | 67.8 | 63.9 | 21.1 | 134.5 | 126.7 | 41.8 |
|  | 0.0 | 13.7 | 13.7 | 19.6 | 12.7 | 12.5 | 1 | 67.8 | 64.4 | 21.3 | 134.5 | 127.7 | 42.3 |
|  | 0.0 | 13.4 | 13.4 | 19.0 | 12.7 | 12.5 | 1 | 67.8 | 64.9 | 21.6 | 134.5 | 128.7 | 42.8 |
|  | 0.0 | 13.1 | 13.1 | 17.6 | 14.1 | 12.5 | 1 | 67.8 | 65.3 | 21.9 | 134.5 | 129.6 | 43.4 |
|  | 0.0 | 12.2 | 12.2 | 17.1 | 14.1 | 12.5 | 1 | 67.8 | 65.7 | 22.1 | 134.5 | 130.4 | 43.9 |
|  | 0.0 | 11.9 | 11.9 | 16.4 | 14.1 | 12.5 | 1 | 67.8 | 66.2 | 22.4 | 134.5 | 131.2 | 44.5 |
|  | 0.0 | 11.6 | 11.6 | 15.8 | 14.1 | 12.5 | 1 | 67.8 | 66.6 | 22.7 | 134.5 | 132.1 | 45.0 |
|  | 0.0 | 11.3 | 11.3 | 15.2 | 14.1 | 12.5 | 1 | 67.8 | 67.0 | 23.0 | 134.5 | 132.8 | 45.6 |
|  | 0.0 | 10.8 | 10.8 | 14.6 | 14.1 | 12.5 | 1 | 67.8 | 67.3 | 23.2 | 134.5 | 133.6 | 46.1 |
|  | 0.0 | 10.5 | 10.5 | 14.1 | 14.1 | 12.5 | 1 | 67.8 | 67.7 | 23.5 | 134.5 | 134.3 | 46.6 |
|  | 0.0 | 10.2 | 10.2 | 13.5 | 14.1 | 12.5 | 1 | 67.8 | 68.1 | 23.8 | 134.5 | 135.0 | 47.2 |
|  | 0.0 | 10.0 | 10.0 | 12.9 | 14.1 | 12.5 | 1 | 67.8 | 68.4 | 24.1 | 134.5 | 135.7 | 47.7 |
|  | 0.0 | 10.0 | 10.0 | 12.4 | 14.1 | 11.8 | 1 | 67.8 | 68.7 | 24.3 | 134.5 | 136.4 | 48.3 |
|  | 0.0 | 9.2 | 9.2 | 11.8 | 14.1 | 11.8 | 1 | 67.8 | 69.1 | 24.6 | 134.5 | 137.0 | 48.8 |
|  | 0.0 | 9.2 | 9.2 | 11.4 | 14.1 | 11.8 | 1 | 67.8 | 69.4 | 24.9 | 134.5 | 137.6 | 49.3 |
|  | 0.0 | 8.9 | 8.9 | 11.4 | 14.1 | 11.8 | 1 | 67.8 | 69.7 | 25.1 | 134.5 | 138.2 | 49.9 |
|  | 0.0 | 8.7 | 8.7 | 10.8 | 14.1 | 11.8 | 1 | 67.8 | 70.0 | 25.4 | 134.5 | 138.8 | 50.4 |
|  | 0.0 | 8.2 | 8.2 | 10.3 | 14.1 | 11.8 | 1 | 67.8 | 70.2 | 25.7 | 134.5 | 139.3 | 50.9 |
|  | 0.0 | 8.4 | 8.4 | 9.8 | 14.1 | 11.8 | 1 | 67.8 | 70.5 | 26.0 | 134.5 | 139.9 | 51.5 |


| Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G601 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \mathrm{G} 602 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \mathrm{G} 603 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \text { G354 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \mathrm{G} 393 \\ \mathrm{cfs} \end{gathered}$ | Day | $\begin{gathered} \mathrm{G} 600 \\ \mathrm{cfs} \end{gathered}$ | G601-3 <br> cfs | $\begin{aligned} & \mathrm{G} 393+\mathrm{G} 354 \\ & \text { Cfs } \end{aligned}$ | G600 $\mathrm{ac}-\mathrm{ft}$ | G601-3 ac-ft | $\begin{gathered} \mathrm{G} 393+\mathrm{G} 354 \\ \mathrm{ac}-\mathrm{ft} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 7.9 | 7.9 | 9.8 | 14.1 | 11.8 | 1 | 67.8 | 70.8 | 26.2 | 134.5 | 140.4 | 52.0 |
|  | 0.0 | 7.7 | 7.7 | 9.3 | 14.1 | 11.8 | 1 | 67.8 | 71.0 | 26.5 | 134.5 | 140.9 | 52.6 |
|  | 0.0 | 7.7 | 7.7 | 8.9 | 15.5 | 11.8 | 1 | 67.8 | 71.3 | 26.8 | 134.5 | 141.4 | 53.1 |
|  | 0.0 | 7.5 | 7.5 | 8.9 | 15.5 | 11.1 | 1 | 67.8 | 71.6 | 27.1 | 134.5 | 141.9 | 53.7 |
|  | 0.0 | 7.0 | 7.0 | 8.5 | 15.5 | 11.1 | 1 | 67.8 | 71.8 | 27.3 | 134.5 | 142.4 | 54.2 |
|  | 0.0 | 7.2 | 7.2 | 8.0 | 15.5 | 11.1 | 1 | 67.8 | 72.0 | 27.6 | 134.5 | 142.9 | 54.8 |
|  | 0.0 | 6.8 | 6.8 | 8.0 | 15.5 | 11.1 | 1 | 67.8 | 72.2 | 27.9 | 134.5 | 143.3 | 55.3 |
|  | 0.0 | 7.0 | 7.0 | 7.5 | 15.5 | 11.1 | 1 | 67.8 | 72.5 | 28.2 | 134.5 | 143.7 | 55.9 |
|  | 0.0 | 6.6 | 6.6 | 7.5 | 15.5 | 11.1 | 1 | 67.8 | 72.7 | 28.4 | 134.5 | 144.2 | 56.4 |
|  | 0.0 | 6.8 | 6.8 | 7.1 | 15.5 | 11.1 | 1 | 67.8 | 72.9 | 28.7 | 134.5 | 144.6 | 57.0 |
|  | 0.0 | 6.3 | 6.3 | 7.2 | 15.5 | 11.1 | 1 | 67.8 | 73.1 | 29.0 | 134.5 | 145.0 | 57.5 |
|  | 0.0 | 6.5 | 6.5 | 6.7 | 15.5 | 11.1 | 1 | 67.8 | 73.3 | 29.3 | 134.5 | 145.4 | 58.1 |
|  | 0.0 | 6.1 | 6.1 | 6.7 | 15.5 | 11.1 | 1 | 67.8 | 73.5 | 29.6 | 134.5 | 145.8 | 58.6 |
|  | 0.0 | 6.3 | 6.3 | 6.3 | 15.5 | 10.4 | 1 | 67.8 | 73.7 | 29.8 | 134.5 | 146.2 | 59.1 |
|  | 0.0 | 5.9 | 5.9 | 6.3 | 15.5 | 10.4 | 1 | 67.8 | 73.9 | 30.1 | 134.5 | 146.6 | 59.7 |
|  | 0.0 | 6.1 | 6.1 | 5.9 | 15.5 | 10.4 | 1 | 67.8 | 74.1 | 30.4 | 134.5 | 146.9 | 60.2 |
|  | 0.0 | 6.1 | 6.1 | 5.9 | 15.5 | 10.4 | 1 | 67.8 | 74.3 | 30.6 | 134.5 | 147.3 | 60.8 |
|  | 0.0 | 5.7 | 5.7 | 5.5 | 14.1 | 10.4 | 1 | 67.8 | 74.4 | 30.9 | 134.5 | 147.7 | 61.3 |
|  | 0.0 | 5.9 | 5.9 | 5.6 | 14.1 | 10.4 | 1 | 67.8 | 74.6 | 31.1 | 134.5 | 148.0 | 61.8 |
|  | 0.0 | 5.5 | 5.5 | 5.2 | 14.1 | 10.4 | 1 | 67.8 | 74.8 | 31.4 | 134.5 | 148.4 | 62.3 |
| 2 | 0.0 | 5.6 | 5.6 | 5.2 | 14.1 | 10.4 | 2 | 67.8 | 75.0 | 31.7 | 134.5 | 148.7 | 62.8 |
|  | 0.0 | 5.3 | 5.3 | 4.8 | 14.1 | 10.4 | 2 | 67.8 | 75.1 | 31.9 | 134.5 | 149.0 | 63.3 |
|  | 0.0 | 5.3 | 5.3 | 4.8 | 14.1 | 9.8 | 2 | 67.8 | 75.3 | 32.2 | 134.5 | 149.3 | 63.8 |
|  | 0.0 | 5.1 | 5.1 | 4.8 | 14.1 | 9.8 | 2 | 67.8 | 75.4 | 32.4 | 134.5 | 149.6 | 64.3 |
|  | 0.0 | 5.1 | 5.1 | 4.5 | 14.1 | 9.8 | 2 | 67.8 | 75.6 | 32.7 | 134.5 | 149.9 | 64.8 |
|  | 0.0 | 5.1 | 5.1 | 4.5 | 14.1 | 9.8 | 2 | 67.8 | 75.7 | 32.9 | 134.5 | 150.2 | 65.3 |
|  | 0.0 | 4.8 | 4.8 | 4.1 | 14.1 | 9.8 | 2 | 67.8 | 75.9 | 33.2 | 134.5 | 150.5 | 65.8 |
|  | 0.0 | 4.8 | 4.8 | 4.2 | 14.1 | 9.8 | 2 | 67.8 | 76.0 | 33.4 | 134.5 | 150.8 | 66.3 |
|  | 0.0 | 4.5 | 4.5 | 4.2 | 14.1 | 9.8 | 2 | 67.8 | 76.2 | 33.7 | 134.5 | 151.1 | 66.7 |
|  | 0.0 | 4.6 | 4.6 | 3.8 | 14.1 | 9.8 | 2 | 67.8 | 76.3 | 33.9 | 134.5 | 151.4 | 67.2 |
|  | 0.0 | 4.6 | 4.6 | 3.8 | 14.1 | 9.8 | 2 | 67.8 | 76.4 | 34.1 | 134.5 | 151.6 | 67.7 |
|  | 0.0 | 4.3 | 4.3 | 3.8 | 14.1 | 9.8 | 2 | 67.8 | 76.6 | 34.4 | 134.5 | 151.9 | 68.2 |
|  | 0.0 | 4.4 | 4.4 | 3.5 | 14.1 | 9.2 | 2 | 67.8 | 76.7 | 34.6 | 134.5 | 152.1 | 68.7 |
|  | 0.0 | 4.4 | 4.4 | 3.5 | 14.1 | 9.2 | 2 | 67.8 | 76.8 | 34.9 | 134.5 | 152.4 | 69.2 |
|  | 0.0 | 4.4 | 4.4 | 3.5 | 14.1 | 9.2 | 2 | 67.8 | 77.0 | 35.1 | 134.5 | 152.7 | 69.7 |
|  | 0.0 | 4.2 | 4.2 | 3.2 | 14.1 | 9.2 | 2 | 67.8 | 77.1 | 35.4 | 134.5 | 152.9 | 70.1 |
|  | 0.0 | 4.2 | 4.2 | 3.2 | 14.1 | 9.2 | 2 | 67.8 | 77.2 | 35.6 | 134.5 | 153.1 | 70.6 |
|  | 0.0 | 3.9 | 3.9 | 3.2 | 14.1 | 9.2 | 2 | 67.8 | 77.3 | 35.8 | 134.5 | 153.4 | 71.1 |
|  | 0.0 | 4.0 | 4.0 | 2.9 | 14.1 | 9.2 | 2 | 67.8 | 77.4 | 36.1 | 134.5 | 153.6 | 71.6 |
|  | 0.0 | 4.0 | 4.0 | 2.9 | 12.7 | 9.2 | 2 | 67.8 | 77.6 | 36.3 | 134.5 | 153.8 | 72.0 |
|  | 0.0 | 3.7 | 3.7 | 2.9 | 12.7 | 9.2 | 2 | 67.8 | 77.7 | 36.5 | 134.5 | 154.0 | 72.5 |
|  | 0.0 | 3.8 | 3.8 | 2.6 | 12.7 | 9.2 | 2 | 67.8 | 77.8 | 36.8 | 134.5 | 154.3 | 72.9 |
|  | 0.0 | 3.8 | 3.8 | 2.6 | 12.7 | 8.5 | 2 | 67.8 | 77.9 | 37.0 | 134.5 | 154.5 | 73.4 |
|  | 0.0 | 3.8 | 3.8 | 2.6 | 12.7 | 8.5 | 2 | 67.8 | 78.0 | 37.2 | 134.5 | 154.7 | 73.8 |
|  | 0.0 | 3.6 | 3.6 | 2.4 | 12.7 | 8.5 | 2 | 67.8 | 78.1 | 37.4 | 134.5 | 154.9 | 74.3 |
|  | 0.0 | 3.6 | 3.6 | 2.4 | 12.7 | 8.5 | 2 | 67.8 | 78.2 | 37.7 | 134.5 | 155.1 | 74.7 |
|  | 0.0 | 3.6 | 3.6 | 2.4 | 12.7 | 8.5 | 2 | 67.8 | 78.3 | 37.9 | 134.5 | 155.3 | 75.1 |
|  | 0.0 | 3.3 | 3.3 | 2.4 | 12.7 | 8.5 | 2 | 67.8 | 78.4 | 38.1 | 134.5 | 155.5 | 75.6 |
|  | 0.0 | 3.5 | 3.5 | 2.1 | 12.7 | 8.5 | 2 | 67.8 | 78.5 | 38.3 | 134.5 | 155.7 | 76.0 |
|  | 0.0 | 3.8 | 3.8 | 2.3 | 12.7 | 9.2 | 2 | 67.8 | 78.6 | 38.6 | 134.5 | 155.9 | 76.5 |


| Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \mathrm{G} 601 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \mathrm{G} 602 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \hline \text { G603 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \text { G354 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \mathrm{G} 393 \\ \mathrm{cfs} \end{gathered}$ | Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{aligned} & \mathrm{G} 601-3 \\ & \mathrm{cfs} \end{aligned}$ | G393+G354 <br> Cfs | G600 $\mathrm{ac}-\mathrm{ft}$ | G601-3 $\mathrm{ac}-\mathrm{ft}$ | $\begin{gathered} \text { G393+G354 } \\ \text { ac-ft } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 3.5 | 3.5 | 2.4 | 14.1 | 9.2 | 2 | 67.8 | 78.7 | 38.8 | 134.5 | 156.1 | 76.9 |
|  | 0.0 | 3.5 | 3.5 | 2.4 | 14.1 | 9.2 | 2 | 67.8 | 78.8 | 39.0 | 134.5 | 156.3 | 77.4 |
|  | 0.0 | 3.3 | 3.3 | 2.4 | 14.1 | 8.5 | 2 | 67.8 | 78.9 | 39.3 | 134.5 | 156.4 | 77.9 |
|  | 0.0 | 3.6 | 3.6 | 2.4 | 14.1 | 8.5 | 2 | 67.8 | 79.0 | 39.5 | 134.5 | 156.6 | 78.4 |
|  | 0.0 | 3.5 | 3.5 | 2.1 | 14.1 | 8.5 | 2 | 67.8 | 79.1 | 39.7 | 134.5 | 156.8 | 78.8 |
|  | 0.0 | 3.3 | 3.3 | 2.6 | 17.0 | 8.5 | 2 | 67.8 | 79.2 | 40.0 | 134.5 | 157.0 | 79.4 |
|  | 0.0 | 3.6 | 3.6 | 2.6 | 18.5 | 9.2 | 2 | 67.8 | 79.3 | 40.3 | 134.5 | 157.2 | 79.9 |
|  | 0.0 | 3.6 | 3.6 | 2.6 | 18.5 | 9.2 | 2 | 67.8 | 79.4 | 40.6 | 134.5 | 157.4 | 80.5 |
|  | 0.0 | 3.3 | 3.3 | 2.4 | 18.5 | 9.2 | 2 | 67.8 | 79.5 | 40.9 | 134.5 | 157.6 | 81.1 |
|  | 0.0 | 3.3 | 3.3 | 2.4 | 18.5 | 9.2 | 2 | 67.8 | 79.6 | 41.2 | 134.5 | 157.8 | 81.6 |
|  | 0.0 | 3.1 | 3.1 | 2.4 | 18.5 | 9.2 | 2 | 67.8 | 79.6 | 41.5 | 134.5 | 158.0 | 82.2 |
|  | 0.0 | 3.4 | 3.4 | 2.1 | 18.5 | 9.2 | 2 | 67.8 | 79.7 | 41.7 | 134.5 | 158.1 | 82.8 |
|  | 0.0 | 3.1 | 3.1 | 2.1 | 18.5 | 9.2 | 2 | 67.8 | 79.8 | 42.0 | 134.5 | 158.3 | 83.4 |
|  | 0.0 | 3.1 | 3.1 | 2.1 | 18.5 | 8.5 | 2 | 67.8 | 79.9 | 42.3 | 134.5 | 158.5 | 83.9 |
|  | 0.0 | 3.1 | 3.1 | 2.1 | 18.5 | 8.5 | 2 | 67.8 | 80.0 | 42.6 | 134.5 | 158.7 | 84.5 |
|  | 0.0 | 2.9 | 2.9 | 2.1 | 17.0 | 8.5 | 2 | 67.8 | 80.1 | 42.9 | 134.5 | 158.8 | 85.0 |
|  | 0.0 | 2.9 | 2.9 | 1.9 | 17.0 | 8.5 | 2 | 67.8 | 80.2 | 43.1 | 134.5 | 159.0 | 85.5 |
|  | 0.0 | 2.9 | 2.9 | 1.9 | 17.0 | 8.5 | 2 | 67.8 | 80.2 | 43.4 | 134.5 | 159.1 | 86.1 |
|  | 0.0 | 2.9 | 2.9 | 1.9 | 17.0 | 8.5 | 2 | 67.8 | 80.3 | 43.7 | 134.5 | 159.3 | 86.6 |
|  | 0.0 | 2.7 | 2.7 | 1.9 | 17.0 | 8.5 | 2 | 67.8 | 80.4 | 43.9 | 134.5 | 159.5 | 87.1 |
|  | 0.0 | 2.7 | 2.7 | 1.6 | 17.0 | 8.5 | 2 | 67.8 | 80.5 | 44.2 | 134.5 | 159.6 | 87.6 |
|  | 0.0 | 2.8 | 2.8 | 1.6 | 17.0 | 8.5 | 2 | 67.8 | 80.5 | 44.5 | 134.5 | 159.7 | 88.2 |
|  | 0.0 | 2.8 | 2.8 | 1.6 | 17.0 | 8.5 | 2 | 67.8 | 80.6 | 44.7 | 134.5 | 159.9 | 88.7 |
|  | 0.0 | 2.5 | 2.5 | 1.6 | 17.0 | 8.5 | 2 | 67.8 | 80.7 | 45.0 | 134.5 | 160.0 | 89.2 |
|  | 0.0 | 2.5 | 2.5 | 1.4 | 15.5 | 7.9 | 2 | 67.8 | 80.7 | 45.2 | 134.5 | 160.2 | 89.7 |
|  | 0.0 | 2.5 | 2.5 | 1.4 | 15.5 | 7.9 | 2 | 67.8 | 80.8 | 45.5 | 134.5 | 160.3 | 90.2 |
|  | 0.0 | 2.6 | 2.6 | 1.4 | 15.5 | 7.9 | 2 | 67.8 | 80.9 | 45.7 | 134.5 | 160.4 | 90.7 |
|  | 0.0 | 2.6 | 2.6 | 1.4 | 15.5 | 7.9 | 2 | 67.8 | 81.0 | 46.0 | 134.5 | 160.6 | 91.2 |
|  | 0.0 | 2.6 | 2.6 | 1.4 | 15.5 | 7.9 | 2 | 67.8 | 81.0 | 46.2 | 134.5 | 160.7 | 91.7 |
|  | 0.0 | 2.3 | 2.3 | 1.4 | 15.5 | 7.9 | 2 | 67.8 | 81.1 | 46.5 | 134.5 | 160.8 | 92.1 |
|  | 0.0 | 2.3 | 2.3 | 1.4 | 15.5 | 7.9 | 2 | 67.8 | 81.2 | 46.7 | 134.5 | 161.0 | 92.6 |
|  | 0.0 | 2.3 | 2.3 | 1.2 | 15.5 | 7.9 | 2 | 67.8 | 81.2 | 46.9 | 134.5 | 161.1 | 93.1 |
|  | 0.0 | 2.3 | 2.3 | 1.2 | 15.5 | 7.9 | 2 | 67.8 | 81.3 | 47.2 | 134.5 | 161.2 | 93.6 |
|  | 0.0 | 2.4 | 2.4 | 1.2 | 15.5 | 7.9 | 2 | 67.8 | 81.3 | 47.4 | 134.5 | 161.3 | 94.1 |
|  | 0.0 | 2.2 | 2.2 | 1.2 | 15.5 | 7.9 | 2 | 67.8 | 81.4 | 47.7 | 134.5 | 161.4 | 94.6 |
|  | 0.0 | 2.2 | 2.2 | 1.0 | 14.1 | 7.9 | 2 | 67.8 | 81.5 | 47.9 | 134.5 | 161.6 | 95.0 |
|  | 0.0 | 2.2 | 2.2 | 1.0 | 14.1 | 7.9 | 2 | 67.8 | 81.5 | 48.1 | 134.5 | 161.7 | 95.5 |
|  | 0.0 | 2.2 | 2.2 | 1.0 | 14.1 | 7.9 | 2 | 67.8 | 81.6 | 48.4 | 134.5 | 161.8 | 95.9 |
|  | 0.0 | 2.0 | 2.0 | 1.0 | 14.1 | 7.9 | 2 | 67.8 | 81.6 | 48.6 | 134.5 | 161.9 | 96.4 |
|  | 0.0 | 2.0 | 2.0 | 0.8 | 14.1 | 7.4 | 2 | 67.8 | 81.7 | 48.8 | 134.5 | 162.0 | 96.8 |
|  | 0.0 | 2.0 | 2.0 | 0.8 | 14.1 | 7.4 | 2 | 67.8 | 81.7 | 49.0 | 134.5 | 162.1 | 97.3 |
|  | 0.0 | 2.0 | 2.0 | 0.8 | 14.1 | 7.4 | 2 | 67.8 | 81.8 | 49.3 | 134.5 | 162.2 | 97.7 |
|  | 0.0 | 2.0 | 2.0 | 0.8 | 14.1 | 7.4 | 2 | 67.8 | 81.8 | 49.5 | 134.5 | 162.3 | 98.2 |
|  | 0.0 | 1.8 | 1.8 | 0.8 | 14.1 | 7.4 | 2 | 67.8 | 81.9 | 49.7 | 134.5 | 162.4 | 98.6 |
|  | 0.0 | 1.9 | 1.9 | 0.7 | 14.1 | 7.4 | 2 | 67.8 | 81.9 | 49.9 | 134.5 | 162.5 | 99.0 |
|  | 0.0 | 1.9 | 1.9 | 0.7 | 14.1 | 7.4 | 2 | 67.8 | 82.0 | 50.2 | 134.5 | 162.6 | 99.5 |
|  | 0.0 | 1.9 | 1.9 | 0.7 | 12.7 | 7.4 | 2 | 67.8 | 82.0 | 50.4 | 134.5 | 162.7 | 99.9 |
|  | 0.0 | 1.9 | 1.9 | 0.7 | 12.7 | 7.4 | 2 | 67.8 | 82.1 | 50.6 | 134.5 | 162.8 | 100.3 |
|  | 0.0 | 1.7 | 1.7 | 0.7 | 12.7 | 7.4 | 2 | 67.8 | 82.1 | 50.8 | 134.5 | 162.8 | 100.7 |
|  | 0.0 | 1.7 | 1.7 | 0.5 | 12.7 | 7.4 | 2 | 67.8 | 82.1 | 51.0 | 134.5 | 162.9 | 101.1 |


| Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G601 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \mathrm{G} 602 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \mathrm{G} 603 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \text { G354 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G393 } \\ \mathrm{cfs} \end{gathered}$ | Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{aligned} & \text { G601-3 } \\ & \text { cfs } \end{aligned}$ | G393+G354 <br> Cfs | G600 <br> ac-ft | G601-3 $\mathrm{ac}-\mathrm{ft}$ | $\begin{gathered} \text { G393+G354 } \\ \text { ac-ft } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 1.7 | 1.7 | 0.5 | 12.7 | 7.4 | 2 | 67.8 | 82.2 | 51.2 | 134.5 | 163.0 | 101.6 |
|  | 0.0 | 1.7 | 1.7 | 0.5 | 12.7 | 7.4 | 2 | 67.8 | 82.2 | 51.4 | 134.5 | 163.1 | 102.0 |
|  | 0.0 | 1.7 | 1.7 | 0.5 | 12.7 | 6.8 | 2 | 67.8 | 82.3 | 51.6 | 134.5 | 163.2 | 102.4 |
|  | 0.0 | 1.5 | 1.5 | 0.5 | 12.7 | 6.8 | 2 | 67.8 | 82.3 | 51.8 | 134.5 | 163.2 | 102.8 |
|  | 0.0 | 1.5 | 1.5 | 0.4 | 12.7 | 6.8 | 2 | 67.8 | 82.3 | 52.0 | 134.5 | 163.3 | 103.2 |
|  | 0.0 | 1.5 | 1.5 | 0.4 | 12.7 | 6.8 | 2 | 67.8 | 82.4 | 52.2 | 134.5 | 163.4 | 103.6 |
|  | 0.0 | 1.5 | 1.5 | 0.4 | 11.4 | 6.8 | 2 | 67.8 | 82.4 | 52.4 | 134.5 | 163.4 | 104.0 |
|  | 0.0 | 1.4 | 1.4 | 0.4 | 11.4 | 6.8 | 2 | 67.8 | 82.4 | 52.6 | 134.5 | 163.5 | 104.3 |
|  | 0.0 | 1.4 | 1.4 | 0.2 | 11.4 | 6.8 | 2 | 67.8 | 82.5 | 52.8 | 134.5 | 163.6 | 104.7 |
|  | 0.0 | 1.4 | 1.4 | 0.2 | 11.4 | 6.8 | 2 | 67.8 | 82.5 | 53.0 | 134.5 | 163.6 | 105.1 |
|  | 0.0 | 1.4 | 1.4 | 0.2 | 11.4 | 6.8 | 2 | 67.8 | 82.5 | 53.2 | 134.5 | 163.7 | 105.5 |
|  | 0.0 | 1.4 | 1.4 | 0.2 | 11.4 | 6.8 | 2 | 67.8 | 82.6 | 53.4 | 134.5 | 163.8 | 105.8 |
|  | 0.0 | 1.2 | 1.2 | 0.2 | 11.4 | 6.8 | 2 | 67.8 | 82.6 | 53.5 | 134.5 | 163.8 | 106.2 |
|  | 0.0 | 1.3 | 1.3 | 0.1 | 11.4 | 6.8 | 2 | 67.8 | 82.6 | 53.7 | 134.5 | 163.9 | 106.6 |
|  | 0.0 | 1.3 | 1.3 | 0.1 | 11.4 | 6.8 | 2 | 67.8 | 82.6 | 53.9 | 134.5 | 163.9 | 107.0 |
|  | 0.0 | 1.3 | 1.3 | 0.1 | 11.4 | 6.2 | 2 | 67.8 | 82.7 | 54.1 | 134.5 | 164.0 | 107.3 |
| 3 | 0.0 | 1.1 | 1.1 | 0.1 | 10.1 | 6.2 | 3 | 67.8 | 82.7 | 54.3 | 134.5 | 164.0 | 107.7 |
|  | 0.0 | 1.1 | 1.1 | 0.1 | 10.1 | 6.2 | 3 | 67.8 | 82.7 | 54.4 | 134.5 | 164.1 | 108.0 |
|  | 0.0 | 1.1 | 1.1 | 0.0 | 10.1 | 6.2 | 3 | 67.8 | 82.7 | 54.6 | 134.5 | 164.1 | 108.3 |
|  | 0.0 | 1.1 | 1.1 | 0.0 | 10.1 | 6.2 | 3 | 67.8 | 82.8 | 54.8 | 134.5 | 164.2 | 108.7 |
|  | 0.0 | 1.1 | 1.1 | 0.0 | 10.1 | 6.2 | 3 | 67.8 | 82.8 | 55.0 | 134.5 | 164.2 | 109.0 |
|  | 0.0 | 1.0 | 1.0 | 0.0 | 10.1 | 6.2 | 3 | 67.8 | 82.8 | 55.1 | 134.5 | 164.2 | 109.3 |
|  | 0.0 | 1.0 | 1.0 | 0.0 | 10.1 | 6.2 | 3 | 67.8 | 82.8 | 55.3 | 134.5 | 164.3 | 109.7 |
|  | 0.0 | 1.0 | 1.0 | 0.0 | 10.1 | 6.2 | 3 | 67.8 | 82.8 | 55.5 | 134.5 | 164.3 | 110.0 |
|  | 0.0 | 1.0 | 1.0 | 0.0 | 10.1 | 6.2 | 3 | 67.8 | 82.9 | 55.6 | 134.5 | 164.4 | 110.4 |
|  | 0.0 | 7.1 | 7.1 | 0.0 | 10.1 | 6.2 | 3 | 67.8 | 83.0 | 55.8 | 134.5 | 164.7 | 110.7 |
|  | 381.7 | 7.1 | 7.1 | 0.0 | 10.1 | 6.2 | 3 | 71.8 | 83.2 | 56.0 | 142.4 | 164.9 | 111.0 |
|  | 379.0 | 18.2 | 18.2 | 5.4 | 10.1 | 6.2 | 3 | 75.8 | 83.6 | 56.1 | 150.3 | 165.8 | 111.4 |
|  | 375.0 | 22.7 | 22.7 | 15.9 | 10.1 | 6.2 | 3 | 79.7 | 84.2 | 56.3 | 158.0 | 167.1 | 111.7 |
|  | 371.2 | 29.6 | 29.6 | 26.3 | 10.1 | 6.2 | 3 | 83.5 | 85.1 | 56.5 | 165.7 | 168.8 | 112.0 |
|  | 363.2 | 35.3 | 35.3 | 37.3 | 8.9 | 6.2 | 3 | 87.3 | 86.3 | 56.6 | 173.2 | 171.1 | 112.4 |
|  | 356.9 | 39.3 | 39.3 | 44.8 | 8.9 | 6.2 | 3 | 91.0 | 87.5 | 56.8 | 180.6 | 173.6 | 112.7 |
|  | 360.3 | 44.8 | 44.8 | 52.9 | 8.9 | 6.2 | 3 | 94.8 | 89.0 | 57.0 | 188.0 | 176.6 | 113.0 |
|  | 351.8 | 48.0 | 48.0 | 59.3 | 8.9 | 5.7 | 3 | 98.4 | 90.6 | 57.1 | 195.3 | 179.8 | 113.3 |
|  | 352.1 | 52.6 | 52.6 | 66.0 | 8.9 | 5.7 | 3 | 102.1 | 92.4 | 57.3 | 202.5 | 183.3 | 113.6 |
|  | 352.3 | 56.0 | 56.0 | 74.6 | 8.9 | 5.7 | 3 | 105.8 | 94.4 | 57.4 | 209.8 | 187.2 | 113.9 |
|  | 347.5 | 59.9 | 59.9 | 80.6 | 8.9 | 5.7 | 3 | 109.4 | 96.5 | 57.6 | 217.0 | 191.3 | 114.2 |
|  | 345.8 | 64.0 | 64.0 | 87.1 | 8.9 | 6.2 | 3 | 113.0 | 98.7 | 57.7 | 224.1 | 195.8 | 114.5 |
|  | 343.0 | 67.4 | 67.4 | 93.9 | 8.9 | 6.2 | 3 | 116.6 | 101.1 | 57.9 | 231.2 | 200.5 | 114.8 |
|  | 342.0 | 70.2 | 70.2 | 97.8 | 8.9 | 6.2 | 3 | 120.1 | 103.6 | 58.0 | 238.3 | 205.4 | 115.1 |
|  | 342.6 | 73.8 | 73.8 | 103.6 | 8.9 | 6.2 | 3 | 123.7 | 106.2 | 58.2 | 245.4 | 210.6 | 115.4 |
|  | 333.2 | 75.4 | 75.4 | 107.7 | 8.9 | 6.8 | 3 | 127.2 | 108.9 | 58.4 | 252.3 | 215.9 | 115.7 |
|  | 334.9 | 78.3 | 78.3 | 112.1 | 8.9 | 6.8 | 3 | 130.7 | 111.7 | 58.5 | 259.2 | 221.5 | 116.1 |
|  | 327.6 | 78.6 | 78.6 | 116.7 | 8.9 | 6.8 | 3 | 134.1 | 114.5 | 58.7 | 265.9 | 227.1 | 116.4 |
|  | 338.6 | 80.8 | 80.8 | 118.1 | 8.9 | 6.8 | 3 | 137.6 | 117.4 | 58.8 | 272.9 | 232.9 | 116.7 |
|  | 327.3 | 81.1 | 81.1 | 121.3 | 8.9 | 7.4 | 3 | 141.0 | 120.4 | 59.0 | 279.7 | 238.8 | 117.1 |
|  | 329.2 | 82.4 | 82.4 | 124.2 | 8.9 | 7.4 | 3 | 144.4 | 123.4 | 59.2 | 286.5 | 244.8 | 117.4 |
|  | 328.1 | 84.1 | 84.1 | 125.6 | 8.9 | 7.4 | 3 | 147.9 | 126.5 | 59.3 | 293.3 | 250.8 | 117.7 |
|  | 329.2 | 84.9 | 84.9 | 127.1 | 8.9 | 7.9 | 3 | 151.3 | 129.5 | 59.5 | 300.1 | 257.0 | 118.1 |
|  | 324.3 | 85.8 | 85.8 | 128.2 | 10.1 | 8.5 | 3 | 154.7 | 132.7 | 59.7 | 306.8 | 263.2 | 118.5 |


| Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \mathrm{G} 601 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \mathrm{G} 602 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \text { G603 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \mathrm{G} 354 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \text { G393 } \\ \text { cfs } \end{gathered}$ | Day | $\begin{gathered} \mathrm{G} 600 \\ \mathrm{cfs} \end{gathered}$ | $\begin{aligned} & \text { G601-3 } \\ & \mathrm{cfs} \end{aligned}$ | $\mathrm{G} 393+\mathrm{G} 354$ <br> Cfs | G600 $\mathrm{ac}-\mathrm{ft}$ | G601-3 $\mathrm{ac}-\mathrm{ft}$ | $\begin{gathered} \mathrm{G} 393+\mathrm{G} 354 \\ \text { ac-ft } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 326.5 | 87.2 | 87.2 | 129.6 | 10.1 | 8.5 | 3 | 158.1 | 135.8 | 59.9 | 313.5 | 269.4 | 118.8 |
|  | 334.3 | 86.6 | 86.6 | 131.5 | 10.1 | 9.2 | 3 | 161.6 | 139.0 | 60.1 | 320.4 | 275.7 | 119.2 |
|  | 333.5 | 87.5 | 87.5 | 133.0 | 10.1 | 9.2 | 3 | 165.0 | 142.2 | 60.3 | 327.3 | 282.1 | 119.6 |
|  | 328.9 | 88.9 | 88.9 | 134.5 | 11.4 | 9.8 | 3 | 168.5 | 145.5 | 60.5 | 334.1 | 288.5 | 120.1 |
|  | 338.0 | 89.8 | 89.8 | 134.1 | 11.4 | 10.4 | 3 | 172.0 | 148.7 | 60.8 | 341.1 | 295.0 | 120.5 |
|  | 336.4 | 89.2 | 89.2 | 135.6 | 11.4 | 10.4 | 3 | 175.5 | 152.0 | 61.0 | 348.1 | 301.5 | 121.0 |
|  | 323.2 | 90.7 | 90.7 | 137.1 | 12.7 | 11.1 | 3 | 178.8 | 155.3 | 61.2 | 354.7 | 308.1 | 121.5 |
|  | 333.5 | 90.7 | 90.7 | 137.1 | 12.7 | 11.8 | 3 | 182.3 | 158.6 | 61.5 | 361.6 | 314.7 | 122.0 |
|  | 330.5 | 90.1 | 90.1 | 138.6 | 12.7 | 11.8 | 3 | 185.8 | 162.0 | 61.7 | 368.5 | 321.3 | 122.5 |
|  | 327.5 | 91.6 | 91.6 | 138.2 | 12.7 | 12.5 | 3 | 189.2 | 165.3 | 62.0 | 375.2 | 327.9 | 123.0 |
|  | 327.3 | 91.0 | 91.0 | 138.2 | 14.1 | 13.1 | 3 | 192.6 | 168.7 | 62.3 | 382.0 | 334.5 | 123.6 |
|  | 323.9 | 91.0 | 91.0 | 139.7 | 15.5 | 13.9 | 3 | 196.0 | 172.0 | 62.6 | 388.7 | 341.2 | 124.2 |
|  | 319.0 | 91.8 | 91.8 | 139.3 | 15.5 | 14.6 | 3 | 199.3 | 175.4 | 62.9 | 395.3 | 347.8 | 124.8 |
|  | 323.3 | 91.8 | 91.8 | 139.3 | 15.5 | 15.3 | 3 | 202.6 | 178.7 | 63.2 | 402.0 | 354.5 | 125.4 |
|  | 326.2 | 90.4 | 90.4 | 138.8 | 17.0 | 15.3 | 3 | 206.0 | 182.1 | 63.6 | 408.7 | 361.1 | 126.1 |
|  | 318.1 | 90.4 | 90.4 | 138.8 | 17.0 | 16.1 | 3 | 209.4 | 185.4 | 63.9 | 415.3 | 367.7 | 126.8 |
|  | 315.4 | 90.4 | 90.4 | 138.8 | 17.0 | 16.8 | 3 | 212.6 | 188.7 | 64.3 | 421.8 | 374.3 | 127.5 |
|  | 316.7 | 90.4 | 90.4 | 136.4 | 17.0 | 17.6 | 3 | 215.9 | 192.0 | 64.6 | 428.3 | 380.9 | 128.2 |
|  | 314.5 | 88.9 | 88.9 | 136.4 | 18.5 | 17.6 | 3 | 219.2 | 195.3 | 65.0 | 434.8 | 387.4 | 128.9 |
|  | 316.2 | 88.9 | 88.9 | 136.4 | 18.5 | 18.4 | 3 | 222.5 | 198.6 | 65.4 | 441.4 | 393.9 | 129.7 |
|  | 315.5 | 88.3 | 88.3 | 136.4 | 18.5 | 19.1 | 3 | 225.8 | 201.8 | 65.8 | 447.9 | 400.3 | 130.5 |
|  | 317.4 | 89.8 | 89.8 | 136.4 | 20.1 | 19.9 | 3 | 229.1 | 205.1 | 66.2 | 454.4 | 406.9 | 131.3 |
|  | 314.9 | 88.3 | 88.3 | 135.9 | 21.7 | 21.6 | 3 | 232.4 | 208.4 | 66.6 | 460.9 | 413.3 | 132.2 |
|  | 317.4 | 88.3 | 88.3 | 135.5 | 21.7 | 22.4 | 3 | 235.7 | 211.6 | 67.1 | 467.5 | 419.8 | 133.1 |
|  | 316.4 | 88.3 | 88.3 | 135.5 | 23.3 | 23.2 | 3 | 239.0 | 214.9 | 67.6 | 474.0 | 426.2 | 134.1 |
|  | 318.7 | 86.9 | 86.9 | 133.5 | 23.3 | 23.2 | 3 | 242.3 | 218.1 | 68.1 | 480.6 | 432.6 | 135.0 |
|  | 312.6 | 86.9 | 86.9 | 133.5 | 23.3 | 24.1 | 3 | 245.6 | 221.3 | 68.6 | 487.1 | 438.9 | 136.0 |
|  | 307.3 | 86.9 | 86.9 | 133.5 | 25.0 | 24.1 | 3 | 248.8 | 224.5 | 69.1 | 493.4 | 445.3 | 137.0 |
|  | 317.5 | 87.1 | 87.1 | 131.6 | 25.0 | 25.0 | 3 | 252.1 | 227.7 | 69.6 | 500.0 | 451.6 | 138.0 |
|  | 318.0 | 89.4 | 89.4 | 133.0 | 26.7 | 25.8 | 3 | 255.4 | 230.9 | 70.1 | 506.6 | 458.0 | 139.1 |
|  | 307.8 | 87.1 | 87.1 | 135.5 | 30.3 | 27.6 | 3 | 258.6 | 234.1 | 70.7 | 512.9 | 464.4 | 140.3 |
|  | 316.2 | 88.8 | 88.8 | 133.5 | 32.1 | 28.5 | 3 | 261.9 | 237.4 | 71.4 | 519.4 | 470.8 | 141.6 |
|  | 312.4 | 87.3 | 87.3 | 134.9 | 34.0 | 30.3 | 3 | 265.1 | 240.6 | 72.1 | 525.9 | 477.2 | 142.9 |
|  | 318.4 | 86.5 | 86.5 | 133.0 | 34.0 | 31.3 | 3 | 268.5 | 243.8 | 72.7 | 532.5 | 483.6 | 144.3 |
|  | 310.5 | 86.5 | 86.5 | 133.0 | 35.9 | 32.2 | 3 | 271.7 | 247.0 | 73.4 | 538.9 | 489.9 | 145.7 |
|  | 313.8 | 85.0 | 85.0 | 133.0 | 37.8 | 32.2 | 3 | 275.0 | 250.1 | 74.2 | 545.4 | 496.1 | 147.1 |
|  | 315.7 | 86.5 | 86.5 | 130.5 | 37.8 | 32.2 | 3 | 278.2 | 253.3 | 74.9 | 551.9 | 502.4 | 148.6 |
|  | 310.5 | 86.5 | 86.5 | 130.5 | 39.8 | 33.2 | 3 | 281.5 | 256.5 | 75.7 | 558.3 | 508.7 | 150.1 |
|  | 305.4 | 85.0 | 85.0 | 130.5 | 39.8 | 34.1 | 3 | 284.7 | 259.6 | 76.4 | 564.6 | 514.9 | 151.6 |
|  | 311.4 | 85.0 | 85.0 | 130.0 | 41.7 | 34.1 | 3 | 287.9 | 262.7 | 77.2 | 571.1 | 521.1 | 153.2 |
|  | 308.8 | 85.0 | 85.0 | 130.0 | 41.7 | 35.1 | 3 | 291.1 | 265.8 | 78.0 | 577.4 | 527.3 | 154.7 |
|  | 303.2 | 83.6 | 83.6 | 128.1 | 43.8 | 35.1 | 3 | 294.3 | 268.9 | 78.8 | 583.7 | 533.4 | 156.4 |
|  | 308.9 | 83.6 | 83.6 | 128.1 | 43.8 | 36.0 | 3 | 297.5 | 272.0 | 79.7 | 590.1 | 539.5 | 158.0 |
|  | 311.0 | 84.2 | 84.2 | 128.1 | 45.8 | 36.0 | 3 | 300.7 | 275.1 | 80.5 | 596.5 | 545.6 | 159.7 |
|  | 308.2 | 83.6 | 83.6 | 126.2 | 45.8 | 37.0 | 3 | 303.9 | 278.1 | 81.4 | 602.9 | 551.7 | 161.4 |
|  | 314.0 | 83.6 | 83.6 | 127.6 | 47.9 | 39.0 | 3 | 307.2 | 281.2 | 82.3 | 609.4 | 557.8 | 163.2 |
|  | 306.1 | 84.4 | 84.4 | 127.6 | 50.1 | 40.0 | 3 | 310.4 | 284.3 | 83.2 | 615.7 | 563.9 | 165.1 |
|  | 310.7 | 87.0 | 87.0 | 127.0 | 50.1 | 41.0 | 3 | 313.6 | 287.4 | 84.2 | 622.1 | 570.1 | 167.0 |
|  | 311.6 | 94.4 | 94.4 | 128.9 | 58.8 | 43.1 | 3 | 316.9 | 290.7 | 85.2 | 628.6 | 576.7 | 169.1 |
|  | 315.3 | 95.4 | 95.4 | 138.7 | 75.3 | 49.5 | 3 | 320.2 | 294.2 | 86.5 | 635.1 | 583.5 | 171.7 |


| Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \mathrm{G} 601 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \mathrm{G} 602 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \text { G603 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \mathrm{G} 354 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \mathrm{G} 393 \\ \mathrm{cfs} \end{gathered}$ | Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{aligned} & \text { G601-3 } \\ & \mathrm{cfs} \end{aligned}$ | G393+G354 <br> Cfs | G600 $\mathrm{ac}-\mathrm{ft}$ | G601-3 $\mathrm{ac}-\mathrm{ft}$ | $\begin{gathered} \mathrm{G} 393+\mathrm{G} 354 \\ \mathrm{ac}-\mathrm{ft} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 314.6 | 98.9 | 98.9 | 146.7 | 93.0 | 53.9 | 3 | 323.5 | 297.8 | 88.1 | 641.6 | 590.6 | 174.7 |
|  | 313.5 | 104.9 | 104.9 | 148.2 | 103.7 | 56.1 | 3 | 326.7 | 301.5 | 89.7 | 648.0 | 598.0 | 178.0 |
|  | 324.7 | 102.4 | 102.4 | 153.3 | 123.2 | 64.2 | 3 | 330.1 | 305.2 | 91.7 | 654.8 | 605.4 | 181.9 |
|  | 323.6 | 103.3 | 103.3 | 151.0 | 134.9 | 68.9 | 3 | 333.5 | 308.9 | 93.8 | 661.4 | 612.8 | 186.1 |
|  | 339.5 | 102.5 | 102.5 | 152.2 | 146.9 | 71.4 | 3 | 337.0 | 312.7 | 96.1 | 668.5 | 620.2 | 190.6 |
|  | 340.7 | 103.3 | 103.3 | 152.8 | 156.1 | 73.8 | 3 | 340.6 | 316.4 | 98.5 | 675.5 | 627.6 | 195.3 |
|  | 343.7 | 105.0 | 105.0 | 152.5 | 168.6 | 77.6 | 3 | 344.1 | 320.2 | 101.0 | 682.6 | 635.1 | 200.4 |
|  | 361.2 | 108.6 | 108.6 | 162.1 | 184.8 | 82.6 | 3 | 347.9 | 324.1 | 103.8 | 690.1 | 642.9 | 205.9 |
|  | 364.5 | 105.8 | 105.8 | 163.2 | 201.3 | 91.7 | 3 | 351.7 | 328.0 | 106.9 | 697.6 | 650.7 | 212.0 |
|  | 365.6 | 108.3 | 108.3 | 157.3 | 211.5 | 94.4 | 3 | 355.5 | 331.9 | 110.1 | 705.1 | 658.4 | 218.3 |
|  | 377.0 | 110.5 | 110.5 | 158.5 | 225.3 | 99.8 | 3 | 359.4 | 335.9 | 113.5 | 712.9 | 666.2 | 225.0 |
|  | 374.8 | 119.4 | 119.4 | 164.8 | 250.1 | 109.4 | 3 | 363.3 | 340.1 | 117.2 | 720.7 | 674.6 | 232.5 |
| 4 | 382.2 | 116.3 | 116.3 | 165.4 | 287.0 | 121.8 | 4 | 367.3 | 344.2 | 121.5 | 728.6 | 682.8 | 240.9 |
|  | 384.9 | 111.4 | 111.4 | 160.2 | 300.1 | 129.8 | 4 | 371.3 | 348.2 | 125.9 | 736.5 | 690.7 | 249.8 |
|  | 391.9 | 112.2 | 112.2 | 156.1 | 305.0 | 136.1 | 4 | 375.4 | 352.2 | 130.5 | 744.6 | 698.6 | 258.9 |
|  | 389.9 | 109.9 | 109.9 | 149.3 | 312.2 | 136.9 | 4 | 379.5 | 356.0 | 135.2 | 752.7 | 706.2 | 268.2 |
|  | 399.8 | 107.0 | 107.0 | 144.6 | 323.6 | 143.6 | 4 | 383.6 | 359.8 | 140.1 | 760.9 | 713.6 | 277.8 |
|  | 393.3 | 107.0 | 107.0 | 140.2 | 334.9 | 145.6 | 4 | 387.7 | 363.5 | 145.1 | 769.1 | 720.9 | 287.8 |
|  | 396.5 | 100.1 | 100.1 | 132.9 | 340.7 | 148.4 | 4 | 391.9 | 366.9 | 150.2 | 777.3 | 727.8 | 297.9 |
|  | 393.7 | 101.3 | 101.3 | 127.2 | 340.0 | 149.7 | 4 | 396.0 | 370.4 | 155.3 | 785.4 | 734.6 | 308.0 |
|  | 400.2 | 100.1 | 100.1 | 124.3 | 347.3 | 150.9 | 4 | 400.1 | 373.7 | 160.5 | 793.7 | 741.3 | 318.3 |
|  | 400.9 | 97.3 | 97.3 | 120.7 | 349.8 | 155.1 | 4 | 404.3 | 377.0 | 165.7 | 801.9 | 747.8 | 328.7 |
|  | 395.4 | 96.5 | 96.5 | 114.8 | 353.0 | 154.7 | 4 | 408.4 | 380.2 | 171.0 | 810.1 | 754.2 | 339.2 |
|  | 399.2 | 95.5 | 95.5 | 111.8 | 353.0 | 156.3 | 4 | 412.6 | 383.4 | 176.3 | 818.4 | 760.4 | 349.7 |
|  | 399.9 | 97.6 | 97.6 | 111.8 | 360.4 | 156.0 | 4 | 416.7 | 386.6 | 181.7 | 826.6 | 766.8 | 360.4 |
|  | 397.9 | 94.2 | 94.2 | 109.6 | 369.4 | 159.5 | 4 | 420.9 | 389.7 | 187.2 | 834.8 | 772.9 | 371.3 |
|  | 401.4 | 99.1 | 99.1 | 110.6 | 376.8 | 160.8 | 4 | 425.1 | 392.9 | 192.8 | 843.1 | 779.3 | 382.4 |
|  | 401.8 | 97.2 | 97.2 | 107.4 | 375.0 | 164.0 | 4 | 429.3 | 396.0 | 198.4 | 851.4 | 785.6 | 393.6 |
|  | 407.6 | 102.5 | 102.5 | 108.9 | 389.9 | 167.4 | 4 | 433.5 | 399.3 | 204.2 | 859.9 | 792.1 | 405.1 |
|  | 402.8 | 99.6 | 99.6 | 109.2 | 405.3 | 172.1 | 4 | 437.7 | 402.5 | 210.2 | 868.2 | 798.4 | 417.0 |
|  | 409.0 | 101.9 | 101.9 | 104.8 | 415.1 | 175.9 | 4 | 442.0 | 405.7 | 216.4 | 876.6 | 804.8 | 429.2 |
|  | 407.1 | 99.6 | 99.6 | 105.7 | 420.5 | 178.4 | 4 | 446.2 | 408.9 | 222.6 | 885.0 | 811.1 | 441.6 |
|  | 407.0 | 96.6 | 96.6 | 101.9 | 429.3 | 180.1 | 4 | 450.4 | 412.0 | 229.0 | 893.4 | 817.2 | 454.2 |
|  | 407.6 | 95.9 | 95.9 | 98.0 | 429.3 | 181.8 | 4 | 454.7 | 415.0 | 235.3 | 901.9 | 823.2 | 466.8 |
|  | 403.5 | 95.1 | 95.1 | 97.2 | 430.4 | 183.9 | 4 | 458.9 | 418.0 | 241.7 | 910.2 | 829.1 | 479.5 |
|  | 403.1 | 94.4 | 94.4 | 96.3 | 430.4 | 183.9 | 4 | 463.1 | 421.0 | 248.1 | 918.5 | 835.0 | 492.2 |
|  | 382.0 | 92.1 | 92.1 | 88.3 | 427.1 | 184.3 | 4 | 467.1 | 423.8 | 254.5 | 926.4 | 840.6 | 504.8 |
|  | 382.9 | 93.6 | 93.6 | 88.3 | 427.1 | 184.3 | 4 | 471.1 | 426.7 | 260.9 | 934.3 | 846.3 | 517.5 |
|  | 382.7 | 92.1 | 92.1 | 91.6 | 428.2 | 184.7 | 4 | 475.0 | 429.6 | 267.3 | 942.2 | 852.0 | 530.1 |
|  | 384.2 | 93.6 | 93.6 | 88.3 | 428.2 | 184.7 | 4 | 479.0 | 432.4 | 273.7 | 950.2 | 857.7 | 542.8 |
|  | 385.4 | 93.6 | 93.6 | 88.3 | 429.3 | 185.1 | 4 | 483.1 | 435.3 | 280.1 | 958.1 | 863.4 | 555.5 |
|  | 383.7 | 92.9 | 92.9 | 87.6 | 429.3 | 185.1 | 4 | 487.1 | 438.2 | 286.5 | 966.1 | 869.1 | 568.2 |
|  | 383.7 | 90.7 | 90.7 | 87.6 | 430.4 | 185.5 | 4 | 491.1 | 441.0 | 292.9 | 974.0 | 874.6 | 580.9 |
|  | 386.2 | 92.1 | 92.1 | 83.4 | 427.0 | 185.9 | 4 | 495.1 | 443.7 | 299.3 | 982.0 | 880.2 | 593.6 |
|  | 388.1 | 92.1 | 92.1 | 86.8 | 427.0 | 186.3 | 4 | 499.1 | 446.6 | 305.6 | 990.0 | 885.8 | 606.2 |
|  | 383.7 | 91.4 | 91.4 | 86.8 | 423.7 | 186.3 | 4 | 503.1 | 449.4 | 312.0 | 997.9 | 891.3 | 618.8 |
|  | 385.6 | 91.4 | 91.4 | 82.7 | 424.7 | 186.6 | 4 | 507.1 | 452.1 | 318.4 | 1005.9 | 896.8 | 631.5 |
|  | 383.9 | 91.4 | 91.4 | 82.7 | 421.4 | 185.0 | 4 | 511.1 | 454.9 | 324.7 | 1013.8 | 902.3 | 644.0 |
|  | 387.9 | 92.8 | 92.8 | 86.1 | 418.0 | 185.3 | 4 | 515.2 | 457.7 | 331.0 | 1021.8 | 907.9 | 656.5 |
|  | 383.9 | 90.7 | 90.7 | 86.1 | 418.0 | 185.7 | 4 | 519.2 | 460.5 | 337.3 | 1029.8 | 913.4 | 668.9 |


| Day | $\begin{gathered} \hline \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \mathrm{G} 601 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \mathrm{G} 602 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \hline \text { G603 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G354 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \mathrm{G} 393 \\ \mathrm{cfs} \end{gathered}$ | Day | $\begin{gathered} \mathrm{G} 600 \\ \mathrm{cfs} \end{gathered}$ | $\begin{aligned} & \text { G601-3 } \\ & \mathrm{cfs} \end{aligned}$ | $\mathrm{G} 393+\mathrm{G} 354$ <br> Cfs | G600 $\mathrm{ac}-\mathrm{ft}$ | G601-3 $\mathrm{ac}-\mathrm{ft}$ | $\begin{gathered} \mathrm{G} 393+\mathrm{G} 354 \\ \mathrm{ac}-\mathrm{ft} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 383.7 | 92.8 | 92.8 | 82.0 | 414.7 | 184.0 | 4 | 523.2 | 463.3 | 343.5 | 1037.7 | 919.0 | 681.3 |
|  | 397.2 | 92.0 | 92.0 | 82.0 | 414.7 | 184.4 | 4 | 527.3 | 466.1 | 349.7 | 1045.9 | 924.5 | 693.7 |
|  | 397.2 | 92.0 | 92.0 | 85.3 | 411.3 | 184.7 | 4 | 531.4 | 468.9 | 355.9 | 1054.1 | 930.0 | 706.0 |
|  | 397.2 | 92.0 | 92.0 | 85.3 | 412.3 | 183.0 | 4 | 535.6 | 471.7 | 362.1 | 1062.3 | 935.6 | 718.3 |
|  | 399.1 | 92.0 | 92.0 | 85.3 | 408.9 | 183.4 | 4 | 539.7 | 474.5 | 368.3 | 1070.6 | 941.2 | 730.5 |
|  | 397.2 | 93.4 | 93.4 | 85.3 | 408.9 | 183.4 | 4 | 543.9 | 477.3 | 374.5 | 1078.8 | 946.8 | 742.8 |
|  | 397.4 | 93.4 | 93.4 | 85.3 | 405.6 | 183.4 | 4 | 548.0 | 480.2 | 380.6 | 1087.0 | 952.4 | 755.0 |
|  | 399.2 | 88.5 | 88.5 | 88.4 | 405.6 | 182.1 | 4 | 552.2 | 482.9 | 386.7 | 1095.2 | 957.9 | 767.1 |
|  | 418.7 | 93.4 | 93.4 | 88.4 | 402.2 | 182.1 | 4 | 556.5 | 485.8 | 392.8 | 1103.9 | 963.6 | 779.2 |
|  | 431.6 | 90.6 | 90.6 | 83.8 | 402.2 | 182.1 | 4 | 561.0 | 488.6 | 398.9 | 1112.8 | 969.0 | 791.2 |
|  | 428.0 | 94.7 | 94.7 | 83.8 | 397.9 | 182.1 | 4 | 565.5 | 491.4 | 405.0 | 1121.7 | 974.7 | 803.2 |
|  | 431.4 | 94.7 | 94.7 | 88.4 | 397.9 | 182.4 | 4 | 570.0 | 494.3 | 411.0 | 1130.6 | 980.4 | 815.2 |
|  | 421.9 | 94.7 | 94.7 | 88.4 | 393.7 | 180.7 | 4 | 574.4 | 497.2 | 417.0 | 1139.3 | 986.2 | 827.1 |
|  | 429.6 | 94.7 | 94.7 | 88.4 | 393.7 | 180.7 | 4 | 578.9 | 500.1 | 423.0 | 1148.2 | 991.9 | 839.0 |
|  | 425.7 | 96.0 | 96.0 | 88.4 | 389.5 | 180.4 | 4 | 583.3 | 503.0 | 428.9 | 1157.0 | 997.7 | 850.7 |
|  | 425.7 | 96.0 | 96.0 | 91.4 | 389.5 | 180.4 | 4 | 587.7 | 506.0 | 434.8 | 1165.7 | 1003.6 | 862.5 |
|  | 425.7 | 96.0 | 96.0 | 91.4 | 389.5 | 178.7 | 4 | 592.2 | 508.9 | 440.8 | 1174.5 | 1009.4 | 874.2 |
|  | 419.5 | 96.0 | 96.0 | 91.4 | 385.2 | 178.7 | 4 | 596.5 | 511.9 | 446.6 | 1183.2 | 1015.3 | 885.9 |
|  | 425.6 | 96.0 | 96.0 | 91.4 | 384.3 | 178.7 | 4 | 601.0 | 514.8 | 452.5 | 1192.0 | 1021.1 | 897.5 |
|  | 426.5 | 96.0 | 96.0 | 91.4 | 380.1 | 178.7 | 4 | 605.4 | 517.8 | 458.3 | 1200.8 | 1027.0 | 909.1 |
|  | 425.7 | 96.0 | 96.0 | 91.4 | 379.2 | 178.7 | 4 | 609.8 | 520.7 | 464.1 | 1209.6 | 1032.8 | 920.6 |
|  | 425.9 | 97.3 | 97.3 | 91.4 | 375.0 | 178.4 | 4 | 614.3 | 523.7 | 469.9 | 1218.4 | 1038.8 | 932.0 |
|  | 425.7 | 97.3 | 97.3 | 91.4 | 375.0 | 176.7 | 4 | 618.7 | 526.7 | 475.6 | 1227.2 | 1044.7 | 943.4 |
|  | 421.8 | 97.3 | 97.3 | 91.4 | 375.0 | 176.7 | 4 | 623.1 | 529.7 | 481.4 | 1235.9 | 1050.6 | 954.8 |
|  | 423.4 | 97.3 | 97.3 | 94.2 | 370.8 | 176.4 | 4 | 627.5 | 532.7 | 487.1 | 1244.7 | 1056.5 | 966.1 |
|  | 425.7 | 97.3 | 97.3 | 94.2 | 369.8 | 176.4 | 4 | 631.9 | 535.7 | 492.8 | 1253.5 | 1062.5 | 977.4 |
|  | 429.4 | 96.5 | 96.5 | 90.6 | 369.8 | 176.4 | 4 | 636.4 | 538.6 | 498.5 | 1262.3 | 1068.4 | 988.7 |
|  | 427.3 | 96.5 | 96.5 | 90.6 | 365.6 | 176.4 | 4 | 640.9 | 541.6 | 504.1 | 1271.2 | 1074.2 | 999.9 |
|  | 433.1 | 96.5 | 96.5 | 90.6 | 365.6 | 176.4 | 4 | 645.4 | 544.5 | 509.8 | 1280.1 | 1080.1 | 1011.1 |
|  | 425.2 | 96.5 | 96.5 | 90.6 | 365.6 | 176.4 | 4 | 649.8 | 547.5 | 515.4 | 1288.9 | 1085.9 | 1022.3 |
|  | 426.9 | 96.5 | 96.5 | 90.6 | 361.5 | 174.7 | 4 | 654.3 | 550.4 | 521.0 | 1297.7 | 1091.8 | 1033.4 |
|  | 428.2 | 96.5 | 96.5 | 93.4 | 361.5 | 174.7 | 4 | 658.7 | 553.4 | 526.6 | 1306.6 | 1097.7 | 1044.5 |
|  | 430.0 | 97.7 | 97.7 | 93.4 | 361.5 | 174.7 | 4 | 663.2 | 556.4 | 532.2 | 1315.5 | 1103.7 | 1055.5 |
|  | 433.6 | 97.7 | 97.7 | 93.4 | 357.3 | 174.7 | 4 | 667.7 | 559.4 | 537.7 | 1324.4 | 1109.6 | 1066.5 |
|  | 434.9 | 97.7 | 97.7 | 93.4 | 357.3 | 174.7 | 4 | 672.2 | 562.4 | 543.2 | 1333.4 | 1115.6 | 1077.5 |
|  | 430.5 | 97.7 | 97.7 | 93.4 | 357.3 | 174.7 | 4 | 676.7 | 565.4 | 548.8 | 1342.3 | 1121.6 | 1088.5 |
|  | 427.4 | 97.7 | 97.7 | 89.8 | 357.3 | 174.7 | 4 | 681.2 | 568.4 | 554.3 | 1351.1 | 1127.5 | 1099.5 |
|  | 429.3 | 96.9 | 96.9 | 89.8 | 353.2 | 174.7 | 4 | 685.7 | 571.4 | 559.8 | 1360.0 | 1133.3 | 1110.4 |
|  | 433.1 | 95.7 | 95.7 | 92.6 | 354.2 | 173.1 | 4 | 690.2 | 574.3 | 565.3 | 1368.9 | 1139.2 | 1121.3 |
|  | 430.5 | 96.9 | 96.9 | 92.6 | 354.2 | 173.1 | 4 | 694.6 | 577.3 | 570.8 | 1377.8 | 1145.1 | 1132.2 |
|  | 427.7 | 96.9 | 96.9 | 92.6 | 350.0 | 173.1 | 4 | 699.1 | 580.3 | 576.3 | 1386.7 | 1151.0 | 1143.0 |
|  | 435.1 | 98.1 | 98.1 | 92.6 | 350.0 | 173.1 | 4 | 703.6 | 583.3 | 581.7 | 1395.7 | 1157.0 | 1153.8 |
|  | 435.1 | 96.9 | 96.9 | 92.6 | 350.0 | 173.1 | 4 | 708.2 | 586.3 | 587.2 | 1404.7 | 1162.9 | 1164.6 |
|  | 434.9 | 98.1 | 98.1 | 92.6 | 350.0 | 173.1 | 4 | 712.7 | 589.3 | 592.6 | 1413.6 | 1168.9 | 1175.4 |
|  | 435.1 | 98.1 | 98.1 | 92.6 | 345.9 | 173.4 | 4 | 717.2 | 592.3 | 598.0 | 1422.6 | 1174.8 | 1186.2 |
|  | 432.6 | 98.1 | 98.1 | 92.6 | 345.9 | 171.8 | 4 | 721.7 | 595.3 | 603.4 | 1431.6 | 1180.8 | 1196.9 |
|  | 428.9 | 98.1 | 98.1 | 95.2 | 345.9 | 171.8 | 4 | 726.2 | 598.3 | 608.8 | 1440.4 | 1186.8 | 1207.6 |
|  | 427.4 | 98.1 | 98.1 | 95.2 | 341.8 | 171.8 | 4 | 730.7 | 601.4 | 614.2 | 1449.3 | 1192.8 | 1218.2 |
|  | 431.0 | 97.3 | 97.3 | 91.7 | 341.8 | 171.8 | 4 | 735.1 | 604.4 | 619.5 | 1458.2 | 1198.7 | 1228.8 |
|  | 434.8 | 99.2 | 99.2 | 91.7 | 342.8 | 171.8 | 4 | 739.7 | 607.4 | 624.9 | 1467.1 | 1204.7 | 1239.4 |



| Day | $\begin{gathered} \hline \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \text { G601 } \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \hline \text { G602 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G603 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G354 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G393 } \\ \text { cfs } \end{gathered}$ | Day | $\begin{gathered} \hline \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \text { G601-3 } \\ \text { cfs } \end{gathered}$ | $\begin{aligned} & \text { G393+G354 } \\ & \text { Cfs } \end{aligned}$ | $\begin{gathered} \hline \text { G600 } \\ \text { ac-ft } \end{gathered}$ | $\begin{gathered} \hline \text { G601-3 } \\ \text { ac-ft } \end{gathered}$ | $\begin{gathered} \text { G393+G354 } \\ \text { ac-ft } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 428.6 | 100.0 | 100.0 | 94.2 | 307.9 | 165.1 | 5 | 966.9 | 760.8 | 884.9 | 1917.9 | 1509.1 | 1755.1 |
|  | 420.5 | 99.0 | 99.0 | 94.2 | 308.6 | 165.1 | 5 | 971.3 | 763.9 | 889.8 | 1926.6 | 1515.1 | 1764.9 |
|  | 421.1 | 100.0 | 100.0 | 94.2 | 304.7 | 165.3 | 5 | 975.7 | 766.9 | 894.7 | 1935.3 | 1521.2 | 1774.6 |
|  | 418.7 | 99.0 | 99.0 | 94.2 | 304.7 | 165.3 | 5 | 980.1 | 770.0 | 899.6 | 1944.0 | 1527.2 | 1784.3 |
|  | 422.9 | 98.2 | 98.2 | 94.2 | 305.4 | 164.0 | 5 | 984.5 | 773.0 | 904.5 | 1952.7 | 1533.2 | 1794.0 |
|  | 418.9 | 98.2 | 98.2 | 96.5 | 305.4 | 164.0 | 5 | 988.8 | 776.0 | 909.4 | 1961.4 | 1539.3 | 1803.7 |
|  | 422.6 | 97.3 | 97.3 | 96.5 | 305.4 | 164.0 | 5 | 993.2 | 779.1 | 914.3 | 1970.1 | 1545.3 | 1813.4 |
|  | 420.4 | 95.5 | 95.5 | 86.8 | 301.5 | 164.0 | 5 | 997.6 | 782.0 | 919.1 | 1978.8 | 1551.0 | 1823.0 |
|  | 424.9 | 96.5 | 96.5 | 90.1 | 302.1 | 164.2 | 5 | 1002.0 | 784.9 | 924.0 | 1987.6 | 1556.9 | 1832.7 |
|  | 426.2 | 97.3 | 97.3 | 92.5 | 302.1 | 164.2 | 5 | 1006.5 | 787.9 | 928.8 | 1996.4 | 1562.8 | 1842.3 |
|  | 422.8 | 103.1 | 103.1 | 92.5 | 302.1 | 164.2 | 5 | 1010.9 | 791.0 | 933.7 | 2005.1 | 1569.0 | 1851.9 |
|  | 422.3 | 96.3 | 96.3 | 58.9 | 302.1 | 162.6 | 5 | 1015.3 | 793.6 | 938.5 | 2013.8 | 1574.2 | 1861.5 |
|  | 425.3 | 100.2 | 100.2 | 92.5 | 298.3 | 162.9 | 5 | 1019.7 | 796.7 | 943.3 | 2022.6 | 1580.2 | 1871.1 |
|  | 426.1 | 107.4 | 107.4 | 104.9 | 298.9 | 162.9 | 5 | 1024.2 | 800.0 | 948.1 | 2031.4 | 1586.8 | 1880.6 |
|  | 427.8 | 104.6 | 104.6 | 102.8 | 298.9 | 162.9 | 5 | 1028.6 | 803.3 | 952.9 | 2040.2 | 1593.3 | 1890.2 |
|  | 430.4 | 109.3 | 109.3 | 108.8 | 298.9 | 162.9 | 5 | 1033.1 | 806.7 | 957.7 | 2049.1 | 1600.0 | 1899.7 |
|  | 427.8 | 110.2 | 110.2 | 112.8 | 298.9 | 162.9 | 5 | 1037.5 | 810.1 | 962.6 | 2058.0 | 1606.9 | 1909.2 |
|  | 425.4 | 110.2 | 110.2 | 113.8 | 295.0 | 162.9 | 5 | 1042.0 | 813.6 | 967.3 | 2066.8 | 1613.8 | 1918.7 |
|  | 425.6 | 112.1 | 112.1 | 116.8 | 295.0 | 163.1 | 5 | 1046.4 | 817.2 | 972.1 | 2075.6 | 1620.9 | 1928.2 |
|  | 422.8 | 114.0 | 114.0 | 119.8 | 295.6 | 163.1 | 5 | 1050.8 | 820.8 | 976.9 | 2084.3 | 1628.1 | 1937.6 |
|  | 425.2 | 113.0 | 113.0 | 117.9 | 295.6 | 163.1 | 5 | 1055.2 | 824.4 | 981.7 | 2093.1 | 1635.2 | 1947.1 |
|  | 425.0 | 113.9 | 113.9 | 120.9 | 295.6 | 163.1 | 5 | 1059.7 | 828.0 | 986.4 | 2101.9 | 1642.4 | 1956.6 |
|  | 424.9 | 113.9 | 113.9 | 120.9 | 291.8 | 163.1 | 5 | 1064.1 | 831.7 | 991.2 | 2110.6 | 1649.6 | 1966.0 |
|  | 425.0 | 114.9 | 114.9 | 118.9 | 291.8 | 163.1 | 5 | 1068.5 | 835.3 | 995.9 | 2119.4 | 1656.8 | 1975.4 |
|  | 425.1 | 113.9 | 113.9 | 122.0 | 291.8 | 163.1 | 5 | 1073.0 | 838.9 | 1000.7 | 2128.2 | 1664.0 | 1984.8 |
|  | 422.5 | 113.9 | 113.9 | 122.0 | 291.8 | 163.4 | 5 | 1077.4 | 842.6 | 1005.4 | 2136.9 | 1671.2 | 1994.2 |
|  | 403.6 | 113.9 | 113.9 | 122.0 | 291.8 | 163.4 | 5 | 1081.6 | 846.2 | 1010.1 | 2145.3 | 1678.5 | 2003.6 |
|  | 403.5 | 113.9 | 113.9 | 118.9 | 292.4 | 163.4 | 5 | 1085.8 | 849.8 | 1014.9 | 2153.6 | 1685.6 | 2013.0 |
|  | 403.8 | 113.9 | 113.9 | 118.9 | 292.4 | 163.4 | 5 | 1090.0 | 853.4 | 1019.6 | 2162.0 | 1692.8 | 2022.4 |
|  | 406.4 | 112.0 | 112.0 | 118.9 | 292.4 | 163.4 | 5 | 1094.2 | 857.0 | 1024.4 | 2170.3 | 1699.9 | 2031.9 |
|  | 401.6 | 112.0 | 112.0 | 118.9 | 292.4 | 163.4 | 5 | 1098.4 | 860.6 | 1029.1 | 2178.6 | 1707.0 | 2041.3 |
|  | 406.4 | 112.0 | 112.0 | 118.9 | 288.6 | 163.4 | 5 | 1102.6 | 864.2 | 1033.8 | 2187.0 | 1714.0 | 2050.6 |
|  | 401.8 | 113.0 | 113.0 | 118.9 | 288.6 | 165.0 | 5 | 1106.8 | 867.7 | 1038.6 | 2195.3 | 1721.2 | 2060.0 |
|  | 404.4 | 113.0 | 113.0 | 118.9 | 288.6 | 165.2 | 5 | 1111.0 | 871.3 | 1043.3 | 2203.7 | 1728.3 | 2069.4 |
|  | 402.0 | 112.0 | 112.0 | 118.9 | 288.6 | 165.0 | 5 | 1115.2 | 874.9 | 1048.0 | 2212.0 | 1735.4 | 2078.7 |
|  | 406.7 | 112.0 | 112.0 | 118.9 | 288.6 | 165.2 | 5 | 1119.4 | 878.5 | 1052.7 | 2220.4 | 1742.5 | 2088.1 |
|  | 402.3 | 113.0 | 113.0 | 116.9 | 288.6 | 165.2 | 5 | 1123.6 | 882.1 | 1057.5 | 2228.7 | 1749.6 | 2097.5 |
|  | 404.7 | 112.0 | 112.0 | 116.9 | 288.6 | 165.2 | 5 | 1127.8 | 885.6 | 1062.2 | 2237.1 | 1756.6 | 2106.9 |
|  | 404.3 | 113.0 | 113.0 | 116.9 | 289.1 | 165.2 | 5 | 1132.1 | 889.2 | 1066.9 | 2245.4 | 1763.7 | 2116.2 |
|  | 407.0 | 113.0 | 113.0 | 116.9 | 289.1 | 165.2 | 5 | 1136.3 | 892.7 | 1071.7 | 2253.8 | 1770.8 | 2125.6 |
|  | 407.0 | 112.0 | 112.0 | 116.9 | 289.1 | 165.2 | 5 | 1140.5 | 896.3 | 1076.4 | 2262.3 | 1777.8 | 2135.0 |
|  | 404.6 | 112.0 | 112.0 | 116.9 | 289.1 | 165.2 | 5 | 1144.8 | 899.8 | 1081.1 | 2270.6 | 1784.8 | 2144.4 |
|  | 407.0 | 113.0 | 113.0 | 116.9 | 289.1 | 165.2 | 5 | 1149.0 | 903.4 | 1085.9 | 2279.0 | 1791.9 | 2153.8 |
|  | 406.7 | 113.0 | 113.0 | 116.9 | 289.1 | 166.8 | 5 | 1153.2 | 907.0 | 1090.6 | 2287.4 | 1799.0 | 2163.2 |
|  | 406.9 | 112.0 | 112.0 | 116.9 | 289.1 | 166.8 | 5 | 1157.5 | 910.5 | 1095.4 | 2295.8 | 1806.1 | 2172.6 |
|  | 406.7 | 113.0 | 113.0 | 116.9 | 289.1 | 166.8 | 5 | 1161.7 | 914.1 | 1100.1 | 2304.2 | 1813.1 | 2182.0 |
|  | 402.0 | 113.0 | 113.0 | 116.9 | 289.1 | 166.8 | 5 | 1165.9 | 917.7 | 1104.8 | 2312.5 | 1820.2 | 2191.5 |
|  | 404.6 | 112.0 | 112.0 | 113.8 | 289.1 | 166.8 | 5 | 1170.1 | 921.2 | 1109.6 | 2320.9 | 1827.2 | 2200.9 |
|  | 403.7 | 113.0 | 113.0 | 116.9 | 289.1 | 166.8 | 5 | 1174.3 | 924.8 | 1114.3 | 2329.2 | 1834.3 | 2210.3 |
|  | 400.6 | 112.0 | 112.0 | 113.8 | 285.4 | 166.8 | 5 | 1178.5 | 928.3 | 1119.1 | 2337.5 | 1841.3 | 2219.7 |



| Day | $\begin{gathered} \hline \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \text { G601 } \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \hline \text { G602 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G603 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G354 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G393 } \\ \text { cfs } \end{gathered}$ | Day | $\begin{gathered} \hline \text { G600 } \\ \text { cfs } \end{gathered}$ | G601-3 <br> cfs | $\begin{aligned} & \text { G393+G354 } \\ & \text { Cfs } \end{aligned}$ | $\begin{gathered} \hline \text { G600 } \\ \text { ac-ft } \end{gathered}$ | $\begin{gathered} \hline \text { G601-3 } \\ \text { ac-ft } \end{gathered}$ | $\begin{gathered} \text { G393+G354 } \\ \text { ac-ft } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 395.9 | 109.1 | 109.1 | 105.2 | 283.1 | 169.0 | 6 | 1391.8 | 1106.2 | 1359.7 | 2760.7 | 2194.1 | 2697.0 |
|  | 393.6 | 109.3 | 109.3 | 108.4 | 283.1 | 169.0 | 6 | 1395.9 | 1109.6 | 1364.4 | 2768.8 | 2200.8 | 2706.4 |
|  | 289.9 | 109.1 | 109.1 | 101.9 | 283.1 | 169.0 | 6 | 1398.9 | 1112.9 | 1369.2 | 2774.8 | 2207.5 | 2715.7 |
|  | 402.8 | 106.4 | 106.4 | 101.9 | 283.1 | 169.0 | 6 | 1403.1 | 1116.2 | 1373.9 | 2783.1 | 2214.0 | 2725.1 |
|  | 396.3 | 109.6 | 109.6 | 105.2 | 286.9 | 169.0 | 6 | 1407.3 | 1119.6 | 1378.6 | 2791.3 | 2220.7 | 2734.5 |
|  | 397.5 | 115.4 | 115.4 | 112.2 | 306.6 | 170.0 | 6 | 1411.4 | 1123.1 | 1383.6 | 2799.5 | 2227.7 | 2744.3 |
|  | 398.3 | 116.3 | 116.3 | 118.5 | 311.8 | 173.7 | 6 | 1415.5 | 1126.8 | 1388.6 | 2807.7 | 2235.0 | 2754.4 |
|  | 394.7 | 113.4 | 113.4 | 111.8 | 311.8 | 175.0 | 6 | 1419.7 | 1130.3 | 1393.7 | 2815.9 | 2242.0 | 2764.4 |
|  | 395.3 | 115.4 | 115.4 | 111.8 | 307.9 | 175.0 | 6 | 1423.8 | 1133.9 | 1398.7 | 2824.1 | 2249.1 | 2774.4 |
|  | 400.4 | 115.4 | 115.4 | 111.8 | 308.6 | 176.7 | 6 | 1427.9 | 1137.5 | 1403.8 | 2832.3 | 2256.1 | 2784.4 |
|  | 397.1 | 113.4 | 113.4 | 108.3 | 308.6 | 176.7 | 6 | 1432.1 | 1140.9 | 1408.9 | 2840.5 | 2263.1 | 2794.5 |
|  | 401.7 | 113.4 | 113.4 | 111.8 | 308.6 | 176.9 | 6 | 1436.3 | 1144.5 | 1413.9 | 2848.8 | 2270.1 | 2804.5 |
|  | 400.9 | 113.4 | 113.4 | 108.3 | 308.6 | 176.9 | 6 | 1440.4 | 1148.0 | 1419.0 | 2857.1 | 2277.0 | 2814.5 |
|  | 396.2 | 113.4 | 113.4 | 108.3 | 308.6 | 176.9 | 6 | 1444.6 | 1151.5 | 1424.0 | 2865.3 | 2283.9 | 2824.6 |
|  | 398.3 | 113.4 | 113.4 | 108.3 | 308.6 | 176.9 | 6 | 1448.7 | 1154.9 | 1429.1 | 2873.5 | 2290.8 | 2834.6 |
|  | 398.3 | 113.4 | 113.4 | 108.3 | 308.6 | 176.9 | 6 | 1452.9 | 1158.4 | 1434.1 | 2881.8 | 2297.8 | 2844.6 |
|  | 400.7 | 114.5 | 114.5 | 108.3 | 309.2 | 176.9 | 6 | 1457.0 | 1161.9 | 1439.2 | 2890.0 | 2304.7 | 2854.7 |
|  | 398.3 | 114.5 | 114.5 | 108.3 | 309.2 | 176.9 | 6 | 1461.2 | 1165.5 | 1444.3 | 2898.3 | 2311.7 | 2864.7 |
|  | 400.7 | 112.5 | 112.5 | 108.3 | 309.2 | 176.9 | 6 | 1465.4 | 1168.9 | 1449.3 | 2906.5 | 2318.6 | 2874.7 |
|  | 395.8 | 112.5 | 112.5 | 108.3 | 309.2 | 176.9 | 6 | 1469.5 | 1172.4 | 1454.4 | 2914.7 | 2325.5 | 2884.8 |
|  | 398.2 | 112.5 | 112.5 | 108.3 | 309.2 | 176.9 | 6 | 1473.6 | 1175.9 | 1459.5 | 2922.9 | 2332.4 | 2894.8 |
|  | 393.6 | 112.5 | 112.5 | 108.3 | 309.2 | 176.9 | 6 | 1477.7 | 1179.3 | 1464.5 | 2931.1 | 2339.2 | 2904.9 |
|  | 399.3 | 112.5 | 112.5 | 108.3 | 305.4 | 176.9 | 6 | 1481.9 | 1182.8 | 1469.5 | 2939.3 | 2346.1 | 2914.8 |
|  | 400.2 | 112.5 | 112.5 | 108.3 | 305.4 | 176.9 | 6 | 1486.1 | 1186.3 | 1474.6 | 2947.6 | 2353.0 | 2924.8 |
|  | 401.4 | 112.5 | 112.5 | 108.3 | 305.4 | 177.2 | 6 | 1490.2 | 1189.8 | 1479.6 | 2955.9 | 2359.9 | 2934.8 |
|  | 399.3 | 112.5 | 112.5 | 108.3 | 305.4 | 177.2 | 6 | 1494.4 | 1193.2 | 1484.6 | 2964.1 | 2366.8 | 2944.8 |
|  | 401.2 | 112.5 | 112.5 | 108.3 | 305.4 | 177.2 | 6 | 1498.6 | 1196.7 | 1489.7 | 2972.4 | 2373.7 | 2954.7 |
|  | 400.7 | 112.5 | 112.5 | 108.3 | 305.4 | 177.2 | 6 | 1502.8 | 1200.2 | 1494.7 | 2980.7 | 2380.6 | 2964.7 |
|  | 402.8 | 112.5 | 112.5 | 108.3 | 305.4 | 177.2 | 6 | 1506.9 | 1203.6 | 1499.7 | 2989.0 | 2387.4 | 2974.7 |
|  | 400.1 | 112.5 | 112.5 | 108.3 | 306.0 | 177.2 | 6 | 1511.1 | 1207.1 | 1504.7 | 2997.3 | 2394.3 | 2984.6 |
|  | 399.5 | 112.5 | 112.5 | 108.3 | 306.0 | 177.2 | 6 | 1515.3 | 1210.6 | 1509.8 | 3005.6 | 2401.2 | 2994.6 |
|  | 398.0 | 112.5 | 112.5 | 108.3 | 306.0 | 177.2 | 6 | 1519.4 | 1214.1 | 1514.8 | 3013.8 | 2408.1 | 3004.6 |
|  | 398.1 | 112.5 | 112.5 | 108.3 | 306.0 | 177.2 | 6 | 1523.6 | 1217.5 | 1519.8 | 3022.0 | 2415.0 | 3014.6 |
|  | 398.3 | 112.5 | 112.5 | 108.3 | 306.0 | 177.2 | 6 | 1527.7 | 1221.0 | 1524.9 | 3030.2 | 2421.9 | 3024.6 |
|  | 396.1 | 112.5 | 112.5 | 108.3 | 306.0 | 177.2 | 6 | 1531.8 | 1224.5 | 1529.9 | 3038.4 | 2428.8 | 3034.6 |
|  | 396.2 | 112.5 | 112.5 | 108.3 | 306.0 | 177.2 | 6 | 1536.0 | 1228.0 | 1534.9 | 3046.6 | 2435.6 | 3044.5 |
|  | 401.6 | 112.5 | 112.5 | 108.3 | 302.1 | 177.2 | 6 | 1540.2 | 1231.4 | 1539.9 | 3054.9 | 2442.5 | 3054.5 |
|  | 399.6 | 112.5 | 112.5 | 108.3 | 302.1 | 177.2 | 6 | 1544.3 | 1234.9 | 1544.9 | 3063.2 | 2449.4 | 3064.4 |
|  | 397.2 | 112.5 | 112.5 | 108.3 | 302.1 | 177.4 | 6 | 1548.5 | 1238.4 | 1549.9 | 3071.4 | 2456.3 | 3074.3 |
|  | 402.2 | 112.5 | 112.5 | 104.8 | 302.1 | 177.4 | 6 | 1552.6 | 1241.8 | 1554.9 | 3079.7 | 2463.1 | 3084.2 |
|  | 402.7 | 112.5 | 112.5 | 108.3 | 302.1 | 177.4 | 6 | 1556.8 | 1245.3 | 1559.9 | 3088.0 | 2470.0 | 3094.1 |
|  | 394.0 | 112.5 | 112.5 | 104.8 | 302.1 | 177.4 | 6 | 1560.9 | 1248.7 | 1564.9 | 3096.1 | 2476.8 | 3104.0 |
|  | 394.7 | 113.6 | 113.6 | 108.3 | 302.1 | 177.4 | 6 | 1565.1 | 1252.2 | 1569.9 | 3104.3 | 2483.7 | 3113.9 |
|  | 395.2 | 112.5 | 112.5 | 104.8 | 302.7 | 177.4 | 6 | 1569.2 | 1255.6 | 1574.9 | 3112.5 | 2490.6 | 3123.8 |
|  | 390.5 | 112.5 | 112.5 | 104.8 | 302.7 | 177.4 | 6 | 1573.2 | 1259.1 | 1579.9 | 3120.5 | 2497.4 | 3133.7 |
|  | 395.7 | 112.5 | 112.5 | 104.8 | 302.7 | 177.4 | 6 | 1577.4 | 1262.5 | 1584.9 | 3128.7 | 2504.2 | 3143.7 |
|  | 398.6 | 112.5 | 112.5 | 104.8 | 302.7 | 177.4 | 6 | 1581.5 | 1265.9 | 1589.9 | 3136.9 | 2511.0 | 3153.6 |
|  | 396.7 | 112.5 | 112.5 | 108.3 | 302.7 | 177.4 | 6 | 1585.6 | 1269.4 | 1594.9 | 3145.1 | 2517.9 | 3163.5 |
|  | 395.3 | 112.5 | 112.5 | 108.3 | 302.7 | 177.4 | 6 | 1589.8 | 1272.9 | 1599.9 | 3153.3 | 2524.8 | 3173.4 |
|  | 394.0 | 112.5 | 112.5 | 108.3 | 302.7 | 177.4 | 6 | 1593.9 | 1276.4 | 1604.9 | 3161.4 | 2531.7 | 3183.3 |



| Day | $\begin{gathered} \hline \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \mathrm{G} 601 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \mathrm{G} 602 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \text { G603 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G354 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G393 } \\ \text { cfs } \end{gathered}$ | Day | $\begin{gathered} \mathrm{G} 600 \\ \mathrm{cfs} \end{gathered}$ | $\begin{aligned} & \text { G601-3 } \\ & \mathrm{cfs} \end{aligned}$ | $\mathrm{G} 393+\mathrm{G} 354$ <br> Cfs | G600 $\mathrm{ac}-\mathrm{ft}$ | G601-3 $\mathrm{ac}-\mathrm{ft}$ | $\begin{gathered} \mathrm{G} 393+\mathrm{G} 354 \\ \mathrm{ac}-\mathrm{ft} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 394.9 | 108.7 | 108.7 | 104.8 | 290.2 | 176.9 | 7 | 1810.8 | 1454.7 | 1856.3 | 3591.6 | 2885.5 | 3682.0 |
|  | 387.7 | 103.1 | 103.1 | 93.0 | 290.2 | 176.9 | 7 | 1814.8 | 1457.9 | 1861.2 | 3599.7 | 2891.7 | 3691.7 |
|  | 391.0 | 102.3 | 102.3 | 92.2 | 289.7 | 176.9 | 7 | 1818.9 | 1460.9 | 1866.0 | 3607.7 | 2897.8 | 3701.3 |
|  | 390.2 | 102.3 | 102.3 | 91.4 | 289.7 | 176.9 | 7 | 1822.9 | 1464.0 | 1870.9 | 3615.8 | 2903.9 | 3710.9 |
|  | 385.9 | 99.5 | 99.5 | 86.9 | 289.7 | 176.9 | 7 | 1827.0 | 1467.0 | 1875.8 | 3623.8 | 2909.8 | 3720.6 |
|  | 395.1 | 99.5 | 99.5 | 86.9 | 289.7 | 176.9 | 7 | 1831.1 | 1470.0 | 1880.6 | 3631.9 | 2915.7 | 3730.2 |
|  | 393.5 | 97.6 | 97.6 | 86.1 | 289.7 | 176.9 | 7 | 1835.2 | 1472.9 | 1885.5 | 3640.1 | 2921.5 | 3739.9 |
|  | 392.9 | 98.7 | 98.7 | 82.3 | 289.7 | 176.9 | 7 | 1839.3 | 1475.8 | 1890.4 | 3648.2 | 2927.3 | 3749.5 |
|  | 395.2 | 96.8 | 96.8 | 81.6 | 289.7 | 176.9 | 7 | 1843.4 | 1478.7 | 1895.2 | 3656.3 | 2933.0 | 3759.2 |
|  | 394.4 | 97.9 | 97.9 | 81.6 | 289.7 | 175.3 | 7 | 1847.5 | 1481.6 | 1900.1 | 3664.5 | 2938.7 | 3768.8 |
|  | 389.6 | 97.9 | 97.9 | 77.7 | 289.7 | 175.3 | 7 | 1851.5 | 1484.4 | 1904.9 | 3672.5 | 2944.4 | 3778.4 |
|  | 389.5 | 96.0 | 96.0 | 80.8 | 289.7 | 175.3 | 7 | 1855.6 | 1487.3 | 1909.7 | 3680.6 | 2950.0 | 3788.0 |
|  | 395.3 | 96.0 | 96.0 | 80.8 | 289.7 | 175.3 | 7 | 1859.7 | 1490.1 | 1914.6 | 3688.8 | 2955.6 | 3797.6 |
|  | 395.9 | 97.1 | 97.1 | 77.0 | 285.9 | 173.7 | 7 | 1863.8 | 1492.9 | 1919.4 | 3696.9 | 2961.3 | 3807.1 |
|  | 391.5 | 95.2 | 95.2 | 80.1 | 285.9 | 173.7 | 7 | 1867.9 | 1495.8 | 1924.2 | 3705.0 | 2966.8 | 3816.6 |
|  | 393.6 | 95.2 | 95.2 | 80.1 | 286.4 | 173.7 | 7 | 1872.0 | 1498.6 | 1929.0 | 3713.2 | 2972.4 | 3826.1 |
|  | 395.5 | 95.2 | 95.2 | 80.1 | 286.4 | 173.7 | 7 | 1876.1 | 1501.4 | 1933.7 | 3721.3 | 2978.0 | 3835.6 |
|  | 389.5 | 96.3 | 96.3 | 76.3 | 286.4 | 172.1 | 7 | 1880.2 | 1504.2 | 1938.5 | 3729.4 | 2983.6 | 3845.1 |
|  | 389.6 | 96.3 | 96.3 | 79.4 | 286.4 | 172.1 | 7 | 1884.3 | 1507.0 | 1943.3 | 3737.4 | 2989.2 | 3854.5 |
|  | 391.5 | 96.3 | 96.3 | 79.4 | 286.4 | 172.1 | 7 | 1888.3 | 1509.9 | 1948.1 | 3745.5 | 2994.8 | 3864.0 |
|  | 391.2 | 94.4 | 94.4 | 79.4 | 282.6 | 172.1 | 7 | 1892.4 | 1512.7 | 1952.8 | 3753.6 | 3000.3 | 3873.4 |
|  | 391.3 | 95.5 | 95.5 | 79.4 | 282.6 | 170.4 | 7 | 1896.5 | 1515.5 | 1957.5 | 3761.7 | 3005.9 | 3882.8 |
|  | 395.5 | 94.4 | 94.4 | 82.3 | 282.6 | 170.4 | 7 | 1900.6 | 1518.3 | 1962.2 | 3769.9 | 3011.5 | 3892.1 |
|  | 389.2 | 95.5 | 95.5 | 78.6 | 282.6 | 170.6 | 7 | 1904.7 | 1521.1 | 1967.0 | 3777.9 | 3017.1 | 3901.5 |
|  | 393.6 | 95.5 | 95.5 | 78.6 | 282.6 | 169.0 | 7 | 1908.8 | 1523.9 | 1971.7 | 3786.0 | 3022.7 | 3910.8 |
|  | 399.3 | 95.5 | 95.5 | 78.6 | 283.1 | 169.0 | 7 | 1912.9 | 1526.7 | 1976.4 | 3794.3 | 3028.2 | 3920.2 |
|  | 391.7 | 95.5 | 95.5 | 81.5 | 283.1 | 169.0 | 7 | 1917.0 | 1529.6 | 1981.1 | 3802.4 | 3033.9 | 3929.5 |
|  | 395.3 | 95.5 | 95.5 | 81.5 | 279.4 | 169.0 | 7 | 1921.1 | 1532.4 | 1985.8 | 3810.5 | 3039.5 | 3938.8 |
|  | 393.2 | 94.7 | 94.7 | 81.5 | 279.4 | 167.4 | 7 | 1925.2 | 1535.2 | 1990.4 | 3818.7 | 3045.1 | 3948.0 |
|  | 402.9 | 94.7 | 94.7 | 81.5 | 279.4 | 167.4 | 7 | 1929.4 | 1538.0 | 1995.1 | 3827.0 | 3050.7 | 3957.2 |
|  | 399.1 | 94.7 | 94.7 | 84.3 | 279.9 | 167.6 | 7 | 1933.6 | 1540.9 | 1999.7 | 3835.2 | 3056.4 | 3966.5 |
|  | 398.8 | 94.7 | 94.7 | 84.3 | 279.9 | 167.6 | 7 | 1937.7 | 1543.7 | 2004.4 | 3843.5 | 3062.0 | 3975.7 |
|  | 387.2 | 94.7 | 94.7 | 80.8 | 276.1 | 166.0 | 7 | 1941.8 | 1546.6 | 2009.0 | 3851.5 | 3067.6 | 3984.9 |
|  | 395.3 | 94.7 | 94.7 | 80.8 | 276.1 | 166.0 | 7 | 1945.9 | 1549.4 | 2013.6 | 3859.6 | 3073.2 | 3994.0 |
|  | 389.2 | 94.7 | 94.7 | 80.8 | 276.1 | 166.0 | 7 | 1949.9 | 1552.2 | 2018.2 | 3867.7 | 3078.7 | 4003.1 |
|  | 389.5 | 94.7 | 94.7 | 83.5 | 276.1 | 164.6 | 7 | 1954.0 | 1555.0 | 2022.8 | 3875.7 | 3084.4 | 4012.2 |
|  | 389.5 | 94.7 | 94.7 | 83.5 | 276.6 | 164.6 | 7 | 1958.0 | 1557.9 | 2027.4 | 3883.8 | 3090.0 | 4021.4 |
|  | 397.1 | 95.7 | 95.7 | 83.5 | 276.6 | 164.6 | 7 | 1962.2 | 1560.7 | 2032.0 | 3892.0 | 3095.7 | 4030.5 |
|  | 391.5 | 93.9 | 93.9 | 83.5 | 272.8 | 164.6 | 7 | 1966.3 | 1563.6 | 2036.6 | 3900.1 | 3101.3 | 4039.5 |
|  | 401.4 | 93.9 | 93.9 | 83.5 | 272.8 | 163.0 | 7 | 1970.4 | 1566.4 | 2041.1 | 3908.4 | 3106.9 | 4048.5 |
|  | 393.3 | 93.9 | 93.9 | 86.0 | 272.8 | 163.0 | 7 | 1974.5 | 1569.2 | 2045.6 | 3916.5 | 3112.6 | 4057.5 |
|  | 397.1 | 93.9 | 93.9 | 86.0 | 273.3 | 163.2 | 7 | 1978.7 | 1572.1 | 2050.2 | 3924.7 | 3118.2 | 4066.5 |
|  | 397.7 | 93.9 | 93.9 | 86.0 | 273.3 | 163.2 | 7 | 1982.8 | 1574.9 | 2054.7 | 3932.9 | 3123.9 | 4075.6 |
|  | 395.0 | 93.9 | 93.9 | 82.7 | 269.6 | 163.2 | 7 | 1986.9 | 1577.8 | 2059.2 | 3941.1 | 3129.5 | 4084.5 |
|  | 404.6 | 93.9 | 93.9 | 82.7 | 269.6 | 161.6 | 7 | 1991.1 | 1580.6 | 2063.7 | 3949.4 | 3135.1 | 4093.4 |
|  | 396.6 | 93.9 | 93.9 | 82.7 | 269.6 | 161.6 | 7 | 1995.3 | 1583.4 | 2068.2 | 3957.6 | 3140.6 | 4102.3 |
| 8 | 398.8 | 93.9 | 93.9 | 85.3 | 269.6 | 161.6 | 8 | 1999.4 | 1586.2 | 2072.7 | 3965.9 | 3146.3 | 4111.2 |
|  | 397.1 | 94.9 | 94.9 | 85.3 | 269.6 | 161.6 | 8 | 2003.6 | 1589.1 | 2077.2 | 3974.1 | 3152.0 | 4120.1 |
|  | 400.5 | 93.9 | 93.9 | 85.3 | 270.0 | 160.2 | 8 | 2007.7 | 1591.9 | 2081.7 | 3982.4 | 3157.6 | 4129.0 |
|  | 396.6 | 94.9 | 94.9 | 85.3 | 266.3 | 160.2 | 8 | 2011.9 | 1594.8 | 2086.1 | 3990.5 | 3163.3 | 4137.8 |


| Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \mathrm{G} 601 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \mathrm{G} 602 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \text { G603 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \mathrm{G} 354 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \text { G393 } \\ \text { cfs } \end{gathered}$ | Day | $\begin{gathered} \mathrm{G} 600 \\ \mathrm{cfs} \end{gathered}$ | $\begin{aligned} & \text { G601-3 } \\ & \text { cfs } \end{aligned}$ | G393+G354 <br> Cfs | G600 $\mathrm{ac}-\mathrm{ft}$ | G601-3 ac-ft | $\begin{gathered} \mathrm{G} 393+\mathrm{G} 354 \\ \mathrm{ac}-\mathrm{ft} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 395.0 | 93.9 | 93.9 | 85.3 | 266.3 | 160.2 | 8 | 2016.0 | 1597.6 | 2090.6 | 3998.7 | 3168.9 | 4146.6 |
|  | 398.6 | 94.9 | 94.9 | 85.3 | 266.3 | 160.2 | 8 | 2020.1 | 1600.5 | 2095.0 | 4006.9 | 3174.6 | 4155.5 |
|  | 399.1 | 94.9 | 94.9 | 85.3 | 266.3 | 158.6 | 8 | 2024.3 | 1603.4 | 2099.4 | 4015.2 | 3180.3 | 4164.2 |
|  | 392.7 | 93.1 | 93.1 | 87.7 | 266.3 | 158.6 | 8 | 2028.4 | 1606.2 | 2103.9 | 4023.3 | 3186.0 | 4173.0 |
|  | 394.7 | 93.1 | 93.1 | 87.7 | 263.0 | 158.6 | 8 | 2032.5 | 1609.1 | 2108.3 | 4031.5 | 3191.6 | 4181.7 |
|  | 398.3 | 93.1 | 93.1 | 87.7 | 263.0 | 158.8 | 8 | 2036.6 | 1611.9 | 2112.7 | 4039.7 | 3197.3 | 4190.4 |
|  | 402.4 | 93.1 | 93.1 | 87.7 | 263.0 | 158.8 | 8 | 2040.8 | 1614.8 | 2117.0 | 4048.0 | 3202.9 | 4199.2 |
|  | 392.7 | 93.1 | 93.1 | 87.7 | 263.0 | 157.2 | 8 | 2044.9 | 1617.6 | 2121.4 | 4056.1 | 3208.6 | 4207.8 |
|  | 392.2 | 93.1 | 93.1 | 87.7 | 263.0 | 157.2 | 8 | 2049.0 | 1620.5 | 2125.8 | 4064.2 | 3214.2 | 4216.5 |
|  | 395.0 | 93.1 | 93.1 | 87.7 | 263.3 | 157.4 | 8 | 2053.1 | 1623.3 | 2130.2 | 4072.4 | 3219.9 | 4225.2 |
|  | 400.0 | 93.1 | 93.1 | 90.0 | 259.7 | 157.4 | 8 | 2057.3 | 1626.2 | 2134.5 | 4080.6 | 3225.6 | 4233.8 |
|  | 388.6 | 93.1 | 93.1 | 90.0 | 259.7 | 157.4 | 8 | 2061.3 | 1629.1 | 2138.9 | 4088.7 | 3231.3 | 4242.5 |
|  | 400.7 | 93.1 | 93.1 | 90.0 | 259.7 | 155.8 | 8 | 2065.5 | 1632.0 | 2143.2 | 4097.0 | 3237.0 | 4251.0 |
|  | 419.2 | 93.1 | 93.1 | 90.0 | 260.0 | 155.8 | 8 | 2069.9 | 1634.8 | 2147.5 | 4105.6 | 3242.7 | 4259.6 |
|  | 420.6 | 94.1 | 94.1 | 86.0 | 260.0 | 156.0 | 8 | 2074.3 | 1637.7 | 2151.9 | 4114.3 | 3248.4 | 4268.2 |
|  | 418.1 | 94.9 | 94.9 | 86.9 | 260.0 | 156.0 | 8 | 2078.6 | 1640.6 | 2156.2 | 4122.9 | 3254.1 | 4276.8 |
|  | 417.8 | 94.9 | 94.9 | 90.0 | 256.4 | 156.0 | 8 | 2083.0 | 1643.5 | 2160.5 | 4131.6 | 3259.9 | 4285.3 |
|  | 415.6 | 94.9 | 94.9 | 90.0 | 256.6 | 156.0 | 8 | 2087.3 | 1646.4 | 2164.8 | 4140.2 | 3265.7 | 4293.9 |
|  | 411.3 | 96.7 | 96.7 | 93.0 | 256.6 | 154.6 | 8 | 2091.6 | 1649.4 | 2169.1 | 4148.7 | 3271.6 | 4302.4 |
|  | 419.1 | 96.7 | 96.7 | 93.0 | 256.6 | 154.6 | 8 | 2096.0 | 1652.4 | 2173.4 | 4157.3 | 3277.5 | 4310.9 |
|  | 415.0 | 101.2 | 101.2 | 93.0 | 256.6 | 154.6 | 8 | 2100.3 | 1655.5 | 2177.6 | 4165.9 | 3283.6 | 4319.4 |
|  | 401.7 | 102.1 | 102.1 | 93.0 | 256.9 | 154.6 | 8 | 2104.5 | 1658.6 | 2181.9 | 4174.2 | 3289.8 | 4327.9 |
|  | 411.3 | 103.8 | 103.8 | 105.0 | 253.3 | 154.7 | 8 | 2108.7 | 1661.8 | 2186.2 | 4182.7 | 3296.2 | 4336.3 |
|  | 406.1 | 106.5 | 106.5 | 111.8 | 253.3 | 153.2 | 8 | 2113.0 | 1665.2 | 2190.4 | 4191.1 | 3302.9 | 4344.7 |
|  | 406.2 | 108.4 | 108.4 | 112.8 | 253.5 | 153.2 | 8 | 2117.2 | 1668.6 | 2194.6 | 4199.5 | 3309.7 | 4353.1 |
|  | 406.0 | 111.2 | 111.2 | 118.6 | 253.5 | 153.3 | 8 | 2121.4 | 1672.2 | 2198.9 | 4207.9 | 3316.8 | 4361.5 |
|  | 399.0 | 111.1 | 111.1 | 119.6 | 253.7 | 153.3 | 8 | 2125.6 | 1675.7 | 2203.1 | 4216.1 | 3323.8 | 4369.9 |
|  | 404.6 | 113.0 | 113.0 | 120.7 | 253.7 | 153.4 | 8 | 2129.8 | 1679.4 | 2207.4 | 4224.5 | 3331.0 | 4378.3 |
|  | 408.4 | 113.0 | 113.0 | 123.6 | 250.0 | 153.4 | 8 | 2134.1 | 1683.0 | 2211.6 | 4232.9 | 3338.2 | 4386.6 |
|  | 398.0 | 114.9 | 114.9 | 124.7 | 250.1 | 153.4 | 8 | 2138.2 | 1686.7 | 2215.8 | 4241.1 | 3345.5 | 4395.0 |
|  | 403.6 | 113.9 | 113.9 | 124.7 | 250.1 | 153.5 | 8 | 2142.4 | 1690.4 | 2220.0 | 4249.5 | 3352.8 | 4403.3 |
|  | 401.2 | 114.8 | 114.8 | 127.6 | 250.1 | 153.5 | 8 | 2146.6 | 1694.1 | 2224.2 | 4257.8 | 3360.2 | 4411.7 |
|  | 399.4 | 114.8 | 114.8 | 127.6 | 250.1 | 153.5 | 8 | 2150.7 | 1697.8 | 2228.4 | 4266.0 | 3367.6 | 4420.0 |
|  | 400.6 | 109.1 | 109.1 | 128.7 | 250.1 | 153.6 | 8 | 2154.9 | 1701.4 | 2232.6 | 4274.3 | 3374.8 | 4428.3 |
|  | 403.8 | 108.3 | 108.3 | 118.8 | 250.1 | 153.6 | 8 | 2159.1 | 1704.9 | 2236.8 | 4282.6 | 3381.7 | 4436.7 |
|  | 404.9 | 104.4 | 104.4 | 117.8 | 250.1 | 153.6 | 8 | 2163.3 | 1708.3 | 2241.0 | 4291.0 | 3388.4 | 4445.0 |
|  | 408.5 | 103.6 | 103.6 | 111.8 | 250.1 | 153.6 | 8 | 2167.6 | 1711.6 | 2245.2 | 4299.4 | 3395.0 | 4453.4 |
|  | 404.6 | 101.7 | 101.7 | 110.8 | 250.1 | 153.6 | 8 | 2171.8 | 1714.9 | 2249.4 | 4307.8 | 3401.5 | 4461.7 |
|  | 407.1 | 100.9 | 100.9 | 107.9 | 250.1 | 153.7 | 8 | 2176.1 | 1718.1 | 2253.6 | 4316.2 | 3407.9 | 4470.1 |
|  | 407.9 | 99.0 | 99.0 | 104.9 | 246.5 | 153.7 | 8 | 2180.3 | 1721.3 | 2257.8 | 4324.6 | 3414.2 | 4478.3 |
|  | 407.7 | 100.0 | 100.0 | 103.9 | 246.5 | 153.7 | 8 | 2184.6 | 1724.5 | 2262.0 | 4333.1 | 3420.5 | 4486.6 |
|  | 409.9 | 99.2 | 99.2 | 100.9 | 246.5 | 153.7 | 8 | 2188.8 | 1727.6 | 2266.1 | 4341.5 | 3426.6 | 4494.9 |
|  | 412.2 | 99.2 | 99.2 | 100.9 | 246.5 | 155.2 | 8 | 2193.1 | 1730.7 | 2270.3 | 4350.0 | 3432.8 | 4503.2 |
|  | 410.6 | 97.3 | 97.3 | 97.9 | 246.5 | 153.7 | 8 | 2197.4 | 1733.7 | 2274.5 | 4358.5 | 3438.9 | 4511.4 |
|  | 412.1 | 97.3 | 97.3 | 100.0 | 246.5 | 153.7 | 8 | 2201.7 | 1736.8 | 2278.7 | 4367.0 | 3445.0 | 4519.7 |
|  | 400.6 | 93.9 | 93.9 | 97.0 | 246.5 | 153.7 | 8 | 2205.9 | 1739.8 | 2282.8 | 4375.3 | 3450.8 | 4528.0 |
|  | 395.7 | 96.5 | 96.5 | 97.0 | 246.5 | 153.7 | 8 | 2210.0 | 1742.8 | 2287.0 | 4383.5 | 3456.8 | 4536.2 |
|  | 401.0 | 93.9 | 93.9 | 96.1 | 246.5 | 153.7 | 8 | 2214.2 | 1745.8 | 2291.2 | 4391.8 | 3462.7 | 4544.5 |
|  | 400.8 | 95.7 | 95.7 | 93.0 | 246.5 | 153.7 | 8 | 2218.3 | 1748.7 | 2295.3 | 4400.1 | 3468.6 | 4552.8 |
|  | 402.2 | 93.9 | 93.9 | 93.0 | 246.5 | 153.8 | 8 | 2222.5 | 1751.6 | 2299.5 | 4408.4 | 3474.4 | 4561.1 |


| Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \mathrm{G} 601 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \mathrm{G} 602 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \mathrm{G} 603 \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \text { G354 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G393 } \\ \text { cfs } \end{gathered}$ | Day | $\begin{gathered} \mathrm{G} 600 \\ \mathrm{cfs} \end{gathered}$ | $\begin{aligned} & \text { G601-3 } \\ & \text { cfs } \end{aligned}$ | G393+G354 <br> Cfs | $\begin{aligned} & \text { G600 } \\ & \text { ac-ft } \end{aligned}$ | $\begin{gathered} \text { G601-3 } \\ \text { ac-ft } \end{gathered}$ | $\begin{gathered} \mathrm{G} 393+\mathrm{G} 354 \\ \mathrm{ac}-\mathrm{ft} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 401.9 | 94.9 | 94.9 | 93.0 | 246.5 | 153.7 | 8 | 2226.7 | 1754.6 | 2303.7 | 4416.7 | 3480.2 | 4569.3 |
|  | 403.7 | 94.9 | 94.9 | 92.2 | 246.5 | 153.8 | 8 | 2230.9 | 1757.5 | 2307.8 | 4425.0 | 3486.0 | 4577.6 |
|  | 401.1 | 94.9 | 94.9 | 92.2 | 246.5 | 153.8 | 8 | 2235.1 | 1760.5 | 2312.0 | 4433.3 | 3491.9 | 4585.9 |
|  | 402.4 | 93.1 | 93.1 | 92.2 | 246.5 | 153.8 | 8 | 2239.3 | 1763.4 | 2316.2 | 4441.6 | 3497.6 | 4594.1 |
|  | 401.8 | 93.1 | 93.1 | 92.2 | 246.5 | 153.8 | 8 | 2243.5 | 1766.3 | 2320.3 | 4449.9 | 3503.4 | 4602.4 |
|  | 402.1 | 93.1 | 93.1 | 92.2 | 246.5 | 152.2 | 8 | 2247.7 | 1769.2 | 2324.5 | 4458.2 | 3509.1 | 4610.6 |
|  | 402.3 | 93.1 | 93.1 | 92.2 | 243.0 | 152.2 | 8 | 2251.9 | 1772.1 | 2328.6 | 4466.5 | 3514.9 | 4618.8 |
|  | 404.8 | 94.1 | 94.1 | 92.2 | 243.0 | 152.2 | 8 | 2256.1 | 1775.0 | 2332.7 | 4474.9 | 3520.7 | 4627.0 |
|  | 402.7 | 93.1 | 93.1 | 91.3 | 243.0 | 152.2 | 8 | 2260.3 | 1777.9 | 2336.8 | 4483.2 | 3526.4 | 4635.1 |
|  | 405.0 | 94.1 | 94.1 | 91.3 | 243.0 | 152.2 | 8 | 2264.5 | 1780.8 | 2341.0 | 4491.6 | 3532.2 | 4643.3 |
|  | 403.2 | 94.1 | 94.1 | 91.3 | 243.0 | 152.2 | 8 | 2268.7 | 1783.7 | 2345.1 | 4499.9 | 3538.0 | 4651.5 |
|  | 405.3 | 94.1 | 94.1 | 91.3 | 243.0 | 150.6 | 8 | 2272.9 | 1786.6 | 2349.2 | 4508.3 | 3543.7 | 4659.6 |
|  | 403.3 | 94.1 | 94.1 | 91.3 | 243.0 | 150.6 | 8 | 2277.1 | 1789.5 | 2353.3 | 4516.6 | 3549.5 | 4667.7 |
|  | 403.5 | 92.3 | 92.3 | 91.3 | 243.0 | 150.6 | 8 | 2281.3 | 1792.4 | 2357.4 | 4525.0 | 3555.2 | 4675.9 |
|  | 403.2 | 92.3 | 92.3 | 91.3 | 243.0 | 150.6 | 8 | 2285.5 | 1795.3 | 2361.5 | 4533.3 | 3560.9 | 4684.0 |
|  | 401.4 | 92.3 | 92.3 | 93.4 | 239.4 | 150.6 | 8 | 2289.7 | 1798.2 | 2365.5 | 4541.6 | 3566.6 | 4692.1 |
|  | 403.7 | 92.3 | 92.3 | 93.4 | 239.4 | 150.6 | 8 | 2293.9 | 1801.1 | 2369.6 | 4549.9 | 3572.4 | 4700.1 |
|  | 406.2 | 92.3 | 92.3 | 93.4 | 239.4 | 150.6 | 8 | 2298.1 | 1804.0 | 2373.7 | 4558.3 | 3578.1 | 4708.2 |
|  | 401.9 | 92.3 | 92.3 | 93.4 | 239.4 | 149.1 | 8 | 2302.3 | 1806.8 | 2377.7 | 4566.6 | 3583.9 | 4716.2 |
|  | 401.7 | 92.3 | 92.3 | 93.4 | 239.4 | 149.1 | 8 | 2306.5 | 1809.7 | 2381.8 | 4574.9 | 3589.6 | 4724.2 |
|  | 404.3 | 92.3 | 92.3 | 93.4 | 239.4 | 149.1 | 8 | 2310.7 | 1812.6 | 2385.8 | 4583.3 | 3595.4 | 4732.3 |
|  | 401.8 | 93.3 | 93.3 | 93.4 | 239.4 | 149.1 | 8 | 2314.9 | 1815.6 | 2389.9 | 4591.6 | 3601.2 | 4740.3 |
|  | 404.2 | 92.3 | 92.3 | 93.4 | 239.4 | 149.1 | 8 | 2319.1 | 1818.5 | 2393.9 | 4599.9 | 3606.9 | 4748.3 |
|  | 406.8 | 93.3 | 93.3 | 93.4 | 235.9 | 149.1 | 8 | 2323.3 | 1821.4 | 2397.9 | 4608.3 | 3612.7 | 4756.3 |
|  | 406.0 | 93.3 | 93.3 | 95.5 | 235.9 | 147.6 | 8 | 2327.6 | 1824.3 | 2401.9 | 4616.7 | 3618.5 | 4764.2 |
|  | 405.4 | 93.3 | 93.3 | 95.5 | 235.9 | 147.6 | 8 | 2331.8 | 1827.2 | 2405.9 | 4625.1 | 3624.3 | 4772.1 |
|  | 400.0 | 93.3 | 93.3 | 92.6 | 235.9 | 147.6 | 8 | 2336.0 | 1830.2 | 2409.9 | 4633.4 | 3630.1 | 4780.0 |
|  | 404.1 | 93.3 | 93.3 | 92.6 | 235.9 | 147.6 | 8 | 2340.2 | 1833.1 | 2413.9 | 4641.7 | 3635.9 | 4788.0 |
|  | 403.5 | 93.3 | 93.3 | 92.6 | 235.9 | 147.6 | 8 | 2344.4 | 1836.0 | 2417.9 | 4650.1 | 3641.6 | 4795.9 |
|  | 400.4 | 93.3 | 93.3 | 92.6 | 235.9 | 147.6 | 8 | 2348.5 | 1838.9 | 2421.9 | 4658.3 | 3647.4 | 4803.8 |
|  | 402.2 | 93.3 | 93.3 | 92.6 | 232.3 | 146.1 | 8 | 2352.7 | 1841.8 | 2425.8 | 4666.6 | 3653.2 | 4811.6 |
|  | 399.9 | 93.3 | 93.3 | 92.6 | 232.3 | 146.1 | 8 | 2356.9 | 1844.7 | 2429.8 | 4674.9 | 3658.9 | 4819.4 |
|  | 399.9 | 93.3 | 93.3 | 92.6 | 232.3 | 146.1 | 8 | 2361.1 | 1847.6 | 2433.7 | 4683.2 | 3664.7 | 4827.3 |
|  | 402.3 | 91.5 | 91.5 | 92.6 | 232.3 | 146.1 | 8 | 2365.3 | 1850.5 | 2437.6 | 4691.5 | 3670.4 | 4835.1 |
|  | 402.2 | 93.3 | 93.3 | 92.6 | 232.3 | 146.1 | 8 | 2369.4 | 1853.4 | 2441.6 | 4699.8 | 3676.2 | 4842.9 |
|  | 399.8 | 91.5 | 91.5 | 94.6 | 232.3 | 146.1 | 8 | 2373.6 | 1856.3 | 2445.5 | 4708.1 | 3681.9 | 4850.7 |
|  | 399.7 | 91.5 | 91.5 | 94.6 | 232.3 | 146.1 | 8 | 2377.8 | 1859.2 | 2449.5 | 4716.3 | 3687.6 | 4858.5 |
|  | 397.7 | 91.5 | 91.5 | 94.6 | 228.8 | 146.1 | 8 | 2381.9 | 1862.0 | 2453.4 | 4724.5 | 3693.4 | 4866.3 |
|  | 399.8 | 91.5 | 91.5 | 94.6 | 228.8 | 144.5 | 8 | 2386.1 | 1864.9 | 2457.3 | 4732.8 | 3699.1 | 4874.0 |
|  | 395.4 | 91.5 | 91.5 | 94.6 | 228.8 | 144.5 | 8 | 2390.2 | 1867.8 | 2461.2 | 4741.0 | 3704.8 | 4881.7 |
|  | 397.4 | 91.5 | 91.5 | 94.6 | 228.8 | 144.5 | 8 | 2394.3 | 1870.7 | 2465.0 | 4749.2 | 3710.6 | 4889.4 |
|  | 390.7 | 91.5 | 91.5 | 94.6 | 228.8 | 144.5 | 8 | 2398.4 | 1873.6 | 2468.9 | 4757.2 | 3716.3 | 4897.1 |
| 9 | 394.4 | 91.5 | 91.5 | 94.6 | 225.3 | 144.5 | 9 | 2402.5 | 1876.5 | 2472.8 | 4765.4 | 3722.0 | 4904.8 |
|  | 395.6 | 91.5 | 91.5 | 94.6 | 225.3 | 143.0 | 9 | 2406.6 | 1879.4 | 2476.6 | 4773.6 | 3727.8 | 4912.4 |
|  | 396.6 | 92.5 | 92.5 | 94.6 | 225.3 | 143.0 | 9 | 2410.8 | 1882.3 | 2480.5 | 4781.8 | 3733.6 | 4920.0 |
|  | 397.8 | 91.5 | 91.5 | 94.6 | 225.3 | 143.0 | 9 | 2414.9 | 1885.2 | 2484.3 | 4790.0 | 3739.3 | 4927.6 |
|  | 396.3 | 92.5 | 92.5 | 94.6 | 225.3 | 143.0 | 9 | 2419.0 | 1888.1 | 2488.1 | 4798.2 | 3745.1 | 4935.2 |
|  | 399.6 | 92.5 | 92.5 | 94.6 | 225.3 | 143.0 | 9 | 2423.2 | 1891.0 | 2492.0 | 4806.4 | 3750.8 | 4942.8 |
|  | 395.8 | 91.5 | 91.5 | 94.6 | 225.3 | 143.0 | 9 | 2427.3 | 1893.9 | 2495.8 | 4814.6 | 3756.6 | 4950.4 |
|  | 396.2 | 91.5 | 91.5 | 96.5 | 225.3 | 143.0 | 9 | 2431.5 | 1896.8 | 2499.6 | 4822.8 | 3762.4 | 4958.0 |


| Day | $\begin{gathered} \hline \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \text { G601 } \\ \mathrm{cfs} \end{gathered}$ | $\begin{gathered} \hline \text { G602 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G603 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G354 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G393 } \\ \text { cfs } \end{gathered}$ | Day | $\begin{gathered} \hline \text { G600 } \\ \text { cfs } \end{gathered}$ | G601-3 <br> cfs | $\begin{aligned} & \text { G393+G354 } \\ & \text { Cfs } \end{aligned}$ | $\begin{gathered} \hline \text { G600 } \\ \text { ac-ft } \end{gathered}$ | $\begin{gathered} \hline \text { G601-3 } \\ \text { ac-ft } \end{gathered}$ | $\begin{gathered} \text { G393+G354 } \\ \text { ac-ft } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 396.3 | 91.5 | 91.5 | 96.5 | 221.8 | 141.5 | 9 | 2435.6 | 1899.7 | 2503.4 | 4831.0 | 3768.1 | 4965.5 |
|  | 396.9 | 92.5 | 92.5 | 96.5 | 221.8 | 141.5 | 9 | 2439.7 | 1902.7 | 2507.2 | 4839.2 | 3773.9 | 4973.1 |
|  | 396.8 | 92.5 | 92.5 | 96.5 | 221.8 | 141.5 | 9 | 2443.8 | 1905.6 | 2511.0 | 4847.4 | 3779.8 | 4980.6 |
|  | 394.9 | 92.5 | 92.5 | 96.5 | 221.8 | 141.5 | 9 | 2448.0 | 1908.5 | 2514.8 | 4855.5 | 3785.6 | 4988.1 |
|  | 397.6 | 91.5 | 91.5 | 96.5 | 221.8 | 141.5 | 9 | 2452.1 | 1911.4 | 2518.6 | 4863.7 | 3791.4 | 4995.6 |
|  | 384.9 | 92.5 | 92.5 | 96.5 | 221.8 | 141.5 | 9 | 2456.1 | 1914.4 | 2522.3 | 4871.7 | 3797.2 | 5003.1 |
|  | 369.3 | 91.5 | 91.5 | 96.5 | 221.8 | 141.5 | 9 | 2460.0 | 1917.3 | 2526.1 | 4879.3 | 3802.9 | 5010.6 |
|  | 357.6 | 91.5 | 91.5 | 96.5 | 221.8 | 141.5 | 9 | 2463.7 | 1920.2 | 2529.9 | 4886.7 | 3808.7 | 5018.1 |
|  | 341.9 | 92.5 | 92.5 | 96.5 | 218.4 | 140.0 | 9 | 2467.2 | 1923.1 | 2533.7 | 4893.8 | 3814.5 | 5025.5 |
|  | 320.8 | 91.5 | 91.5 | 96.5 | 218.4 | 140.0 | 9 | 2470.6 | 1926.0 | 2537.4 | 4900.4 | 3820.3 | 5032.9 |
|  | 302.4 | 91.5 | 91.5 | 96.5 | 218.4 | 140.0 | 9 | 2473.7 | 1929.0 | 2541.1 | 4906.7 | 3826.1 | 5040.3 |
|  | 211.0 | 88.2 | 88.2 | 98.4 | 218.4 | 140.0 | 9 | 2475.9 | 1931.8 | 2544.9 | 4911.0 | 3831.8 | 5047.7 |
|  | 212.3 | 70.5 | 70.5 | 92.8 | 218.4 | 140.0 | 9 | 2478.1 | 1934.3 | 2548.6 | 4915.4 | 3836.6 | 5055.1 |
|  | 0.0 | 82.1 | 82.1 | 64.1 | 218.4 | 140.0 | 9 | 2478.1 | 1936.6 | 2552.3 | 4915.4 | 3841.3 | 5062.5 |
|  | 379.1 | 74.7 | 74.7 | 55.4 | 218.4 | 140.0 | 9 | 2482.1 | 1938.8 | 2556.0 | 4923.2 | 3845.5 | 5069.9 |
|  | 385.2 | 90.1 | 90.1 | 75.2 | 214.9 | 138.5 | 9 | 2486.1 | 1941.4 | 2559.7 | 4931.2 | 3850.8 | 5077.2 |
|  | 379.1 | 90.7 | 90.7 | 91.0 | 214.9 | 138.5 | 9 | 2490.1 | 1944.3 | 2563.4 | 4939.0 | 3856.4 | 5084.5 |
|  | 380.3 | 91.7 | 91.7 | 91.0 | 214.9 | 138.5 | 9 | 2494.0 | 1947.1 | 2567.1 | 4946.9 | 3862.1 | 5091.8 |
|  | 365.5 | 95.9 | 95.9 | 100.2 | 214.9 | 138.5 | 9 | 2497.8 | 1950.2 | 2570.8 | 4954.4 | 3868.1 | 5099.1 |
|  | 346.7 | 95.9 | 95.9 | 101.1 | 214.9 | 137.0 | 9 | 2501.4 | 1953.2 | 2574.4 | 4961.6 | 3874.2 | 5106.4 |
|  | 327.2 | 97.7 | 97.7 | 103.8 | 214.9 | 137.0 | 9 | 2504.8 | 1956.3 | 2578.1 | 4968.4 | 3880.4 | 5113.7 |
|  | 304.1 | 99.4 | 99.4 | 107.6 | 214.9 | 137.0 | 9 | 2508.0 | 1959.5 | 2581.8 | 4974.6 | 3886.7 | 5120.9 |
|  | 285.0 | 100.4 | 100.4 | 110.3 | 211.5 | 137.0 | 9 | 2511.0 | 1962.8 | 2585.4 | 4980.5 | 3893.1 | 5128.1 |
|  | 282.7 | 101.2 | 101.2 | 113.0 | 211.5 | 137.0 | 9 | 2513.9 | 1966.0 | 2589.0 | 4986.4 | 3899.7 | 5135.3 |
|  | 284.7 | 102.1 | 102.1 | 114.0 | 211.5 | 137.0 | 9 | 2516.9 | 1969.4 | 2592.7 | 4992.3 | 3906.2 | 5142.5 |
|  | 291.4 | 102.1 | 102.1 | 114.0 | 211.5 | 137.0 | 9 | 2519.9 | 1972.7 | 2596.3 | 4998.3 | 3912.8 | 5149.7 |
|  | 322.8 | 98.4 | 98.4 | 108.6 | 211.5 | 135.5 | 9 | 2523.3 | 1975.9 | 2599.9 | 5004.9 | 3919.1 | 5156.9 |
|  | 340.6 | 99.4 | 99.4 | 108.6 | 211.5 | 135.5 | 9 | 2526.8 | 1979.1 | 2603.5 | 5012.0 | 3925.5 | 5164.1 |
|  | 382.0 | 98.4 | 98.4 | 108.6 | 211.5 | 135.5 | 9 | 2530.8 | 1982.2 | 2607.1 | 5019.9 | 3931.8 | 5171.2 |
|  | 414.8 | 101.1 | 101.1 | 108.6 | 208.1 | 135.5 | 9 | 2535.1 | 1985.5 | 2610.7 | 5028.4 | 3938.2 | 5178.3 |
|  | 406.8 | 102.9 | 102.9 | 111.3 | 208.1 | 135.5 | 9 | 2539.4 | 1988.8 | 2614.3 | 5036.9 | 3944.7 | 5185.4 |
|  | 408.4 | 107.5 | 107.5 | 117.8 | 208.1 | 135.5 | 9 | 2543.6 | 1992.2 | 2617.9 | 5045.3 | 3951.6 | 5192.5 |
|  | 409.9 | 106.5 | 106.5 | 121.7 | 208.1 | 135.5 | 9 | 2547.9 | 1995.7 | 2621.4 | 5053.8 | 3958.5 | 5199.6 |
|  | 406.9 | 109.3 | 109.3 | 124.4 | 208.1 | 135.5 | 9 | 2552.1 | 1999.3 | 2625.0 | 5062.2 | 3965.6 | 5206.7 |
|  | 406.4 | 110.2 | 110.2 | 125.5 | 208.1 | 135.5 | 9 | 2556.4 | 2002.9 | 2628.6 | 5070.6 | 3972.8 | 5213.8 |
|  | 408.9 | 111.2 | 111.2 | 128.3 | 208.1 | 135.5 | 9 | 2560.6 | 2006.6 | 2632.2 | 5079.0 | 3980.0 | 5220.9 |
|  | 406.3 | 112.1 | 112.1 | 129.4 | 208.1 | 137.0 | 9 | 2564.9 | 2010.2 | 2635.8 | 5087.4 | 3987.3 | 5228.1 |
|  | 408.4 | 111.1 | 111.1 | 129.4 | 208.1 | 137.0 | 9 | 2569.1 | 2013.9 | 2639.4 | 5095.8 | 3994.6 | 5235.2 |
|  | 408.1 | 113.0 | 113.0 | 127.8 | 208.1 | 137.0 | 9 | 2573.4 | 2017.6 | 2643.0 | 5104.3 | 4001.9 | 5242.3 |
|  | 405.5 | 112.0 | 112.0 | 130.6 | 208.1 | 137.0 | 9 | 2577.6 | 2021.3 | 2646.6 | 5112.7 | 4009.2 | 5249.5 |
|  | 407.6 | 112.0 | 112.0 | 133.4 | 208.1 | 137.0 | 9 | 2581.8 | 2025.0 | 2650.2 | 5121.1 | 4016.6 | 5256.6 |
|  | 407.5 | 113.9 | 113.9 | 133.4 | 208.1 | 137.0 | 9 | 2586.1 | 2028.8 | 2653.8 | 5129.5 | 4024.1 | 5263.7 |
|  | 405.3 | 113.9 | 113.9 | 131.7 | 208.1 | 137.0 | 9 | 2590.3 | 2032.5 | 2657.3 | 5137.9 | 4031.5 | 5270.8 |
|  | 397.8 | 113.9 | 113.9 | 131.7 | 208.1 | 137.0 | 9 | 2594.4 | 2036.3 | 2660.9 | 5146.1 | 4038.9 | 5278.0 |
|  | 395.1 | 112.0 | 112.0 | 128.9 | 208.1 | 138.5 | 9 | 2598.6 | 2039.9 | 2664.6 | 5154.3 | 4046.2 | 5285.1 |
|  | 395.5 | 112.0 | 112.0 | 131.7 | 208.1 | 138.5 | 9 | 2602.7 | 2043.6 | 2668.2 | 5162.4 | 4053.6 | 5292.3 |
|  | 397.9 | 113.9 | 113.9 | 131.7 | 208.1 | 138.5 | 9 | 2606.8 | 2047.4 | 2671.8 | 5170.6 | 4061.0 | 5299.5 |
|  | 392.9 | 112.0 | 112.0 | 131.7 | 208.1 | 138.5 | 9 | 2610.9 | 2051.1 | 2675.4 | 5178.8 | 4068.3 | 5306.6 |
|  | 397.2 | 113.9 | 113.9 | 131.7 | 208.1 | 140.0 | 9 | 2615.1 | 2054.8 | 2679.0 | 5187.0 | 4075.8 | 5313.8 |
|  | 397.2 | 112.9 | 112.9 | 131.7 | 208.1 | 140.0 | 9 | 2619.2 | 2058.6 | 2682.6 | 5195.2 | 4083.2 | 5321.0 |


| Day | $\begin{gathered} \hline \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \text { G601 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G602 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \text { G603 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \text { G354 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \text { G393 } \\ \text { cfs } \end{gathered}$ | Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | G601-3 cfs | $\begin{aligned} & \text { G393+G354 } \\ & \text { Cfs } \end{aligned}$ | $\begin{aligned} & \hline \text { G600 } \\ & \text { ac-ft } \end{aligned}$ | $\begin{gathered} \text { G601-3 } \\ \text { ac-ft } \end{gathered}$ | G393+G354 $\mathrm{ac}-\mathrm{ft}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 397.0 | 112.9 | 112.9 | 130.0 | 208.1 | 140.0 | 9 | 2623.3 | 2062.3 | 2686.3 | 5203.4 | 4090.5 | 5328.2 |
|  | 394.2 | 113.9 | 113.9 | 130.0 | 208.1 | 140.0 | 9 | 2627.4 | 2066.0 | 2689.9 | 5211.5 | 4097.9 | 5335.4 |
|  | 396.8 | 112.9 | 112.9 | 130.0 | 208.1 | 140.0 | 9 | 2631.6 | 2069.7 | 2693.5 | 5219.7 | 4105.3 | 5342.6 |
|  | 396.8 | 112.9 | 112.9 | 130.0 | 208.1 | 141.5 | 9 | 2635.7 | 2073.4 | 2697.2 | 5227.9 | 4112.6 | 5349.8 |
|  | 393.9 | 112.9 | 112.9 | 130.0 | 208.1 | 141.5 | 9 | 2639.8 | 2077.1 | 2700.8 | 5236.1 | 4120.0 | 5357.0 |
|  | 394.2 | 112.9 | 112.9 | 130.0 | 211.5 | 141.5 | 9 | 2643.9 | 2080.8 | 2704.5 | 5244.2 | 4127.3 | 5364.3 |
|  | 396.1 | 112.9 | 112.9 | 128.3 | 211.5 | 141.5 | 9 | 2648.0 | 2084.5 | 2708.1 | 5252.4 | 4134.6 | 5371.6 |
|  | 393.6 | 112.9 | 112.9 | 131.2 | 211.5 | 143.0 | 9 | 2652.1 | 2088.2 | 2711.8 | 5260.5 | 4142.0 | 5378.9 |
|  | 391.4 | 112.9 | 112.9 | 128.3 | 211.5 | 143.0 | 9 | 2656.2 | 2091.9 | 2715.5 | 5268.6 | 4149.3 | 5386.3 |
|  | 396.0 | 112.9 | 112.9 | 128.3 | 211.5 | 143.0 | 9 | 2660.3 | 2095.6 | 2719.2 | 5276.8 | 4156.6 | 5393.6 |
|  | 393.4 | 112.9 | 112.9 | 128.3 | 211.5 | 143.0 | 9 | 2664.4 | 2099.3 | 2722.9 | 5284.9 | 4163.9 | 5400.9 |
|  | 396.0 | 112.9 | 112.9 | 128.3 | 211.5 | 143.0 | 9 | 2668.6 | 2103.0 | 2726.6 | 5293.1 | 4171.3 | 5408.2 |
|  | 395.8 | 112.9 | 112.9 | 131.2 | 211.5 | 144.5 | 9 | 2672.7 | 2106.7 | 2730.3 | 5301.3 | 4178.6 | 5415.6 |
|  | 393.2 | 112.9 | 112.9 | 126.5 | 211.5 | 144.5 | 9 | 2676.8 | 2110.4 | 2734.0 | 5309.4 | 4185.9 | 5422.9 |
|  | 395.8 | 112.9 | 112.9 | 126.5 | 211.5 | 144.5 | 9 | 2680.9 | 2114.0 | 2737.7 | 5317.6 | 4193.2 | 5430.3 |
|  | 395.7 | 112.9 | 112.9 | 126.5 | 211.5 | 144.5 | 9 | 2685.0 | 2117.7 | 2741.4 | 5325.8 | 4200.5 | 5437.7 |
|  | 395.6 | 111.8 | 111.8 | 129.4 | 214.9 | 144.5 | 9 | 2689.1 | 2121.4 | 2745.2 | 5333.9 | 4207.8 | 5445.1 |
|  | 395.4 | 111.8 | 111.8 | 129.4 | 214.9 | 146.1 | 9 | 2693.3 | 2125.1 | 2749.0 | 5342.1 | 4215.1 | 5452.5 |
|  | 395.0 | 111.8 | 111.8 | 129.4 | 214.9 | 146.1 | 9 | 2697.4 | 2128.7 | 2752.7 | 5350.3 | 4222.3 | 5460.0 |
|  | 390.4 | 111.8 | 111.8 | 129.4 | 214.9 | 146.1 | 9 | 2701.4 | 2132.4 | 2756.5 | 5358.3 | 4229.6 | 5467.5 |
|  | 392.8 | 111.8 | 111.8 | 129.4 | 214.9 | 146.1 | 9 | 2705.5 | 2136.1 | 2760.2 | 5366.4 | 4236.9 | 5474.9 |
|  | 390.2 | 111.8 | 111.8 | 127.6 | 214.9 | 146.1 | 9 | 2709.6 | 2139.8 | 2764.0 | 5374.5 | 4244.2 | 5482.4 |
|  | 392.5 | 111.8 | 111.8 | 127.6 | 214.9 | 146.1 | 9 | 2713.7 | 2143.4 | 2767.8 | 5382.6 | 4251.5 | 5489.8 |
|  | 392.4 | 111.8 | 111.8 | 127.6 | 214.9 | 147.6 | 9 | 2717.8 | 2147.1 | 2771.5 | 5390.7 | 4258.7 | 5497.3 |
|  | 392.1 | 111.8 | 111.8 | 127.6 | 214.9 | 147.6 | 9 | 2721.9 | 2150.7 | 2775.3 | 5398.8 | 4266.0 | 5504.8 |
|  | 390.1 | 111.8 | 111.8 | 127.6 | 214.9 | 147.6 | 9 | 2725.9 | 2154.4 | 2779.1 | 5406.9 | 4273.2 | 5512.3 |
|  | 391.9 | 111.8 | 111.8 | 125.8 | 218.4 | 147.6 | 9 | 2730.0 | 2158.0 | 2782.9 | 5415.0 | 4280.4 | 5519.9 |
|  | 391.9 | 110.7 | 110.7 | 125.8 | 218.4 | 147.6 | 9 | 2734.1 | 2161.6 | 2786.7 | 5423.1 | 4287.6 | 5527.4 |
|  | 394.3 | 111.8 | 111.8 | 125.8 | 218.4 | 147.6 | 9 | 2738.2 | 2165.3 | 2790.5 | 5431.2 | 4294.8 | 5535.0 |
|  | 391.9 | 110.7 | 110.7 | 125.8 | 218.4 | 149.1 | 9 | 2742.3 | 2168.9 | 2794.3 | 5439.3 | 4302.0 | 5542.6 |
|  | 393.8 | 110.7 | 110.7 | 125.8 | 218.4 | 149.1 | 9 | 2746.4 | 2172.5 | 2798.2 | 5447.5 | 4309.2 | 5550.2 |
|  | 394.1 | 110.7 | 110.7 | 125.8 | 218.4 | 149.1 | 9 | 2750.5 | 2176.1 | 2802.0 | 5455.6 | 4316.4 | 5557.8 |
|  | 393.9 | 110.7 | 110.7 | 125.8 | 218.4 | 149.1 | 9 | 2754.6 | 2179.7 | 2805.8 | 5463.7 | 4323.5 | 5565.4 |
|  | 391.5 | 110.7 | 110.7 | 125.8 | 218.4 | 149.1 | 9 | 2758.7 | 2183.4 | 2809.7 | 5471.8 | 4330.7 | 5573.0 |
|  | 391.7 | 110.7 | 110.7 | 125.8 | 218.4 | 149.1 | 9 | 2762.8 | 2187.0 | 2813.5 | 5479.9 | 4337.9 | 5580.6 |
|  | 391.5 | 110.7 | 110.7 | 123.9 | 218.4 | 150.7 | 9 | 2766.8 | 2190.6 | 2817.3 | 5488.0 | 4345.0 | 5588.2 |
|  | 393.7 | 110.7 | 110.7 | 123.9 | 218.4 | 150.7 | 9 | 2770.9 | 2194.2 | 2821.2 | 5496.1 | 4352.2 | 5595.8 |
|  | 388.5 | 110.7 | 110.7 | 123.9 | 218.4 | 150.7 | 9 | 2775.0 | 2197.8 | 2825.0 | 5504.2 | 4359.3 | 5603.4 |
| 10 | 388.5 | 110.7 | 110.7 | 123.9 | 221.8 | 150.7 | 10 | 2779.0 | 2201.4 | 2828.9 | 5512.2 | 4366.4 | 5611.1 |
|  | 391.0 | 110.7 | 110.7 | 123.9 | 221.8 | 150.7 | 10 | 2783.1 | 2205.0 | 2832.8 | 5520.3 | 4373.6 | 5618.8 |
|  | 391.0 | 110.7 | 110.7 | 123.9 | 221.8 | 150.7 | 10 | 2787.2 | 2208.6 | 2836.7 | 5528.4 | 4380.7 | 5626.5 |
|  | 390.8 | 110.7 | 110.7 | 123.9 | 221.8 | 152.2 | 10 | 2791.2 | 2212.2 | 2840.6 | 5536.4 | 4387.8 | 5634.2 |
|  | 393.3 | 110.7 | 110.7 | 123.9 | 221.8 | 152.2 | 10 | 2795.3 | 2215.8 | 2844.5 | 5544.6 | 4395.0 | 5642.0 |
|  | 391.0 | 110.7 | 110.7 | 122.0 | 221.8 | 152.2 | 10 | 2799.4 | 2219.3 | 2848.4 | 5552.6 | 4402.1 | 5649.7 |
|  | 390.8 | 109.6 | 109.6 | 122.0 | 221.8 | 152.2 | 10 | 2803.5 | 2222.9 | 2852.2 | 5560.7 | 4409.1 | 5657.4 |
|  | 393.2 | 109.6 | 109.6 | 122.0 | 221.8 | 152.2 | 10 | 2807.6 | 2226.4 | 2856.1 | 5568.8 | 4416.2 | 5665.2 |
|  | 388.3 | 110.7 | 110.7 | 122.0 | 221.8 | 152.2 | 10 | 2811.6 | 2230.0 | 2860.0 | 5576.9 | 4423.3 | 5672.9 |
|  | 393.0 | 109.6 | 109.6 | 122.0 | 221.8 | 152.2 | 10 | 2815.7 | 2233.6 | 2863.9 | 5585.0 | 4430.3 | 5680.6 |
|  | 390.7 | 109.6 | 109.6 | 122.0 | 221.8 | 152.2 | 10 | 2819.8 | 2237.1 | 2867.8 | 5593.1 | 4437.3 | 5688.4 |
|  | 391.2 | 111.6 | 111.6 | 122.0 | 221.8 | 153.8 | 10 | 2823.9 | 2240.7 | 2871.7 | 5601.1 | 4444.5 | 5696.1 |


| Day | $\begin{gathered} \hline \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \text { G601 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G602 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G603 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G354 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G393 } \\ \text { cfs } \end{gathered}$ | Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \text { G601-3 } \\ \text { cfs } \end{gathered}$ | $\begin{aligned} & \text { G393+G354 } \\ & \text { Cfs } \end{aligned}$ | $\begin{aligned} & \hline \text { G600 } \\ & \text { ac-ft } \end{aligned}$ | $\begin{gathered} \hline \text { G601-3 } \\ \text { ac-ft } \end{gathered}$ | $\begin{gathered} \text { G393+G354 } \\ \text { ac-ft } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 391.6 | 109.6 | 109.6 | 122.0 | 221.8 | 153.8 | 10 | 2827.9 | 2244.3 | 2875.7 | 5609.2 | 4451.5 | 5703.9 |
|  | 393.8 | 111.6 | 111.6 | 119.9 | 225.3 | 153.8 | 10 | 2832.0 | 2247.9 | 2879.6 | 5617.4 | 4458.6 | 5711.7 |
|  | 393.9 | 111.6 | 111.6 | 119.9 | 225.3 | 153.8 | 10 | 2836.1 | 2251.4 | 2883.6 | 5625.5 | 4465.7 | 5719.5 |
|  | 391.8 | 111.6 | 111.6 | 119.9 | 225.3 | 153.8 | 10 | 2840.2 | 2255.0 | 2887.5 | 5633.6 | 4472.8 | 5727.4 |
|  | 391.8 | 111.6 | 111.6 | 119.9 | 225.3 | 153.8 | 10 | 2844.3 | 2258.6 | 2891.5 | 5641.7 | 4479.9 | 5735.2 |
|  | 394.0 | 111.6 | 111.6 | 119.9 | 225.3 | 153.8 | 10 | 2848.4 | 2262.2 | 2895.4 | 5649.8 | 4487.0 | 5743.0 |
|  | 393.7 | 111.6 | 111.6 | 119.9 | 225.3 | 153.8 | 10 | 2852.5 | 2265.7 | 2899.4 | 5658.0 | 4494.1 | 5750.9 |
|  | 393.8 | 111.6 | 111.6 | 119.9 | 221.8 | 153.8 | 10 | 2856.6 | 2269.3 | 2903.3 | 5666.1 | 4501.2 | 5758.6 |
|  | 393.8 | 111.6 | 111.6 | 119.9 | 225.3 | 153.8 | 10 | 2860.7 | 2272.9 | 2907.2 | 5674.2 | 4508.2 | 5766.5 |
|  | 391.4 | 111.6 | 111.6 | 119.9 | 225.3 | 153.8 | 10 | 2864.8 | 2276.5 | 2911.2 | 5682.3 | 4515.3 | 5774.3 |
|  | 391.2 | 111.6 | 111.6 | 119.9 | 225.3 | 155.3 | 10 | 2868.9 | 2280.0 | 2915.1 | 5690.4 | 4522.4 | 5782.2 |
|  | 393.6 | 111.6 | 111.6 | 117.9 | 225.3 | 155.3 | 10 | 2873.0 | 2283.6 | 2919.1 | 5698.5 | 4529.5 | 5790.0 |
|  | 391.4 | 111.6 | 111.6 | 117.9 | 225.3 | 155.3 | 10 | 2877.0 | 2287.1 | 2923.1 | 5706.6 | 4536.5 | 5797.9 |
|  | 391.1 | 109.6 | 109.6 | 117.9 | 225.3 | 155.3 | 10 | 2881.1 | 2290.6 | 2927.0 | 5714.7 | 4543.5 | 5805.8 |
|  | 390.6 | 111.6 | 111.6 | 117.9 | 225.3 | 155.3 | 10 | 2885.2 | 2294.2 | 2931.0 | 5722.8 | 4550.5 | 5813.6 |
|  | 390.7 | 110.5 | 110.5 | 117.9 | 225.3 | 155.3 | 10 | 2889.3 | 2297.7 | 2935.0 | 5730.9 | 4557.5 | 5821.5 |
|  | 393.0 | 111.6 | 111.6 | 117.9 | 225.3 | 155.3 | 10 | 2893.4 | 2301.3 | 2938.9 | 5739.0 | 4564.6 | 5829.4 |
|  | 393.0 | 111.6 | 111.6 | 117.9 | 225.3 | 155.3 | 10 | 2897.4 | 2304.8 | 2942.9 | 5747.1 | 4571.6 | 5837.2 |
|  | 388.0 | 111.6 | 111.6 | 117.9 | 225.3 | 155.3 | 10 | 2901.5 | 2308.4 | 2946.9 | 5755.1 | 4578.7 | 5845.1 |
|  | 392.8 | 110.5 | 110.5 | 117.9 | 225.3 | 156.9 | 10 | 2905.6 | 2311.9 | 2950.8 | 5763.2 | 4585.7 | 5853.0 |
|  | 390.7 | 111.6 | 111.6 | 117.9 | 225.3 | 156.9 | 10 | 2909.7 | 2315.5 | 2954.8 | 5771.3 | 4592.7 | 5860.9 |
|  | 387.9 | 111.6 | 111.6 | 117.9 | 225.3 | 156.9 | 10 | 2913.7 | 2319.0 | 2958.8 | 5779.3 | 4599.8 | 5868.8 |
|  | 390.1 | 110.5 | 110.5 | 117.9 | 225.3 | 156.9 | 10 | 2917.8 | 2322.5 | 2962.8 | 5787.4 | 4606.8 | 5876.7 |
|  | 390.1 | 111.6 | 111.6 | 117.9 | 225.3 | 156.9 | 10 | 2921.8 | 2326.1 | 2966.8 | 5795.4 | 4613.8 | 5884.6 |
|  | 392.5 | 111.6 | 111.6 | 115.8 | 228.8 | 156.9 | 10 | 2925.9 | 2329.6 | 2970.8 | 5803.5 | 4620.8 | 5892.5 |
|  | 390.1 | 111.6 | 111.6 | 115.8 | 228.8 | 156.9 | 10 | 2930.0 | 2333.2 | 2974.8 | 5811.6 | 4627.8 | 5900.5 |
|  | 389.9 | 110.5 | 110.5 | 115.8 | 228.8 | 156.9 | 10 | 2934.0 | 2336.7 | 2978.8 | 5819.7 | 4634.8 | 5908.5 |
|  | 389.7 | 106.8 | 106.8 | 115.8 | 228.8 | 156.9 | 10 | 2938.1 | 2340.1 | 2982.8 | 5827.7 | 4641.6 | 5916.4 |
|  | 391.2 | 110.5 | 110.5 | 115.8 | 228.8 | 156.9 | 10 | 2942.2 | 2343.6 | 2986.8 | 5835.8 | 4648.5 | 5924.4 |
|  | 392.8 | 107.6 | 107.6 | 115.8 | 228.8 | 156.9 | 10 | 2946.3 | 2347.1 | 2990.9 | 5843.9 | 4655.4 | 5932.4 |
|  | 399.5 | 110.5 | 110.5 | 114.7 | 228.8 | 156.9 | 10 | 2950.4 | 2350.6 | 2994.9 | 5852.2 | 4662.3 | 5940.4 |
|  | 399.2 | 110.5 | 110.5 | 112.6 | 228.8 | 156.9 | 10 | 2954.6 | 2354.0 | 2998.9 | 5860.4 | 4669.2 | 5948.3 |
|  | 396.2 | 110.5 | 110.5 | 115.8 | 228.8 | 156.9 | 10 | 2958.7 | 2357.5 | 3002.9 | 5868.6 | 4676.2 | 5956.3 |
|  | 398.1 | 110.5 | 110.5 | 115.8 | 228.8 | 156.9 | 10 | 2962.9 | 2361.0 | 3006.9 | 5876.8 | 4683.1 | 5964.3 |
|  | 400.3 | 110.5 | 110.5 | 115.8 | 228.8 | 156.9 | 10 | 2967.0 | 2364.6 | 3011.0 | 5885.1 | 4690.1 | 5972.2 |
|  | 395.5 | 110.5 | 110.5 | 115.8 | 228.8 | 156.9 | 10 | 2971.1 | 2368.1 | 3015.0 | 5893.3 | 4697.0 | 5980.2 |
|  | 400.0 | 112.5 | 112.5 | 118.9 | 228.8 | 158.5 | 10 | 2975.3 | 2371.6 | 3019.0 | 5901.5 | 4704.2 | 5988.2 |
|  | 397.3 | 112.5 | 112.5 | 118.9 | 228.8 | 158.5 | 10 | 2979.4 | 2375.2 | 3023.0 | 5909.7 | 4711.3 | 5996.2 |
|  | 397.3 | 107.6 | 107.6 | 118.9 | 228.8 | 158.5 | 10 | 2983.6 | 2378.7 | 3027.1 | 5917.9 | 4718.2 | 6004.2 |
|  | 397.3 | 112.5 | 112.5 | 116.8 | 232.3 | 158.5 | 10 | 2987.7 | 2382.3 | 3031.1 | 5926.1 | 4725.2 | 6012.3 |
|  | 312.4 | 108.5 | 108.5 | 116.8 | 232.3 | 158.5 | 10 | 2991.0 | 2385.7 | 3035.2 | 5932.6 | 4732.1 | 6020.4 |
|  | 382.7 | 110.5 | 110.5 | 112.6 | 232.3 | 158.5 | 10 | 2995.0 | 2389.2 | 3039.3 | 5940.5 | 4739.0 | 6028.4 |
|  | 378.6 | 112.5 | 112.5 | 115.8 | 232.3 | 158.5 | 10 | 2998.9 | 2392.8 | 3043.4 | 5948.3 | 4746.0 | 6036.5 |
|  | 378.3 | 110.5 | 110.5 | 116.8 | 232.3 | 158.5 | 10 | 3002.8 | 2396.3 | 3047.4 | 5956.2 | 4753.0 | 6044.6 |
|  | 380.1 | 112.5 | 112.5 | 113.5 | 232.3 | 158.5 | 10 | 3006.8 | 2399.8 | 3051.5 | 5964.0 | 4760.0 | 6052.7 |
|  | 384.8 | 112.5 | 112.5 | 116.8 | 232.3 | 160.1 | 10 | 3010.8 | 2403.4 | 3055.6 | 5972.0 | 4767.1 | 6060.8 |
|  | 377.9 | 110.5 | 110.5 | 116.8 | 232.3 | 160.1 | 10 | 3014.8 | 2406.9 | 3059.7 | 5979.8 | 4774.1 | 6068.9 |
|  | 380.2 | 112.5 | 112.5 | 116.8 | 232.3 | 160.1 | 10 | 3018.7 | 2410.4 | 3063.8 | 5987.6 | 4781.1 | 6077.0 |
|  | 381.7 | 112.5 | 112.5 | 116.8 | 232.3 | 160.1 | 10 | 3022.7 | 2414.0 | 3067.9 | 5995.5 | 4788.2 | 6085.1 |
|  | 380.0 | 112.5 | 112.5 | 116.8 | 232.3 | 160.1 | 10 | 3026.6 | 2417.6 | 3071.9 | 6003.4 | 4795.2 | 6093.2 |


| Day | $\begin{gathered} \hline \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \text { G601 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G602 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \text { G603 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \text { G354 } \\ \text { cfs } \end{gathered}$ | $\begin{gathered} \hline \text { G393 } \\ \text { cfs } \end{gathered}$ | Day | $\begin{gathered} \text { G600 } \\ \text { cfs } \end{gathered}$ | $\begin{aligned} & \hline \text { G601-3 } \\ & \text { cfs } \end{aligned}$ | $\begin{aligned} & \hline \text { G393+G354 } \\ & \text { Cfs } \end{aligned}$ | $\begin{aligned} & \hline \text { G600 } \\ & \text { ac-ft } \end{aligned}$ | $\begin{gathered} \hline \text { G601-3 } \\ \text { ac-ft } \end{gathered}$ | $\begin{gathered} \text { G393+G354 } \\ \text { ac-ft } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 377.6 | 112.5 | 112.5 | 116.8 | 232.3 | 160.1 | 10 | 3030.6 | 2421.1 | 3076.0 | 6011.2 | 4802.3 | 6101.3 |
|  | 382.4 | 112.5 | 112.5 | 116.8 | 232.3 | 160.1 | 10 | 3034.6 | 2424.7 | 3080.1 | 6019.1 | 4809.4 | 6109.4 |
|  | 379.8 | 111.4 | 111.4 | 116.8 | 232.3 | 160.1 | 10 | 3038.5 | 2428.2 | 3084.2 | 6026.9 | 4816.4 | 6117.5 |
|  | 379.4 | 112.5 | 112.5 | 116.8 | 232.3 | 160.1 | 10 | 3042.5 | 2431.8 | 3088.3 | 6034.7 | 4823.4 | 6125.6 |
|  | 382.0 | 111.4 | 111.4 | 116.8 | 235.9 | 160.1 | 10 | 3046.5 | 2435.3 | 3092.4 | 6042.6 | 4830.5 | 6133.8 |
|  | 377.6 | 111.4 | 111.4 | 114.5 | 235.9 | 160.1 | 10 | 3050.4 | 2438.8 | 3096.5 | 6050.4 | 4837.4 | 6142.0 |
|  | 377.5 | 111.4 | 111.4 | 114.5 | 235.9 | 160.1 | 10 | 3054.3 | 2442.3 | 3100.7 | 6058.2 | 4844.4 | 6150.2 |
|  | 381.2 | 111.4 | 111.4 | 114.5 | 235.9 | 160.1 | 10 | 3058.3 | 2445.9 | 3104.8 | 6066.1 | 4851.4 | 6158.3 |
|  | 381.9 | 111.4 | 111.4 | 114.5 | 235.9 | 160.1 | 10 | 3062.3 | 2449.4 | 3108.9 | 6074.0 | 4858.3 | 6166.5 |
|  | 379.1 | 111.4 | 111.4 | 114.5 | 235.9 | 161.6 | 10 | 3066.2 | 2452.9 | 3113.0 | 6081.8 | 4865.3 | 6174.7 |
|  | 381.0 | 112.5 | 112.5 | 114.5 | 235.9 | 161.6 | 10 | 3070.2 | 2456.4 | 3117.2 | 6089.7 | 4872.3 | 6182.9 |
|  | 378.9 | 111.4 | 111.4 | 114.5 | 235.9 | 161.6 | 10 | 3074.1 | 2459.9 | 3121.3 | 6097.5 | 4879.3 | 6191.2 |
|  | 377.1 | 112.5 | 112.5 | 114.5 | 235.9 | 161.6 | 10 | 3078.1 | 2463.5 | 3125.5 | 6105.3 | 4886.3 | 6199.4 |
|  | 379.2 | 111.4 | 111.4 | 114.5 | 235.9 | 161.6 | 10 | 3082.0 | 2467.0 | 3129.6 | 6113.2 | 4893.3 | 6207.6 |
|  | 378.8 | 111.4 | 111.4 | 114.5 | 235.9 | 161.6 | 10 | 3086.0 | 2470.5 | 3133.7 | 6121.0 | 4900.2 | 6215.8 |
|  | 378.5 | 111.4 | 111.4 | 114.5 | 235.9 | 161.6 | 10 | 3089.9 | 2474.0 | 3137.9 | 6128.8 | 4907.2 | 6224.0 |
|  | 381.1 | 111.4 | 111.4 | 114.5 | 235.9 | 161.6 | 10 | 3093.9 | 2477.5 | 3142.0 | 6136.7 | 4914.2 | 6232.2 |
|  | 376.2 | 111.4 | 111.4 | 114.5 | 235.9 | 161.6 | 10 | 3097.8 | 2481.0 | 3146.2 | 6144.5 | 4921.1 | 6240.4 |
|  | 376.6 | 111.4 | 111.4 | 114.5 | 235.9 | 161.6 | 10 | 3101.7 | 2484.5 | 3150.3 | 6152.2 | 4928.1 | 6248.6 |
|  | 378.6 | 111.4 | 111.4 | 114.5 | 235.9 | 161.6 | 10 | 3105.7 | 2488.1 | 3154.5 | 6160.1 | 4935.1 | 6256.9 |
|  | 380.8 | 111.4 | 111.4 | 112.2 | 235.9 | 161.6 | 10 | 3109.6 | 2491.6 | 3158.6 | 6167.9 | 4942.0 | 6265.1 |
|  | 376.0 | 111.4 | 111.4 | 112.2 | 235.9 | 161.6 | 10 | 3113.5 | 2495.0 | 3162.7 | 6175.7 | 4948.9 | 6273.3 |
|  | 380.5 | 111.4 | 111.4 | 112.2 | 235.9 | 161.6 | 10 | 3117.5 | 2498.5 | 3166.9 | 6183.6 | 4955.8 | 6281.5 |
|  | 378.4 | 111.4 | 111.4 | 112.2 | 235.9 | 161.6 | 10 | 3121.4 | 2502.0 | 3171.0 | 6191.4 | 4962.8 | 6289.7 |
|  | 378.6 | 111.4 | 111.4 | 112.2 | 235.9 | 163.2 | 10 | 3125.4 | 2505.5 | 3175.2 | 6199.2 | 4969.7 | 6297.9 |
|  | 378.0 | 111.4 | 111.4 | 112.2 | 235.9 | 163.2 | 10 | 3129.3 | 2509.0 | 3179.3 | 6207.0 | 4976.6 | 6306.2 |
|  | 380.3 | 111.4 | 111.4 | 112.2 | 235.9 | 163.2 | 10 | 3133.3 | 2512.5 | 3183.5 | 6214.9 | 4983.5 | 6314.4 |
|  | 378.1 | 111.4 | 111.4 | 112.2 | 239.4 | 163.2 | 10 | 3137.2 | 2516.0 | 3187.7 | 6222.7 | 4990.4 | 6322.8 |
|  | 375.9 | 111.4 | 111.4 | 112.2 | 239.4 | 163.2 | 10 | 3141.1 | 2519.5 | 3191.9 | 6230.4 | 4997.4 | 6331.1 |
|  | 376.0 | 111.4 | 111.4 | 112.2 | 239.4 | 163.2 | 10 | 3145.1 | 2523.0 | 3196.1 | 6238.2 | 5004.3 | 6339.4 |
|  | 380.7 | 111.4 | 111.4 | 112.2 | 239.4 | 163.2 | 10 | 3149.0 | 2526.4 | 3200.3 | 6246.1 | 5011.2 | 6347.7 |
|  | 375.6 | 111.4 | 111.4 | 112.2 | 239.4 | 163.2 | 10 | 3152.9 | 2529.9 | 3204.5 | 6253.8 | 5018.1 | 6356.0 |
|  | 377.9 | 111.4 | 111.4 | 112.2 | 239.4 | 163.2 | 10 | 3156.9 | 2533.4 | 3208.6 | 6261.7 | 5025.0 | 6364.4 |
|  | 375.5 | 111.4 | 111.4 | 112.2 | 239.4 | 163.2 | 10 | 3160.8 | 2536.9 | 3212.8 | 6269.4 | 5032.0 | 6372.7 |
| 11 | 375.5 | 111.4 | 111.4 | 112.2 | 239.4 | 163.2 | 11 | 3164.7 | 2540.4 | 3217.0 | 6277.2 | 5038.9 | 6381.0 |
|  | 377.1 | 111.4 | 111.4 | 112.2 | 239.4 | 163.2 | 11 | 3168.6 | 2543.9 | 3221.2 | 6285.0 | 5045.8 | 6389.3 |
|  | 375.3 | 112.5 | 112.5 | 112.2 | 239.4 | 163.2 | 11 | 3172.5 | 2547.4 | 3225.4 | 6292.7 | 5052.8 | 6397.6 |
|  | 375.1 | 111.4 | 111.4 | 112.2 | 239.4 | 163.2 | 11 | 3176.4 | 2550.9 | 3229.6 | 6300.5 | 5059.7 | 6405.9 |
|  | 374.7 | 111.4 | 111.4 | 112.2 | 239.4 | 163.2 | 11 | 3180.3 | 2554.4 | 3233.8 | 6308.2 | 5066.6 | 6414.3 |
|  | 377.6 | 111.4 | 111.4 | 112.2 | 239.4 | 163.2 | 11 | 3184.3 | 2557.9 | 3238.0 | 6316.0 | 5073.5 | 6422.6 |
|  | 374.7 | 111.4 | 111.4 | 112.2 | 239.4 | 163.2 | 11 | 3188.2 | 2561.4 | 3242.2 | 6323.8 | 5080.5 | 6430.9 |
|  | 377.0 | 111.4 | 111.4 | 109.9 | 239.4 | 163.2 | 11 | 3192.1 | 2564.8 | 3246.4 | 6331.5 | 5087.3 | 6439.2 |
|  | 379.1 | 106.5 | 106.5 | 109.9 | 239.4 | 163.2 | 11 | 3196.1 | 2568.2 | 3250.6 | 6339.4 | 5094.0 | 6447.5 |
|  | 376.8 | 111.4 | 111.4 | 109.9 | 239.4 | 163.2 | 11 | 3200.0 | 2571.7 | 3254.8 | 6347.2 | 5100.9 | 6455.9 |
|  | 393.8 | 108.5 | 108.5 | 109.9 | 239.4 | 163.2 | 11 | 3204.1 | 2575.1 | 3259.0 | 6355.3 | 5107.6 | 6464.2 |
|  | 390.2 | 111.4 | 111.4 | 112.2 | 239.4 | 163.2 | 11 | 3208.1 | 2578.5 | 3263.2 | 6363.4 | 5114.5 | 6472.5 |
|  | 394.3 | 113.4 | 113.4 | 108.9 | 239.4 | 163.2 | 11 | 3212.3 | 2582.0 | 3267.4 | 6371.5 | 5121.5 | 6480.8 |
|  | 386.8 | 111.4 | 111.4 | 113.2 | 239.4 | 163.2 | 11 | 3216.3 | 2585.5 | 3271.6 | 6379.5 | 5128.4 | 6489.1 |
|  | 390.9 | 112.2 | 112.2 | 113.2 | 239.4 | 164.8 | 11 | 3220.4 | 2589.1 | 3275.8 | 6387.6 | 5135.4 | 6497.5 |
|  | 391.9 | 112.2 | 112.2 | 113.2 | 239.4 | 164.8 | 11 | 3224.4 | 2592.6 | 3280.0 | 6395.7 | 5142.4 | 6505.8 |


| Day | G600 | G601 | G602 | G603 | G354 | G393 | Day | G600 | G601-3 | G393+G354 | G600 | G601-3 | G393+G354 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | cfs | cfs | cfs | cfs | cfs | cfs |  | cfs | cfs | Cfs | ac-ft | ac-ft | ac-ft |
|  | 388.8 | 112.2 | 112.2 | 113.2 | 239.4 | 164.8 | 11 | 3228.5 | 2596.1 | 3284.2 | 6403.7 | 5149.4 | 6514.2 |


[^0]:    Notes: All discharges are in cfs. All length dimensions are in ft . Section width/depth is diameter for circular culverts.

