

DRE-93

DRAFT – Clad Model and Its Applications

FOY

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## ABSTRACT

The CLAD model is an abbreviation for concentrations, loadings and discharge model. This model was developed to estimate future basin discharges and concentrations of conservative chemical constituents for these discharges. It is a simplistic mass balance model for both quantity and quality. Output is on a monthly basis. The model is deterministic and is rainfall driven. It requires historical discharges for the period of record to be analyzed. The mass balance computations call for the January 1975 version of the Corps of Engineer's STORM model (STORM stands for storage, treatment, overflow and runoff model).

The STORM requires hourly rainfall, land uses and their corresponding pollutant loading rates along with some general basin description parameters.

The CLAD model estimates future discharges by (a) calculating the historical groundwater contributions to discharges (i.e., by subtracting surface runoff of the STORM model from the historical discharges), (b) accounting for changes in groundwater evapotranspiration and surface water evaporation, and (c) adding the net groundwater contributions to the surface water runoff estimated from STORM.

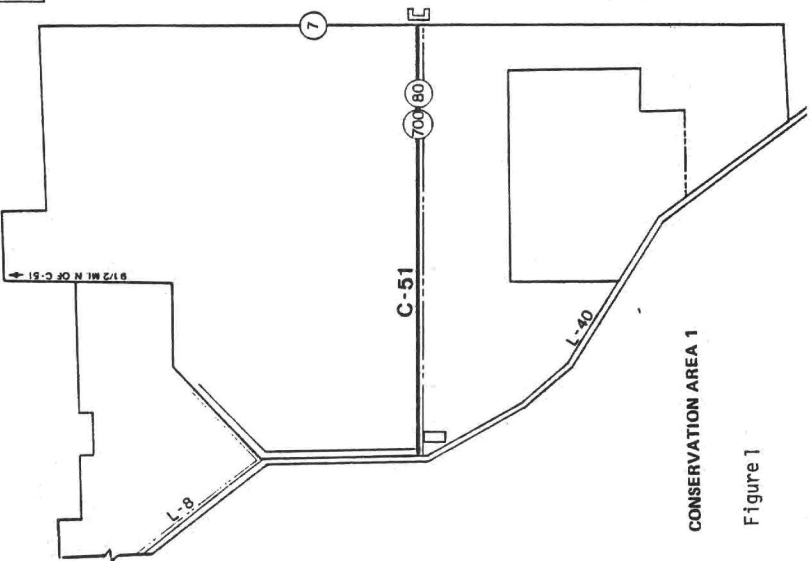
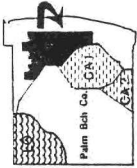
As a part of water quality calculations, the CLAD model estimates the net amount of water quality concentrations from all the historical nonpoint sources and sinks by subtracting surface runoff contributions (as estimated by the STORM model) from the historical water quality data. These monthly concentrations are assumed to be constant in the analysis until further definition can be made. In other words, both historical and future concentrations for all sources and sinks (other than surface water) are assumed to be equal. Using surface runoff, groundwater flow contributions, the surface runoff quality, and quality of the nonpoint sources and sinks, the CLAD model estimates the future water quality of basin discharges.



## 1. INTRODUCTION

There were several water resources planning alternatives that were considered by the South Florida Water Management District while preparing its Water Use and Supply Development Plan for the Lower East Coast Planning Area in South Florida. One of these alternatives is known as the backpumping scheme, where normal eastward flow of excess water to the Atlantic Ocean is reversed by pumping it westward to the conservation areas to increase the water supply capability for the regions of south Florida during the dry period (November through April). This backpumping alternative has several elements associated with it. These elements (including technical, economic, water quality factors, etc.) need to be thoroughly analyzed before an overall impact of the backpumping alternative is assessed. One of the useful inputs is related to the estimation of both quantity and quality of the canal water that will be backpumped to the three conservation areas. In other words, this is a situation where the estimation of the water quantity and quality for future land use scenarios is required at the current time. This type of situation, which is often encountered in water resources planning, demands a reliable mathematical model. To fulfill such a need, the CLAD model was designed. The primary purpose of the CLAD model, as described in this report, is to estimate the quantity and quality of backpumped water that is received from the drainage basin of three lower east coast canals (West Palm Beach Canal basin (C-51 basin), Hillsboro Canal basin and Tamiami Canal basin (C-4 basin)). It should be noted that the model is set up in a manner that is consistent with two other District models: the linear optimization model which analyzes different elements of the backpumping scheme but utilizes the output of the CLAD model and the water quality model. These backpumping alternatives call for building surface water control structures to separate these basins into east and west subbasins, see Figures 1, 2,

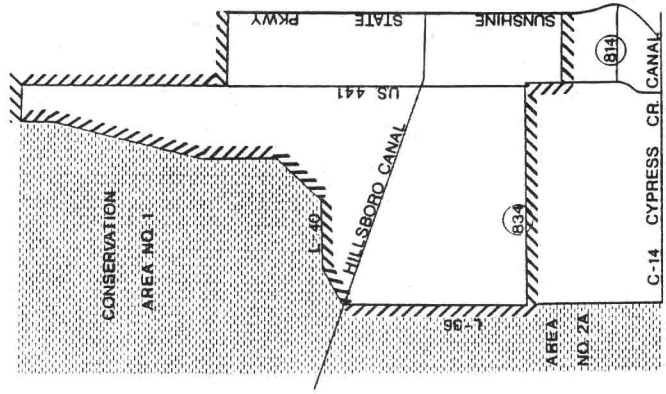
WEST PALM BEACH CANAL (C-51)  
BACKPUMPING AREA



CONSERVATION AREA 1

Figure 1

HILLSBORO CANAL



□ PUMP STATION  
▭ NEW STRUCTURE

Figure 2



# TAMIAMI CANAL (C-4) BACKPUMPING AREA

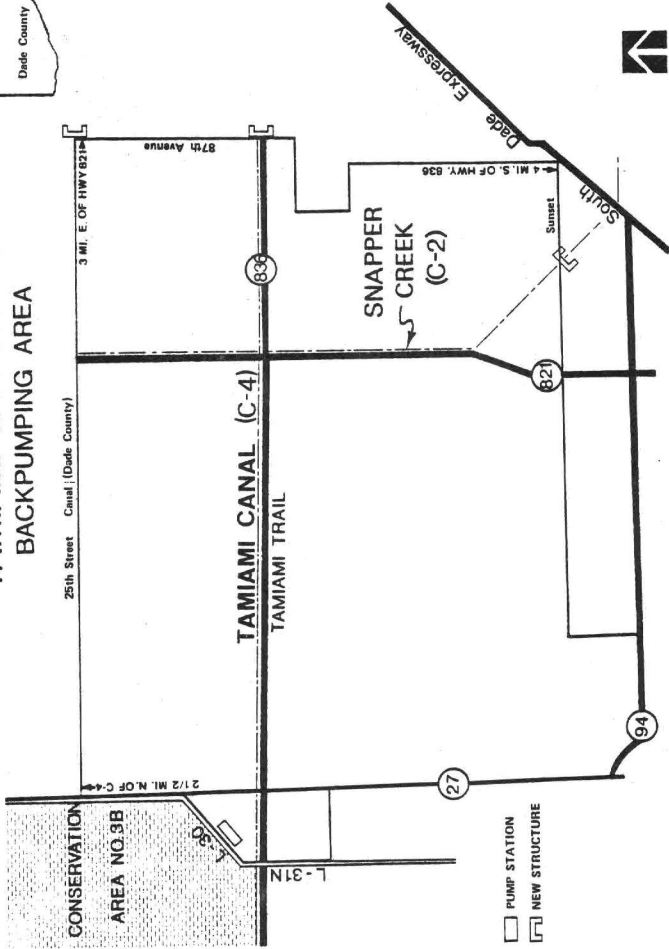


Figure 3

and 3. The east basins would still discharge to tidewaters, while the west basins would be totally or partially backpumped to the Conservation Areas (see Figure 4).

## 2. DESCRIPTION OF THE CLAD MODEL

Basically, the CLAD model (CLAD stands for concentrations, loadings and discharge) has the following three major components:

1. The Discharge model
2. The STORM model
3. Quality calculations

These components are discussed below:

### 2.1 THE DISCHARGE MODEL

Using a water balance approach on a monthly basis, the discharge model estimates future discharges from the following equations:

$$\text{Inflow} - \text{Outflow} = \text{Storage Change} \quad (1)$$

Using various inflow, outflow and storage entities, equation (1) is rewritten as shown below:

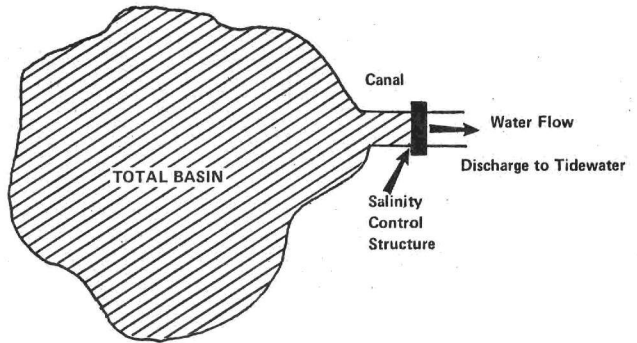
$$\begin{aligned} &\text{Rainfall (R)} - \text{Discharge (DIS)} - \text{Surface Water Evapotranspiration (SWET)} \\ &- \text{groundwater evapotranspiration} = \text{groundwater outward seepage} - \text{ground-} \\ &\text{water inward seepage} + \text{depression storage evapotranspiration (DSET)} + \\ &\text{groundwater storage change (includes surface water storage change)} \end{aligned}$$

Surface water storage was considered an extension of the groundwater system. The basins modeled have controlled surface water (canal) elevations.

Combining groundwater terms together, we define:

$$\begin{aligned} \text{net groundwater loss (NGWL)} = &\text{groundwater outward seepage} - \text{groundwater} \\ &\text{inward seepage} + \text{groundwater storage change} + \text{groundwater evapotranspiration} \quad (3) \end{aligned}$$

PRESENT



FUTURE  
BACKPUMPING

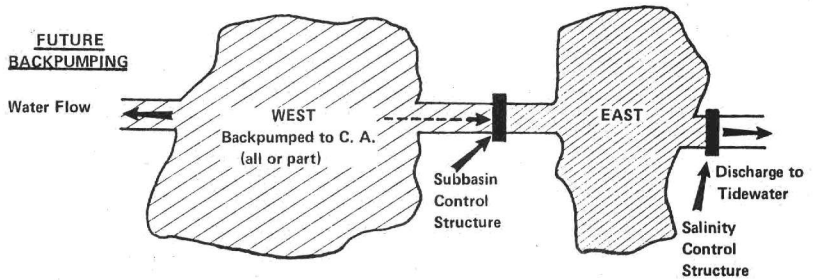


FIGURE 4

SCHEMATICS OF THE BACKPUMPING ALTERNATIVE

This simplification provides us with the following water balance equation

$$R = DIS + DSET + SWET + NGWL \quad (4)$$

where

R = Rainfall data largely obtained from United States Weather Bureau data,

DIS = Surface water discharge of the basin obtained from United States Geological Survey water supply papers,

SWET = Evapotranspiration from surface water which is determined by multiplying monthly potential evaporation rates by the evaporation coefficient and area of open surface water.

NGWL = Net groundwater loss which is estimated

DSET = Evapotranspiration from depression storage. This is calculated using the following equation:

$$DSET = R - (\text{Runoff})/(C) \quad (5)$$

where

R = hourly rainfall

Runoff = hourly runoff computed by STORM model

C = Area weighted runoff coefficient. (This coefficient can be computed as weighted average of various land uses).

Using present combinations of land use related input data and observed sets of rainfall (R) and discharges (DIS), net groundwater losses for a historical case are estimated by

$$NGWLH = R - DISH - DSETH - SWETH \quad (6)$$

where

NGWLH = Net groundwater loss for historical case

R = Rainfall (as before)  
 DISH = Historical discharge  
 DSETH = Evapotranspiration from depression storage  
           for historical case,  
 SWETH = Evapotranspiration from surface water for historical case.

It is to be noted that Equation 6 is a rearrangement of Equation 4 and H is added to the end of every term to represent the historical case.

The discharge model estimates future discharges in the following steps (Please note that F is added to the end of every term of the mass balance Equation 4 to represent future condition).

- (1) Use the same rainfall record as was used for the historical case
- (2) Assuming that future groundwater losses decrease as the impervious cover increases, future net groundwater losses (NGWLF) are estimated by

$$\begin{aligned} \text{NGWLF} &= \text{NGWLH}/(1+\text{IFI}) \quad \text{if } \text{NGWLH} > 0 \\ \text{and} & \\ \text{NGWLF} &= (\text{NGWLH})(1+\text{IFI}) \quad \text{if } \text{NGWLH} < 0 \end{aligned} \tag{7}$$

where

$$\begin{aligned} \text{IFI} &= \text{Increase in impervious fraction} \\ &= \sum_{i=1}^N [(\text{IF}_i)(\text{Area}_i)/\text{Total Area}]_{\text{future condition}} \\ &\quad - \sum_{i=1}^N [(\text{IF}_i)(\text{Area}_i)/\text{Total Area}]_{\text{historical condition}} \end{aligned} \tag{8}$$

and  $\text{IF}_i$  = Impervious Fraction for land use i

- (3) Estimate Evapotranspiration from depression storage for future conditions (DSETF) using Equation 5.
- (4) Evapotranspiration from surface water (SWETF) is a model input

- (5) Compute future discharges (DISF) by plugging all the known terms of the righthand side of the following equation:

$$\text{DISF} = R - \text{DSETF} - \text{SEWTF} - \text{NGWLF} \quad (9)$$

- (6) The nonpoint discharge (ONPSQN) is finally estimated as

$$\text{ONPSQN} = \text{DISF} = \text{Surface runoff} \quad (10)$$

The discharge model is summarized in Figure 5.

Surface runoff is computed by the STORM model which is briefly described in the following section.

## 2.2 STORM MODEL

The STORM (storage, treatment, overflow and runoff) model is a mathematical model developed by the United States Army Corps of Engineers for estimating quantity and quality of surface runoff. There are several versions of STORM. In this report, the January 1975 version is used. STORM has the following two computational steps which are subsequently used by the CLAD model.

A. Surface runoff quantities: The runoff contributions from urban and nonurban areas are computed by the following equation:

$$R_s = C_u(P - ADS_u) + C_n(P - ADS_n) \quad (11)$$

where

$R_s$  = surface runoff (to be estimated)

$C_u$  = urban runoff coefficient

This coefficient is estimated by taking the weighted average of pervious and impervious runoff coefficients for each of the five land uses (single family, multiple family, commercial, industrial and open space) with their respective percentages of urban area and imperviousness.



HISTORICAL

FUTURE

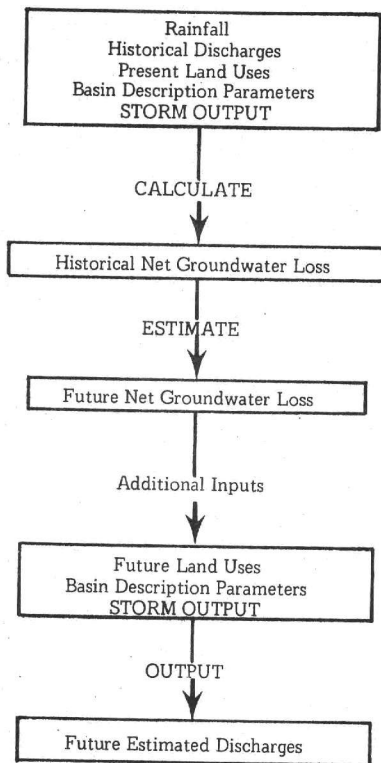


FIGURE 5

A Flowchart of the Discharge Model

- P = Hourly rainfall
- ADS<sub>u</sub> = Available urban depression storage. This is a function of depression storage and evaporation rate which are input parameters.
- ADS<sub>n</sub> = Available nonurban depression storage

B. Storage Runoff Quality: The pollutant runoff form of the equation is

$$\text{Washoff} = P_o(1 - e^{-KR_s}) \quad (12)$$

where

- Washoff = Pollutant washed off by the rainfall in pounds,
- P<sub>o</sub> = Initial pounds of pollutant on the basin
- K = Washoff coefficient (an input value)
- R<sub>s</sub> = Surface runoff (computed from Step 1)

The five pollutants considered in the January 1975 version of STORM for both urban and nonurban land uses are suspended solids, settleable solids, biochemical oxygen demand (BOD), nitrogen and phosphorus. The solids and nonurban loadings are independently calculated, however, the urban BOD, N and P washoffs are dependent on urban solids washoffs. This dependence can be annuled by inputting very small accumulation rates for urban solids (not zero since STORM has default values)

Street sweeping and its efficiency in reducing the amount of pollutants accumulated is an additional option available in these surface runoff quality computations.

### 2.3 QUALITY COMPUTATIONS

The following steps are involved in the water quality analysis.

- 1) Using at least one year of monthly water quality data coupled with monthly discharge data, monthly nonpoint loadings from the basin are computed. Any point source contributions during the data collection period must be deducted.

The term "data collection period" is also referred to as "data base period" in this report. The nonpoint loadings computed in this step are also known as historical loadings which include surface runoff loadings and loadings from other nonpoint sources and sinks. These calculations are done before CLAD model is run.

2) Estimate the surface runoff loading by using STORM for the data base period. To do this, first run STORM and STORM SUM (a program in CLAD model to sum up surface runoff on monthly basis), and second calibrate STORM output to the data above by trends (loadings and/or concentrations versus time) and the maximum limits (discharge loadings).

3) Knowing the total historical loadings and quantities from Step 1 and calculating the surface runoff loadings and quantities from Step 2, the quantities and loadings of other nonpoint sources are obtained by subtraction. Other nonpoint sources and sinks concentrations can then be calculated. An iterative procedure is employed by the user to find the best data fit with output from Steps 1 and 2.

4) Using the computed other nonpoint source concentrations and projected land uses, the CLAD model provides quantity and quality (loading and concentrations) for future scenarios.

The parameters most effective in quality calibrations are the exponents for dust and dirt washoffs and the pollutant accumulation rates. Runoff coefficients and depression storage also affect quality outputs, but they affect quantity much more.

The CLAD model is also designed to reduce future urban loadings by expected pollutant removal efficiencies. These removal efficiencies are model inputs for the entire urban area. They were calculated for grassed swale drainage and detention basins as follows:

$$REFF = [(EFFGS)(FRACGS) + [1-(EFFGS)(FRACGS)](EFFDB)(FRACDB)](NDUA/TFUA) \quad (13)$$

where

- REFF = Removal efficiency for future urban areas
- EFFGS = Removal efficiency for grassed swales,
- FRACGS = Fraction of area in newly developed urban areas to have grass swales,
- EFFDB = Removal efficiency of detention basins,
- FRACDB = Fraction of area in newly developed urban areas to have detention basins,
- NDUA = Newly developed urban area,
- TFUA = Total future urban area.

#### 2.4 CLAD MODEL OUTPUT

The CLAD model with its preceding three components produces the following output which has 11 output sections:

- (1) List of input, an echo print excluding rainfall.
- (2-4) STORM quality output for three land uses: present, future, and future urban. These outputs are identical to the STORM quality printout. They give, for each event (an event occurs when there is sufficient rainfall to cause surface runoff), rainfall, runoff, and pollutant washoffs in pounds.
- (5-7) STORM SUM, monthly runoff quality summary from STORM plus depression storage evapotranspiration for the three land uses.
- (8) Surface runoff concentrations for the three land uses.
- (9) Other nonpoint sources and sinks quantities and loadings.
- (10) Quantity output; listing monthly rainfalls and for present and future land uses: basin discharges, runoffs, depression storage evapotranspirations, surface water evapotranspirations, and net groundwater losses.

(11) Future basin discharged quality: monthly loadings and concentrations.

## 2.5 LIMITATIONS OF THE MODEL

The water balance is a gross estimation of how historical discharges change with future land uses. The CLAD model cannot be considered accurate for short term events (less than monthly for either quantity or quality). Therefore, neither flood analyses nor peak pollutant concentrations or loadings can be obtained through the use of the CLAD model. Appropriate use of the model is for long term or accumulative water quantity and quality effects on basin discharges for projected land uses. Such applications are, for example, regional water supply routings, seasonal storage analyses, and gross quantity and loading evaluations on downstream receiving waters.

There is a general lack of definition and knowledge concerning other non-point groundwater sources and sinks, and their variations. These monthly concentrations have been assumed constant from year to year. During high rainfall other nonpoint source concentrations would probably be lower. For low rainfall years, other nonpoint source concentrations would probably be higher, but the sinks may balance out the discharged loadings.

Future discharge predictions were made by assuming the net groundwater losses in a basin would decrease in proportion to the increase in impervious ground cover. This was assumed for simplicity, and because of the general lack of knowledge and complexities in predicting future groundwater mass balances. The assumption is most valid for small increases in impervious areas, non zero net groundwater losses, and when the net groundwater losses are dominated by groundwater evapotranspiration.

Increases in water demand must be considered separately. These discharge predictions don't include increased demands, or their effects on the groundwater system.

Quality predictions presently lack well defined, area sensitive, land use pollutant accumulation rates. However, they are initiated with Florida data (Nonpoint Source Effects, Wanielista), and then they are calibrated by limits and trends, as previously explained.

Presently this model doesn't include any mixing calculations. That is the water quality of surface runoff plus that of other nonpoint sources and sinks is equivalent to the discharged water quality, they are not mixed with the water stored in the conveyances. This causes little or no problems during the wet season, but it can cause high pollutant concentration predictions during the dry season. When surface runoff exceeds discharge, the pollutant loadings into the canal will probably exceed the discharged loadings. In these cases the discharged quality is set equal to the surface runoff quality. In reality, during these periods the surface runoff is diluted by stored surface water, and some uptakes are likely. Mixing effects should be added to this model to adjust the high pollutant concentration predictions during the dry season, and to add temporal cohesion to the model.

The model is applied to canal drained basins. Canals are deep, narrow water conveyances, with little or no littoral areas. Canals are not conducive to biological activity. It is therefore easier to model canal discharged loadings because of their deficiency in natural pollutant sinks. For a natural watercourse, uptakes will become much more significant. This may require additional calibrations or program modifications in terms of ET changes, demand supplied, quality and mixing processes.

### 3. INPUT REQUIREMENTS

#### 3.1 INPUT DATA

There are the following types of input data pertaining to (A) discharges (B) quality related concentrations (C) rainfall and (D) input information to STORM

DATA BASE

Water Quality Data, Monthly for One Year  
Basin Discharges  
Point Source Contributions

CALCULATE

Basin Discharged Nonpoint Pollutant Loadings

INPUTS

CALIBRATION

Hourly Rainfall  
Basin Description Parameters  
Land Uses  
STORM Output

CALCULATE

Other Nonpoint Sources and Sinks Loadings and  
Concentrations (best data fit)

ADDITIONAL INPUTS

QUALITY PREDICTIONS

Future Land Uses  
Basin Description Parameters  
Expected Abatement Efficiencies  
Discharge Model Output  
STORM Output

CALCULATE

Basin Discharged Nonpoint Source Loadings  
and Concentrations

FIGURE 6

VARIOUS STEPS OF THE QUALITY CALCULATIONS

for present, future and future urban land uses.

(A) Input Set Related to Discharges:

<u>Variable</u>	<u>NO. Cards</u>	<u>Card</u>	<u>Card Columns</u>	<u>Descriptions</u>
SWETH	2	1	1-7	Basin identification, must be identical to all other Basin ID's
			11-20, ..., 71-80 (fields of ten)	Surface water ET for Jan. thru July, in Ac. Ft. assumed repetitive each year.
		2	1-7	Basin ID
			11-20, ..., 51-60	Surface water ET for Aug. through Dec.
		71-75	Card ID "SWETH"	
SWETF	2	Both		Same as SWETH for future
IFI	1	1	3-6	Increased fraction impervious, (see Equation No. (8))
			71-3	Card ID "IFI"
DISH	2 per yr.	1	1-7	Basin ID
			9-10	Year
		2	11-20, ..., 71-80	Historical basin discharges for Jan. through July, Ac-Ft.
			1-7	Basin ID
		9-10	Year	
		11-20, ..., 51-60	Historical basin discharges for Aug. through Dec.	
		71-4	Card ID "DISH"	
(B) Quality Inputs:				
(2) Quality	2			
ONPSCSS	2	1	1-7	Basin ID
			11-20, ..., 71-80	Other nonpoint sources and sinks suspended solids concentrations for Jan. through July, mg/l
		2	1-7	Basin ID
			11-20, ..., 71-77	as above for August through December Card ID "ONPSCSS"
ONPSCBOD	2			Same as above but for BOD
ONPSCTN	2			" " " " " " Total Nitrogen
ONPSCPT	2			" " " " " " Total Phosphorus
REFF	1	1	1-7	Basin ID
			11-20, ..., 71-4	Future abatement efficiencies for total urban area. See equation (13), in order: SS, BOD, TN, TP: Input Fraction (0.50 not 50%) Card ID "REFF"



- (C) Rainfall: The format is the same as STORM with the exception that the C2 card is omitted. Card or tape files may be used.
- (D) Input to STORM: The format of input sets to STORM is given in details in reference No. 12. The CLAD model has restricted certain fields which are given below:
- 1) Omit rainfall data which is already included in section (C) above
  - 2) On B1 card, field 1 must be 1 because CLADM is presently limited to one watershed per analysis.
  - 3) On B1 card, field 2 must be 0 if a rainfall tape is used. The file reserved for snowmelt computations (Tape 11) is used for rainfall tape inputs. If both snowmelt computations and a rainfall tape are desired, another tape I/O unit must be reserved.
  - 4) On C1 card, field 9 must be 1.
  - 5) C2 card is omitted.
  - 6) On E1 card, field 0, basin identification. This must be the same in columns 4-10 as in columns 1-7 of discharge and quality inputs. This is a check for data continuity.
  - 7) Land uses must be put in order: present, future, and future urban. Future urban land use is identical to future, but input 0.0 on H1 card, field 1.

The calibration run is made with three land uses: present, present, and present urban. The abatement removal efficiencies and increased fraction impervious are set equal to zero.

### 3.2 INPUT DERIVATIONS

#### A. Pollutant Accumulation Rates for Surface Runoff

The land use loading rates (pollutant accumulations on land surfaces in lbs/acre/day) used in the backpumping studies are values published by Wanielista, et al, of Florida Technological University (FTU) modified to reflect five urban land uses. These loadings were used in STORM to estimate pollutant (SS, BOD<sub>5</sub>, Total N, and Total P) loadings into primary drainage canals. The FTU loadings are published for both urban and nonurban land uses. The nonurban land uses are divided into cultivated, pasture, and woodland. The urban loadings were not subdivided by land uses as depicted in Table 1.

To more closely reflect urban land use loadings, the average urban loadings were subdivided into the following land uses: (1) single family, (2) multiple family, (3) commercial, (4) industrial, and (5) open space as shown in Table 2. Values in Table 2 are computed by weighing the land use loadings according to

TABLE 1  
FTU Land Use Loading Rates\*  
(lbs/acre/day)

	BOD <sub>5</sub>	Total Nitrogen	Total Phosphorus	Suspended Solids
Urban-Range** Average	0.130-0.200 0.183	0.00782-0.0440 0.0208	0.00244-0.0122 0.00489	1.780-11.720 4.156
Pasture-Range Average	0.0147-0.0416 0.0269	0.00611-0.0208 0.0130	0.000587-0.00161 0.000733	only one value 2.054 *
Cultivated-Range Average	0.00978-0.0758 0.0440	0.0367-0.0905 0.0636	0.000440-0.00396 0.00257	only one value 10.268
Woodland-Range Average	0.00978-0.0171 0.0122	0.00587-0.0125 0.00758	0.0000244-0.00210 0.000244	0.110-0.323 0.240

\* References used were: Burton (1975), Angino (1972), Weibel (1964), Weibel (1966), Weibel (1969), Weidner (1969), Colston (1974), Shannon (1972), Kluesener (1974), EPA (1973), Harriss (1974), Sherwood (1975), and Lamonds (1974).

\*\* Range is the limits of average loadings over a complete discharge hydrograph.

TABLE 2  
Urban Land Use Loading Rates\*  
(lbs/acre/day)

	BOD <sub>5</sub>	Total Nitrogen	Total Phosphorus	Suspended Solids
Single - Range**	0.0317-0.0487	0.00211-0.0119	0.000584-0.00292	0.424-2.795
Family Average	0.0446	0.00562	0.00117	0.991
Multiple-Range	0.0753-0.116	0.00880-0.0495	0.00191-0.00956	1.005-6.619
Family Average	0.106	0.0234	0.00383	2.347
Commercial-Range	0.318-0.490	0.0117-0.0660	0.00534-0.0267	4.240-27.915
Average	0.448	0.0312	0.0107	9.899
Industrial-Range	0.125-0.192	0.0186-0.105	0.00343-0.0172	2.526-16.632
Average	0.176	0.0495	0.00689	5.898
Open - Range	0.00978-0.0171	0.00587-0.0125	0.0000244-0.00210	0.110-0.323
Space Average	0.0122	0.00758	0.000244	0.240

\* Calculated as explained in text

\*\* Calculated from ranges in table 1

the ratios of the loadings as recommended in STORM and by area weighting with average land uses. The open space loadings were equated to woodland loadings. To understand this conversion, an example is discussed below:

First, the pollutant accumulation rates in STORM were converted to lbs/acre/day. This was done by using STORM's default values and assuming curb lengths per acre for each land use as given in Table 3. Next, these values are multiplied together to obtain the desired results as shown in Table 4. For example, commercial nitrogen loading in lbs/acre/day =  $(3.3/100) * (0.041/100) * 83 = 0.001123$ . The third step is to assume an urban land use distribution. Open space loadings were assumed equivalent to woodland, and the assumed other land uses were 33.75 percent for single family, 33.75 percent for multiple family 27.8 percent for commercial, and 4.7 percent for industrial in Florida. Finally, the one urban accumulation rate in Table 1 was subdivided into the other land uses by the fraction of the land uses contribution to the total urban contributions:

$$\text{Accumulation rate} = \left( \frac{\text{Accumulation rate for land use } i}{\Sigma \text{ Urban Accumulation}} \right)_{\text{STORM}} * (\text{Accumulation of FTU})$$

where  $\Sigma(\text{Urban Accumulation Rate of STORM}) = \Sigma(\text{Accumulation } i * \text{Fraction of land use } i)$ . For example, suspended solids accumulation rate for single family in STORM is 0.0466 from Table 4, the FTU urban accumulation rate is 4.156 from Table 1 and

$$\begin{aligned} \Sigma(\text{Urban Accumulation})_{\text{STORM}} &= 0.0466 * 0.3375 + 0.1104 * 0.03375 \\ &+ 0.04656 * 0.2780 + 0.2774 * 0.047 \\ &= 0.19547 \end{aligned}$$

$$\begin{aligned} \text{and Accumulation for S.S.} &= \left( \frac{0.0466}{0.19547} \right) * 4.156 \\ &= 0.991 \text{ lbs/acre/day} \end{aligned}$$

Suspended solids accumulation rates for multiple family, commercial and

TABLE 3

## Conversion of STORM loadings into lbs/acre/day

Land Use	Dust and Dirt* Accumulation (lbs/day/100 ft. gutter)	Pounds of Pollutant/100 lbs. of Dust and Dirt				Curb length** (ft/acre)
		SS	BOD	N	PO <sub>4</sub>	
Single Family	0.7	11.1	0.50	0.048	0.005	60.0
Multiple Family	2.3	8.0	0.36	0.061	0.005	60.0
Commercial	3.3	17.0	0.77	0.041	0.007	83.0
Industrial	4.6	6.7	0.30	0.043	0.003	90.0
Open or Park	1.5	11.1	0.50	0.048	0.005	30.0

\* STORM default values

\*\* Assumed average values

TABLE 4  
 STORM Pollutant Accumulation Rates\*  
 (lbs/acre/day)

Land Use	SS	BOD	N	PO <sub>4</sub>
Single Family	0.0466	0.00210	0.000202	0.000004
Multiple Family	0.1104	0.00497	0.000842	0.000021
Commercial	0.4656	0.02109	0.001123	0.000012
Industrial	0.2774	0.00828	0.001780	0.000005
Open or Park	0.0500	0.00225	0.000216	0.000009

\* FOR CALCULATION PURPOSES ONLY, NOT INTENDED AS MODEL INPUTS. Note these BOD, N and PO<sub>4</sub> loadings are dependent on solids loadings.

industrial land uses are 2.347, 9.899, and 5.898 respectively (see Table 2).

The Crops of Engineers has recommended loading rates in the July 1976 STORM users manual, these values are compiled in Table 5.

#### B. Removal Efficiencies in Surface Runoff

A limited, in-house, literature search was done to investigate pollutant removal efficiencies in detention basins, grass swales, and through soil filtration. This brief search was done in conjunction with the proposed backpumping alternatives considered in the CLAD model to simulate required pollution abatement measures on future developments.

Removal efficiencies applicable to stormwater runoff detention ponds are shown in Table 6. The requirement to retain the first one inch of runoff will allow sufficient time for biological stabilization. A 40% removal efficiency for both nitrogen and phosphorus is selected from the data. From Weibel, et al., nitrogen removals may be even greater.

The efficiencies of grass and grass-soil filters for the water quality treatment of urban runoff was examined by Popkin. The treatment system consisted of a grass-covered filter of native calcareous loam. Both warm and cool season conditions were studied. The following are maximum measured treatment efficiencies in percent, for the grass and grass-soil filters respectively: chemical oxygen demand: 19 and 88; suspended solids; 34 and 99.6; volatile suspended solids; 26 and 97; turbidity: 97 and 98; total coliforms: 84 and 98; fecal coliforms: 50 and 98. Grass maturity and soil compaction improve pollutant removals. Popkin also reviewed literature on grass and soil filtration. Hydraulic loadings or loading capacities and average infiltration rates are established. From this study the author concludes that chlorination of the filtration treated runoff is necessary.

Table 5

Pollutant Accumulation Rates from  
July 1976 STORM  
(lbs/acre/day)

<u>Land Use</u>	<u>SUS</u>	<u>SET</u>	<u>BOD</u>	<u>NIT*</u>	<u>PO<sub>4</sub></u>	<u>COLI**</u>
Low Density Res. 2-5 DU/AC	.12	.09	.04	.007	.0042	1.200
Med. Density Res. 5-10 DU/AC	.45	.18	.07	.028	.0063	1.260
High Density Res. >10 DU/AC	3.16	1.00	.13	.025	.0200	9.800
Commercial			.46	.212	.0400	9.000
Industrial			.39	.209	.0300	10.000
Open Space and Rural	Average values not available. Consult local water quality specialists.		.02	.007	.0020	1.000
Pastures			3.10	.392	.3500	120.000
Farming			.02	.044	.0002	.500
Forests (Douglas Fir)			.01	.002	.000024	.001

\* organic nitrogen + NH<sub>3</sub> + NO<sub>3</sub>

\*\* 10<sup>9</sup> MPN/acre/day

Note: These coefficients may not be representative of a given study area and should be adjusted based on site-specific data.



Table 6  
Detention Removal Efficiencies (Percent)

	COD	BOD <sub>5</sub>	SS	VSS	Tot-N	NH <sub>3</sub>	NO <sub>2</sub>	NO <sub>3</sub>	TKN	Org-N	Tot-P	Sol-P	Reference
Drain Sedimentation		20	60		15					15			Johnson
Sedimentation & Stabilization		95	95		40					40			
Detention Storage		20											Burke
Detention time													
1 hr.		20	40							35			
2 hrs.		25	60							40			
3 hrs.		25	65							40			
4 hrs.		30	70							40			
5 hrs.		30	70							40			
Settling Characteristics													Weibel, et. al.
Settling time													
10 min.	13	40	39	34	9	0	0	0	0	14	4	0	
20 min.	13	44	46	45	14	0	0	0	0	21	13	0	
1 hr.	18	20	57	50	28	0	0	0	0	43	13	0	
4 hrs.	34	20	71	60	56	0	0	0	0	86	34	0	
24 hrs.	47	48	87	84	56	0	0	0	0	86	39	0	
Sedimentation													Morris, et. al.
Detention time													
15 min.	16,61	17	37,77						15		7		
13-19		13	33-38	24-37					20		13		
30 min.	10	12	38						20,37		43	13,15	
1 hr.	18,30	11,20	51,57										
2 hr.	33												
4 hrs.													
5 hrs.	33,35	31	50,75	62	15						40	30	
Design Storm = 2 yr., 1 hr.		35	60								43	35	
											35	35	
Sedimentation % in Sediment													Gill, et.al.
Site 1					32								63
Site 2					23								66
Site 3					17								31
Storage Basin	91			28	62								Lager & Smith

Myers has done a field study on nutrient (nitrate and phosphate) removal using grass filtration. The parameters studied include: application rate, flow distance, application frequency, and season of the year. Nutrient removals were low ranging from 0-20%. Field and lab tests indicated that contact time was the most important variable. Removal efficiencies increased with increasing flow distance, reduced application rates, and reduced application frequencies. With a soil-grass system, lab tests showed a 90% reduction in nitrate. The authors recommend the incorporation of an impervious layer. Other considerations were: ground cover, temperature, and initial concentrations.

The removal efficiencies that are considered in the CLAD model are related to surface runoff only. The reductions in loadings due to infiltration are accounted for in runoff coefficients for the drainage system. The range of nutrient removal efficiency used in the CLAD model for predicting the future loading from developments with abatement measures is 40-52% assuming 40% reduction in detention basins and 0-20% reductions in grass swales.

#### C. Runoff Coefficients and Depression Storages for STORM

The runoff coefficients used in STORM for Palm Beach and Broward Counties are as follows: 0.90 for urban impervious areas with direct drainage systems connecting these impervious areas to the drainage canals; 0.40 or 0.45 for urban impervious with grassed swale drainage, 0.20 for urban pervious areas, and 0.23 for nonurban areas. In STORM, only one urban impervious runoff coefficient can be input. This coefficient is an area weighted average. The urban pervious runoff coefficient is lower than the nonurban coefficient because there is a potential for runoff to drain under impervious areas thus reducing its runoff. In Dade County the assumed runoff coefficients are 0.90 for urban direct drainage impervious, 0.40 for urban grassed swale drainage,

and 0.10 for both urban pervious and nonurban.

Depression storages are also necessary for runoff calculations in STORM. The assumed depression storages are: 0.10" for urban, 0.30" for forest, 0.20" for pasture, and 0.30" for cultivated. For high intensity (smooth) cultivated areas a value of 0.10" could be used, however, 0.30" was used because of the flat topography of south Florida. There is only one value of nonurban depression storage used in STORM. These values are also area weighted averages according to land uses.

It is to be noted that all of these values are preliminary estimates, and are subject to revision as more site specific data becomes available.

#### D. Land Use Aggregation

The mathematical model STORM requires land use pollutant accumulation rates as an input to generate the quality of surface runoff. These land uses are divided into a nonurban classification and five urban groups (1) single family, (2) multiple family, (3) commercial, (4) industrial, and (5) open or park. The nonurban classification is divided external to the program into three land use categories: (1) pasture, (2) cultivated, and (3) woodland. The pollutant accumulation rates for these land uses are area weighted averages for the one nonurban land use classification.

The "Land Use Coding System" (South Florida Water Management District) is divided into three levels: I, II, and III, each with increasing land use clarification. The interface of this system with the STORM model is given in Table 7. The basin model inputs and outputs are listed in figure 7.

## 4. APPLICATIONS

### 4.1 Western West Palm Beach Canal (C-51) Plus L-8

Water quantity and quality predictions are made for the West Palm Beach Canal basin with backpumping. This backpumping alternative includes both

TABLE 7

Aggregation of SFWMD's Land Use Coding System  
into STORM Land Uses

Level I	Level II	Level III	STORM
Urban & Built Up Land	Residential	Single Family Low density Medium density Mobile home	Single Family
		Sing.Fam-High density Multiple Family	Multiple Family
	Commercial & Services Open & Other	*  Golf Course	Commercial
	Industrial Institutional Transportation	* * *	Industrial
	Open & Other (less golf course and underdevelopment)	*	Open Space
Wetlands	*	*	Woodland**
Barren Land	*		
Forest Land	*	*	
Rangeland	*		
Water	*		
Agriculture	Cropland Orchards etc. Confined Feeding Operations	* *	Cultivated** Non-Urban
	Pasture	*	Pasture**

\* Expanded Classification Omitted, for further breakdown the reader is referred to the South Florida Water Management District's Land Use Coding System.

\*\* Subgroup, area weighted for nonurban land use

INPUTS

Present Land Use Analysis  
Future Land Use Projections  
Hourly Rainfall  
Historical Discharges  
Expected Abatement Measures and Efficiencies  
General Basin Description Parameters  
Data Base - Monthly Water Quality for one year  
Point Source Contributions

MODELS

Basin Nonpoint Model Comprised of:  
a) STORM  
b) Discharge Model  
c) Quality Model

OUTPUTS

Estimated Future Discharges  
Basin Discharged Loadings  
Basin Discharged Concentrations

FIGURE 7

THE MODEL INPUTS AND OUTPUTS

the west C-51 and L-8 basins. The west C-51 analysis makes use of the CLAD model. The requirement to subtract M-Canal demands from L-8 discharges necessitated a separate analysis for this basin. The results for both basins, for two land uses (1973-74 and plan scenario), are included. Model inputs and assumptions are discussed below:

#### 4.1.1 Discussion

This discussion is divided into three sections:

1) The west C-51 basin analysis, 2) the L-8 basin analysis and 3) the total backpumped basin.

##### (1) West C-51 basin

In conjunction with the backpumping studies, the west C-51 basin (Figure 1) discharges and nutrient water quality are estimated for two-land uses: 1973-74 and plan scenario. The basin discharge CLAD model is used.

Land uses have been aggregated or expanded for use in the model as shown in Table 8. Future land use projections did not subdivide agricultural usage into pasture and cultivated. This was done after consultation with the Land Resources's staff, by assuming only 60% of the present pasture lands would remain pastures, the remainder is assumed to be cultivated. In Table 8, the obvious omissions of future multiple family, commercial, and industrial land uses are a result of the land use projection source: (i.e., in the Palm Beach County Master Land Use Plan, the scale was too large to include such land uses). Table 8 also gives the area weighted impervious percentages used in the model.

Pollutant accumulation rates (lbs/acre/day) and depression storages (interception plus surface ponding) are correlated to land uses. Depression storages, as in the WPCF Manual of Practice No. 9, are assumed to be 0.1" for urban areas and for nonurban areas: 0.3" for forest, 0.2" for pasture, 0.1" for high intensity (smooth) cultivated, and 0.3" for low intensity cultivated. The area weighted nonurban depression storages were calculated to be 0.294" and 0.162"

Table 8. West C-51 Land Uses

	1973-4 LAND COVER		PLAN SCENARIO	
	Area (Acres)	Percent Imperviousness (Area Weighted)	Area (Acres)	Percent Imperviousness (Area Weighted)
<u>URBAN</u>				
Single Family	3747	21.4	51707	20.0
Multiple Family	28	80.0		
Commercial	239	85.0		
Industrial	22	61.1		
Open Or Park	14338	5.0	811	5.0
Total Urban	18373		52518	
<u>NONURBAN</u>				
Cultivated	12676		13017	
Pasture	7833		4700	
Woodland	35968		4616	
Total Nonurban	56477		22333	
Total Basin	74851		74851	

for 1973-74 and plan scenario land uses, respectively. The pollutant accumulation rates used for the west C-51 basin are listed in Table 9. The nonurban loading rates have also been area weighted. In the calibration run, if these loading rates did not fit, then they would have been adjusted accordingly. However, no such adjustment is necessary to the west C-51 basin.

As mentioned earlier, the January 1975 version of the Corps of Engineers mathematical model called STORM is incorporated into the CLAD model. In this version of STORM, BOD, N, and P urban washoffs are a function of urban solids loadings. These urban solids loadings were omitted because they would have led to erroneous BOD, N, and P washoffs. However, if zero loadings are input then default values are included in calculations. To avoid this situation very small values, such as 0.000001 for solids dust and dirt accumulation rates are added. Nonurban area loadings don't have this solids dependence, and therefore, are used as model inputs.

This version of STORM was set up for curb and gutter drainage. That is, the pollutant accumulation rates are as a function of the footage of gutters per acre. However, loading rates can be forced into lbs/acre/day by simply inputting pseudo curb lengths and pounds of dust and dirt accumulation rates. For example, in STORM, the inputs are:

$$\left( X \frac{\text{ft. gutters}}{\text{acre}} \right) * \left( Y \frac{\text{lbs. dust and dirt}}{100 \text{ ft. gutter/day}} \right) * \left( \frac{\text{lbs. of pollutant}}{100 \text{ lbs of dust and dirt}} \right)$$

$$= XY \frac{\text{lbs. of a pollutant}}{10,000 \text{ acre/day}}$$

Therefore, by using any combination of  $X*Y = 10,000$ , the pollutant accumulation rates in lbs/acre/day can be directly converted to "lbs. of a pollutant/100lms. of dust and dirt". Note, because of the low loading rates and limited input fields, the program was set up to use ten times the lbs/acre/day loadings by inputting  $X*Y$  value of only 1000. The July 1976 version of STORM has the option to use lbs/acre/day accumulation rates; however, it wasn't available at



Table 9. Pollutant Accumulation Rates (lbs/acre/day) for the West C-51 basin.

	<u>BOD<sub>5</sub></u>	<u>Total Nitrogen</u>	<u>Total Phosphorus</u>	<u>Suspended Solids</u>
<u>URBAN</u>				
Single Family	0.0446	0.00562	0.00117	0.0
Multiple Family	0.106	0.0234	0.00383	0.0
Commercial	0.488	0.0312	0.0107	0.0
Industrial	0.176	0.0495	0.00689	0.0
Open Or Park	0.0122	0.00758	0.000244	0.0
<u>NONURBAN</u>				
Pasture	0.0269	0.0130	0.000733	2.054
Cultivated	0.0440	0.0636	0.00257	10.268
Woodland	0.0122	0.00758	0.000244	0.240
<u>NONURBAN AREA WEIGHTED</u>				
1973-74 Land Uses	0.0213	0.0206	0.000825	2.705
Plan Scenario	0.0338	0.0414	0.001703	6.467

the time the CLAD Mode was written.

The exponents used for dust and dirt washoffs are 15.0 and 0.46 for urban and nonurban land uses respectively. These are arrived at by calibrating STORM's output for total nitrogen and total phosphorus. The following combinations of urban and nonurban exponents were tried: 15,4.6; 15,0.46; 15,0.05; 4.6,0.46; 4.6,0.05, and 0.46,0.46.

STORM uses a modified rational method to calculate surface runoff:

$$\text{Surface Runoff} = C * (\text{Rain} - \text{Available Depression Storage})$$

The calculation interval is hourly. For this basin, hourly rainfall at the Loxahatchee recording stations, Florida climatological data was used. In cases where data was missing, West Palm Beach airport precipitation was substituted. This data has been stored on tape at FSU in Tallahassee (location RI1098, number 7782, File 1), and is also available on cards.

The runoff coefficients used in this analysis are: 0.2 for urban pervious areas, 0.9 for urban impervious areas, 0.23 for nonurban areas, and 0.45 for urban impervious areas with grassed swale drainage. For the 1973-74 and plan scenario land uses, the area weighted runoff coefficients are calculated as 0.239 and 0.255 respectively. The urban pervious coefficient of 0.2 is lower than the nonurban coefficient because these areas are thought to drain under the impervious areas, thus reducing their runoff. Many variables are considered in selection of these runoff coefficients, including the low ground slopes, soil transmissivities, indirect routing of rooftop drainage over lawns to storm drainage, secondary drainage under impervious areas, and grassed swale drainage.

Three separate approaches were taken to estimate the maximum urban runoff coefficient for the 1973-74 land uses. First, as shown in Table 10, using WPCF's Manual of Practice No. 9 as a reference the runoff coefficient is calculated as 0.291. This coefficient is applicable for storms of 5-10 year frequency. If less frequent and more intense storms are under consideration,

Table 10. "C" of Q=CIA West C-51 1973-4 Land Uses.

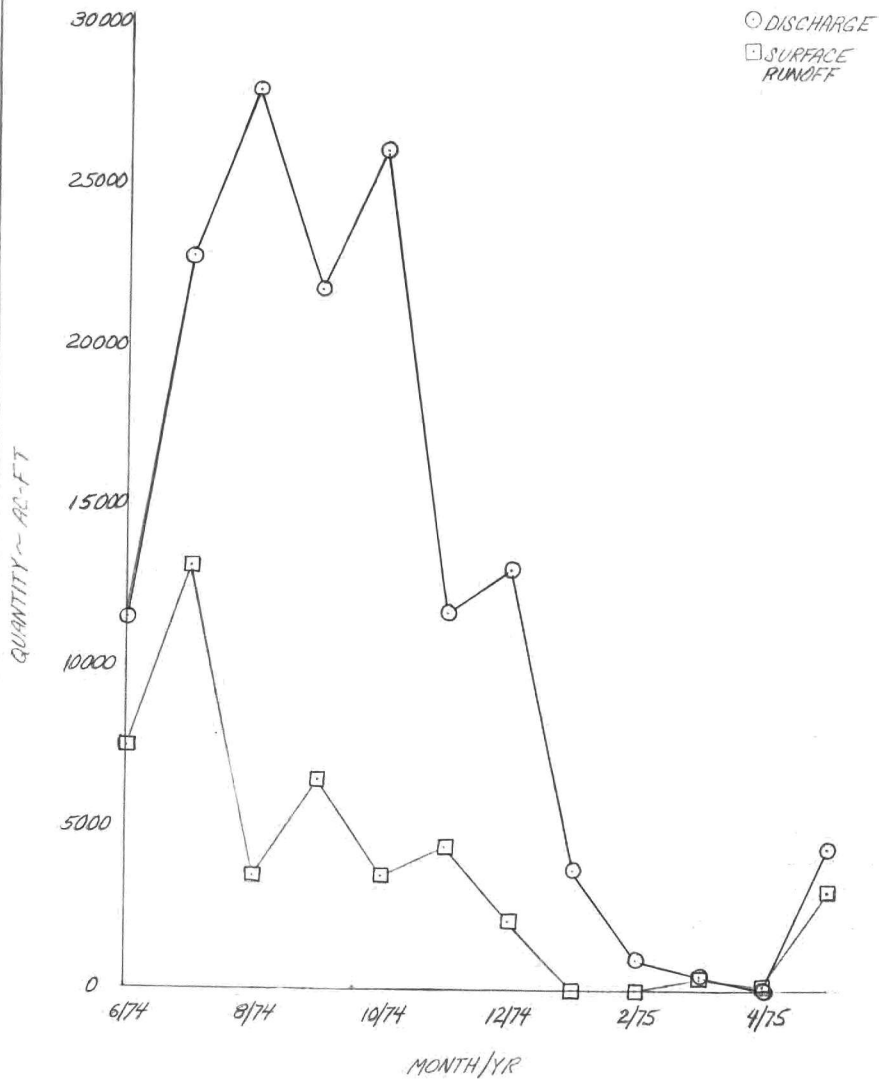
LAND USE (SFWMD)	EQUIVALENT (WPCF)	AREA (Acres)	RUNOFF COEFFICIENT (Average)	C*AREA
Residential				
Low density	Residential Suburban	3591.29	0.375	1405
Med. density	" "	155.33	"	
Multiple family	Multi Detached	28.01	0.50	14
Commercial	Neighborhood Business	239.37	0.60	162
Institutional Gov.	" "	9.36	"	
Industrial	Light Industrial	6.35	0.65	8
Water Supply Plant	" "	5.94	"	
Open & Other				
Golf Course	Park	154.73	0.175	3708
Under Development	Avg. Res. Sub. and Unimproved	14126.72	0.2625	
Open & Undeveloped	Unimproved	56.14	0.20	15
		<u>18373.23</u>		<u>5339</u>
Runoff Coefficient (Area Weighted)				0.291

higher coefficients should be used. Five and ten year storms of 24 hours duration in southeastern Florida are about 3.8 and 9 inches of rainfall, respectively. These are obviously not average events. The 0.291 runoff coefficient should therefore be too high for most rainfall events. This coefficient is used in calculations of peak runoff with the formula  $Q = CIA$ . By using the runoff calculation as in STORM, this runoff is reduced by the initial abstractions to depression storage. Secondly, an attempt to use the SCS curve number technique was made. For the hydrologic soil groups of this basin,  $C_n = 55$ , and a 10 year, 24 hour storm the equivalent runoff coefficient is 0.388. Finally, runoff hydrographs were graphed by SFWMD's hydrology staff. This resulted in runoff coefficients of about 40%. These calculations are all for major events, and therefore serve only to set a limit on the runoff coefficient as input in STORM.

These runoff coefficients could be studied and defined with more accuracy in the future. However, because these coefficients are applied to such a large basin (74851 acres), when considering the data accuracy (rainfall, discharges, etc.), improvements in defining one variable without improving all variables would probably be unjustified. Also since the CLAD model is based on discharges, and surface runoff is only a portion of that amount, these coefficients become less critical to the overall analysis. The resultant proportionment of surface runoff to discharges for the data base period is illustrated in Figure 8.

When estimating future runoff coefficients for urban areas, ninety percent of future developments were assumed to have grassed swales (GS), the remaining ten percent are assumed to have curb and gutter (CG) drainage. The overall urban impervious runoff coefficient is calculated by area weighting. For the west C-51 basin the newly developed urban area (NDUA) is:

FIGURE 8  
WEST C-51 BASIN QUANTITIES FOR THE  
DATA BASE PERIOD



$$\begin{aligned}
\text{NDUA} &= \text{Total future urban area (TFUA)} \\
&- \text{open future urban area} \\
&- [\text{total present urban area (TPUA)} - \text{open} \\
&\quad \text{present urban area}] \\
&= 47672 \text{ acres}
\end{aligned}$$

and the urban impervious coefficient is:

$$\begin{aligned}
\text{CIMP} &= \frac{\text{NDUA}}{\text{TFUA}} * (\text{Fraction GS} * \text{CIMP of GS}) \\
&+ (1 - \text{fraction GS}) * \text{CIMP of CG} \\
&+ ((\text{TFUA} - \text{TPUA}) / \text{TFUA}) * \text{CIMP of present drainage system} \\
&= 0.532
\end{aligned}$$

This analysis assumed that for future nonurban land uses, no abatement measures would be required. Two probable abatement measures have been included as nutrient sinks for future urban developments: (1) grassed swales; 90% of the newly developed urban areas are expected to have this type of drainage, and (2) detention basins; it was assumed that 50% of the newly developed urban areas will be required to have these. The nutrient removal efficiencies used in this analysis are from a limited literature search. These efficiencies are 10% and 40% for both total nitrogen and phosphorus, for grassed swales and detention basins, respectively. These removals for the entire future urban area are calculated to be:

$$\begin{aligned}
\text{REFF} &= \text{EFFGS} * \text{FRACGS} + (1 - \text{EFFGS} * \text{FRACGS}) * \text{EFFDB} * \text{FRACDB} * \text{NDUA} / \text{TFUA} \\
&= 0.247 \text{ or } 24.7\%
\end{aligned}$$

where

$$\begin{aligned}
\text{REFF} &= \text{Removal efficiency for future urban areas} \\
\text{EFFGS} &= \text{Removal efficiency for grassed swales} \\
\text{FRACGS} &= \text{Fraction of area in newly developed urban areas} \\
&\quad \text{to have grassed swales} \\
\text{EFFDB} &= \text{Removal efficiency of detention basins}
\end{aligned}$$

- FRACDB = Fraction of area in newly developed urban areas  
to have detention basins
- NDUA = Newly developed urban area
- TFUA = Total future urban area

This calculation assumes that all areas required to have detention basins will also be required to have grassed swale drainage. It further assumes, for areas with both abatement measures, that after grassed swales remove 10% of the nutrients, 40% of the remaining nutrients (40% of 90%, or 36%) can still be removed in the detention basins. There is obviously a limit to these removals from abatement measures applied in series. A great deal of research in these areas is necessary to establish abatement removal efficiencies.

The uptakes from abatement measures are difficult to define where groundwater components are involved. A total mass balance is necessary to define the system correctly. For example, consider nutrient inflows to a detention basin of 100 lbs via surface runoff at 1.0 mg/l, and 100 lbs. via groundwater flow at 0.5 mg/l. For these, the outflows are 20 lbs. at 0.5 mg/l via overflow, and 50 lbs. at 0.5 mg/l via groundwater. Removal efficiencies of this system could be calculated as: 65% (200 lbs. in, 70 lbs. out), or 80% (100 lbs. in, 20 lbs. out via surface waters). The first calculation is probably the best, while data collection would be much easier for the surface water calculations. There are many unanswered questions in the above, such as: where and how would groundwater measurements be made? What is the sediments role in uptakes and releases? What roles do soils and soil sorption play? and what are the long term removals? In short, abatement removal efficiencies are ill defined and need a lot of future research. This backpumping alternative calls for raising the west C-51 stage from 8.5 to 14.0 ft. The effects of this were investigated by the Groundwater Division of the South Florida Water Management District. Their conclusion was that it should have minimal effects on the water budget. Potential evaporation

data was taken from an unpublished manuscript by the RPD of the SFWMD, "Drought Analysis for the Florida Lower East Coast", see Table 11. In STORM, these are used to evaporate water from depression storage during hours of no rainfall. These values are also used to calculate surface water evapotranspirations. For present land uses, they are simply multiplied by the measured surface water area. For future conditions, the surface water is increased by assuming 10% of the lands required to have detention basins (50% of the newly developed urban areas) would be used for water control.

Historical discharges (1963-75) from the west C-51 basin are calculated from available USGS surface water data. This is done by assuming 65% of the C-51 basin generated discharges are from the west subbasin. This 65% is based on the basins area ratio (west C-51/C-51 area = 64.4%) and three hydrologic calculations completed by the hydrology staff which resulted in percentages around 65%. Flows are calculated because flow measurements at the east boundary of the west C-51 basin are not available. The west C-51 generated discharges are calculated from:

$$Q = 0.65 (WPB - S5AE)$$

where,

WPB = flow discharged at the West Palm Beach locks

S5AE = flow discharged at Structure 5A East

Discharges were calculated on a daily basis and are available from January 1961 through June 1975. These discharges are not allowed to be negative, (i.e., if S5AE discharges exceeded WPB discharges, the flow generated in the C-51 basin is assumed to be zero). Additional basin inflows from S5AE probably introduce some discharge calculation errors. For example, this inflow keeps the groundwater artificially high in the dry season. At the beginning of the wet season, higher discharges probably occur because of this.



Table 11. Potential Evaporation Rates

MONTH	POTENTIAL EVAPORATION	
	(in/month)	(in/day)
January	3.23	0.104
February	1.36	0.048
March	2.41	0.078
April	5.08	0.169
May	5.64	0.182
June	6.39	0.213
July	6.71	0.216
August	6.79	0.219
September	6.01	0.200
October	4.83	0.156
November	3.88	0.129
December	2.54	0.082
Yearly	54.87	

Future discharge calculations are made from historical discharges, surface runoff calculations, depression storage evapotranspirations, and surface water evapotranspirations and are correlated to the increase in impervious cover. This increased fraction of imperviousness is calculated using the following equation:

$$\begin{aligned} \text{IFI} &= \text{increased fraction impervious} \\ &= \Sigma(\text{IF} * \text{Area}_i / \text{Total Area}) \text{ Future} \\ &\quad - \Sigma(\text{IF}_i * \text{Area}_i / \text{Total Area}) \text{ Historical} \\ &= 0.116 \text{ or } 11.6\% \end{aligned}$$

where

$$\text{IF}_i = \text{Impervious fraction for land use } i$$

The quality calculations are based on one year of bimonthly data taken at four locations in the west C-51 basin from 6/74 to 5/75, see Table 12. These sampling sites are located, going from west to east: just east of S5AE, at McArthur Bridge, at Old Wellington Road, and at State Road 7. Monthly nutrient values are obtained by simply averaging all four collection stations. Questions have been raised about what concentrations should be used to represent monthly discharge concentrations. First, simple data calculations for total nitrogen can be different; e.g., if any NO's or TKN's are missing from a sample, one might argue that none of the other values in this sample should be used in the monthly averages. In the approach chosen, all measured values are used. Some other logistical problems also arise from assuming this simple average is representative of discharged monthly concentrations. Alternative approaches are available that address these problems, such as: area weighted average of the measured data, and using the values at SR7 or S5AE. Elaborate statistical and logistical calculations could be made, but because of the measurement frequency and data accuracy, these calculations are not justified.

Table 12. West C-51 Surface Water Quality Data

Date	TKN (mg/l)	No. TKN Samples	NO <sub>3</sub> -N (mg/l)	No. NO <sub>3</sub> Samples	NO <sub>2</sub> -N (mg/l)	No. NO <sub>2</sub> Samples	Total N =TKN+NO <sub>x</sub> (mg/l)	Total P (mg/l)	No. TP Samples
June 74 <sup>1</sup>	3.48	8	0.799	8	0.067	8	4.35	0.065	8
July	1.68	8	0.229	8	0.023	8	1.93	0.131	8
August	1.54	8	0.185	9	0.052	9	1.78	0.077	9
September	1.27	4	0.087	8	0.014	8	1.37	0.068	8
October	1.44	12	0.194	12	0.021	12	1.66	0.113	12
November	0.87	8	0.124	8	0.004	8	1.00	0.133	8
December	1.45	4	1.112	4	0.030	4	2.59	0.108	4
January 75 <sup>1</sup>	0.72	8	0.103	7	0.011	8	0.83	0.176	8
February	1.19	4	0.353	4	0.011	4	1.55	0.049	4
March	1.36	8	0.583	7	0.056	8	2.00	0.113	8
April	1.01	8	0.254	8	0.007	8	1.27	0.050	8
May	1.48	14	0.307	14	0.046	12	1.83	0.050	13

Quality calculations are made with a mass balance approach. Yearly discharged nutrients from the CLAD model are equated to the calculated loadings from the data base. Table 13 and Figures 9 and 10 present the resultant model output with the quality data for the calibration period (6/74-5/75). The total discharged pollutants are equated to the sum of those in surface runoff plus those from other nonpoint sources and sinks. These other nonpoint concentrations are set to match yearly and monthly loadings.

Any point sources must be allowed for external to the program. Future point source contributions are assumed to be zero.

At present there is very little knowledge concerning these other nonpoint sources. Two attempts have been made to gain some knowledge concerning these sources. First, a literature search for groundwater nutrient data was done.

Unfortunately, all nutrient data in this basin, except for one  $\text{NO}_3^-$ -N measurement = 0.34 mg/l at 23 ft. depth, is below 50 ft. Nutrient concentrations to depths of 200 ft. are reviewed for reference. The average total nitrogen -N and total phosphorus -P groundwater concentrations from this literature search are 1.22 and 0.08 mg/l respectively. The second investigative measure was taken to drill three shallow wells adjacent to C-51, collect samples and measure their nutrient concentrations. To date only one set of samples has been collected. The average total nitrogen and total phosphorus concentrations are 1.96 mg/l and 0.068 mg/l. For comparison the average other nonpoint sources and sinks concentrations for the data base period used in this analysis are 2.26 mg/l and 0.117 mg/l for total nitrogen -N and total phosphorus -P, respectively. A concentration summary for the data base period is given in Table 14.

The nutrients in rainfall that fall directly on surface water are also considered. Because of the relatively small areas of surface waters, these contributions are found to be negligible.

Table 13. West C-51 Quantities and Quality Data Base Period

DATE	DISCHARGE (Ac-Ft)	DATA BASE			MODELED			
		Total Nitrogen Loading Conc. (mg/l)	Total Phosphorus Loading Conc. (mg/l)	Total Nitrogen Loading Conc. (mg/l)	Total Phosphorus Loading Conc. (mg/l)	Total Nitrogen Loading Conc. (mg/l)	Total Phosphorus Loading Conc. (mg/l)	
June 74'	11466	135555	2026	0.065	138413	4.44	2187	0.070
July	22746	119310	8098	0.131	123120	1.99	7924	0.128
August	27868	134815	5832	0.077	134474	1.78	5741	0.076
September	21697	80786	4010	0.068	81016	1.37	3959	0.067
October	26051	117529	8000	0.113	117207	1.66	7822	0.110
November	11677	31735	4221	0.133	32100	1.01	4157	0.131
December	13127	92401	3853	0.108	91811	2.57	3766	0.106
January 75'	3695	8335	1767	0.176	8288	0.83	1722	0.172
February	956	4027	127	0.049	4002	1.54	268	0.103
March	450	2446	138	0.113	8179	6.69	579	0.474
April	0	0	0	0.050	0	-	0	-
May	4407	21918	599	0.050	22020	1.84	1024	0.085
Total Avg.	144140	748857	38671	(0.099)	760630	(1.94)	39149	(0.100)

FIGURE 9  
 WEST C-51 BASIN  
 TOTAL NITROGEN LOADINGS FOR THE  
 DATA BASE PERIOD

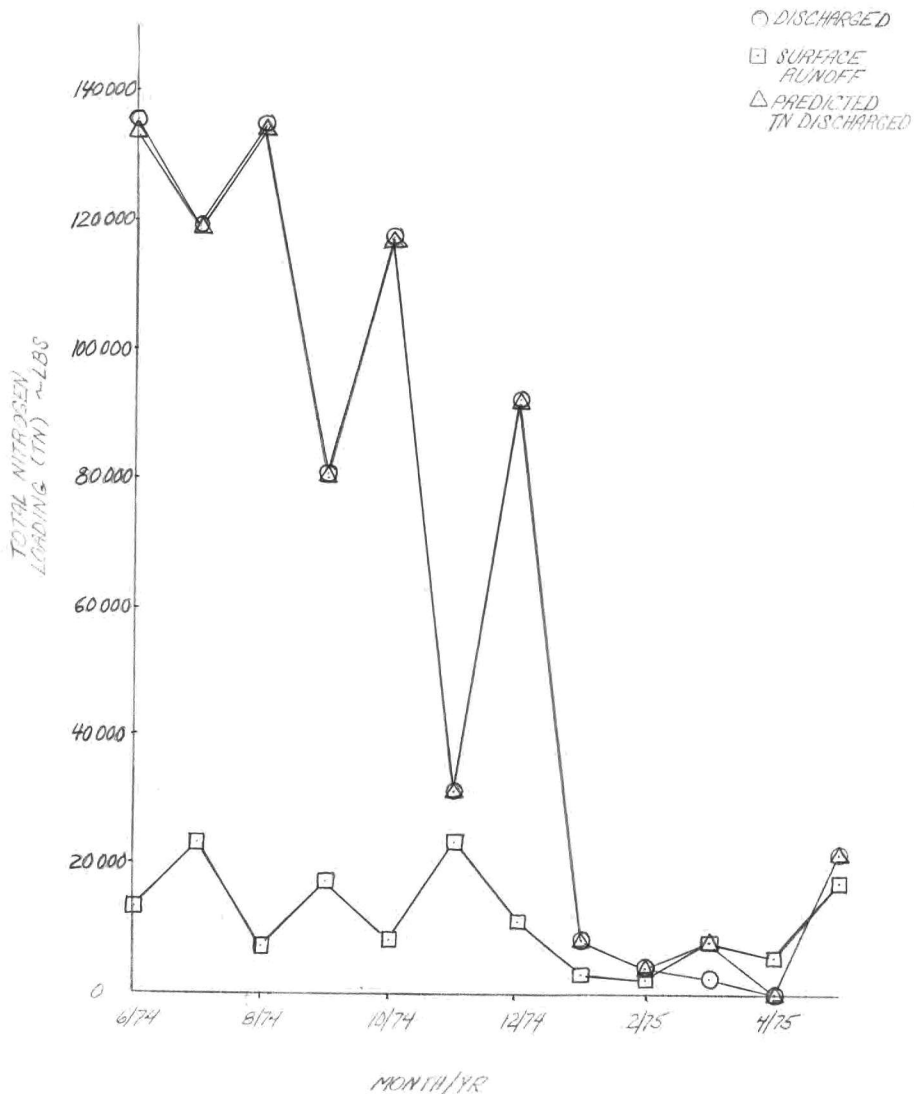


FIGURE 10  
 WEST C-51 BASIN  
 TOTAL PHOSPHORUS LOADINGS FOR THE  
 DATA BASE PERIOD

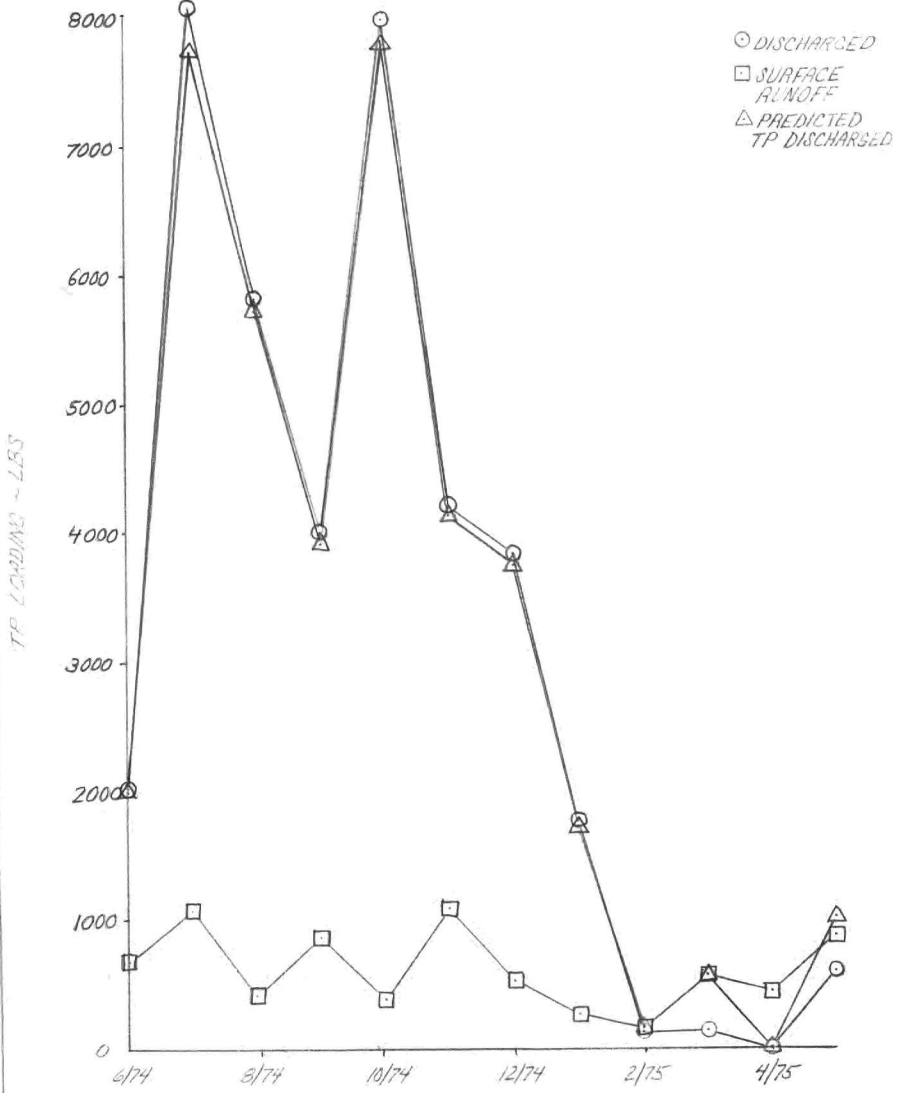


Table 14. West C-51 Nutrient Concentrations Data Base Period Yearly Averages

	Total Nitrogen (mg/l)	Total Phosphorus (mg/l)
Discharged	1.91	0.099
Modeled Discharge	1.94	0.100
Modeled ONPS*	2.26	0.117
STORM	1.27	0.066
Shallow Groundwater		
Literature Search	1.22	0.080
Collected Data	1.96	0.068

\* Other nonpoint sources and sinks



These calculations for the west C-51 future basin discharges include no increased demands. These increases will be considered elsewhere in the back-pumping evaluations.

All west C-51 model inputs and their results are given in Exhibits 7.1 and 7.2 for the 1973-74 and Exhibits 7.3 and 7.4 for plan scenario land uses.

## (2) L-8 Basin

The L-8 Basin analysis assumed that there would be no land use changes within this basin. The results from this analysis are, therefore, used in both the 1973-74 and plan scenario land uses. Quantities available for backpumping are calculated from available USGS surface water data, and from M-Canal demands for the City of West Palm Beach. M-Canal demands are calculated from pumping hours as recorded in "West Palm Beach Water Department Source of Supply Reports" from 1/65 to 5/75. These demands are calculated by assuming a pumping rate of 12 Ac-Ft/hr/pump. By adding L-8 discharges (USGS data) and the calculated M-Canal demands, the total L-8 generated discharges are obtained. However, these discharges are not representative of what can be expected to be available for future backpumping. L-8 discharges must consider M-Canal demands. This was done by assuming any increased demands would be satisfied by Lake Okeechobee. Therefore, M-Canal demands from L-8 were not increased over present demands.

Several attempts were made to define M-Canal demands, including correlations to: the month of year, L-8 discharges, and the following rainfalls; accumulative, for the same month, for the present and preceding months, for the present and two preceding months, for the preceding month, and for the two preceding months. From the above, there were no clear cut correlations, however, it was found that maximum demands could be related to rainfall. The approach finally chosen to calculate quantities of water available from L-8 for backpumping was: for the rainfall record of 1969-74, use L-8 generated

flows less the demands from that period; for the 1963-8 rainfall record, use L-8 generated flows less M-Canal demands as correlated to the rainfall of the two preceding months, see Figure 5. The 1969-74 period had some negative L-8 flows. These were taken to be zero since they obviously weren't generated on the basin. During months of both positive and negative flows only the positive flows were used.

The M-Canal demands in Figure 11 are shown to be 11400 Ac-Ft/month for no rainfall, and linearly reducing to 6,600 Ac-Ft/month for 22 inches of rainfall for the two preceding months. Above this 22 inches, it is assumed that M-Canal demands would be zero. When these demands exceed L-8 basin discharges, the available backpumped quantities are set equal to zero. As previously stated, this simply means these additional demands will be supplied from Lake Okeechobee. This approach may give low available discharges but it is conservative in estimating backpumped quantities. For no reason should these discharges be used for a flood protection analysis. When making flood protection calculations, the safest and most realistic assumption to make is that the M-Canal demands would be zero. These quantity calculations are shown in Exhibit 7.5.

Quality calculations for the L-8 basin were made from data available at the time of computations (12/76). These data and the monthly concentrations used in loading calculations are listed in Table 16. For months when two data points are available, their average is used. When no data is available, the average of all the other data is substituted. The nutrient loadings, as shown in Table 15, are calculated from these concentrations and the aforementioned quantities.

### (3) Total West Palm Beach Backpumped Basin

One area being analyzed for possible backpumping is the west C-51 plus the L-8 basins. This is titled the West Palm Beach Canal Backpumping Alternative. The quantities and quality of water from the total basin are simply

FIGURE II  
HISTORICAL M-CANAL DEMANDS FROM L-8

- △ 1970
- △ 1971
- ◇ 1972
- 1973
- 1974

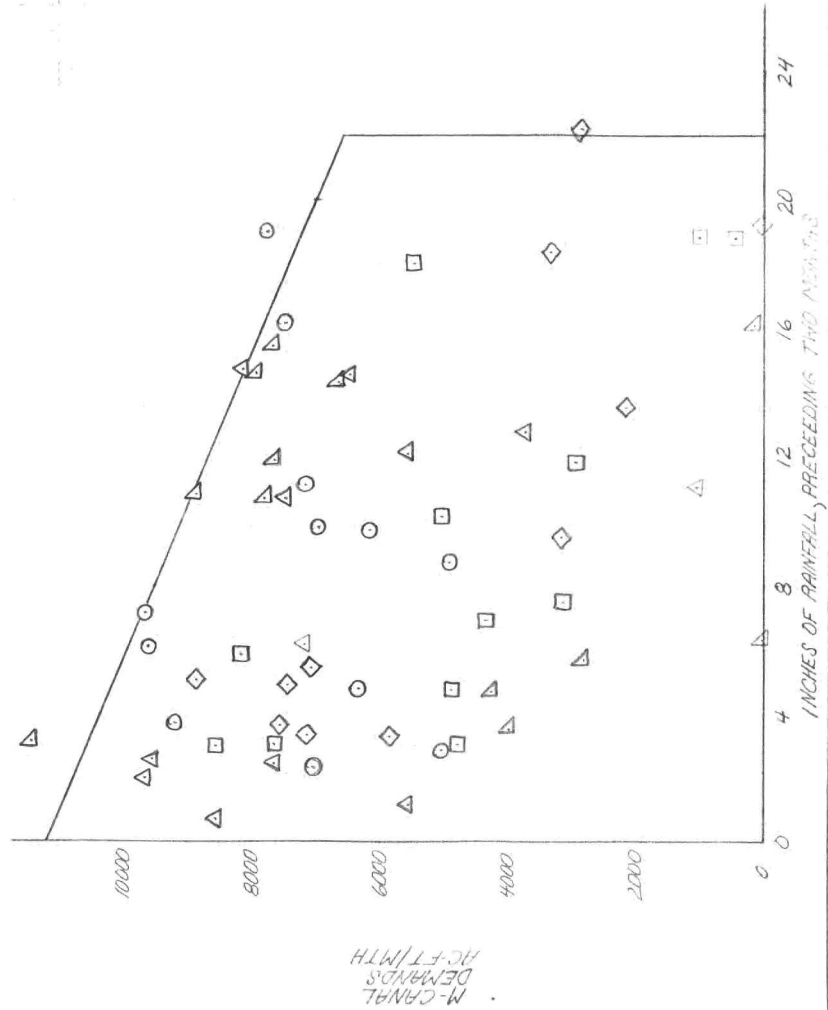


Table 15. L-8 Basin Available Backpumped Quantities and Nutrient Loadings

Date	Historical M-Canal Demands (Ac-Ft)	Historical L-8 Discharges (Ac-Ft)	Historical L-8 Basin Dis. (Ac-Ft)	Future M-Canal Demands (Ac-Ft)	Future Available L-8 Dis. (Ac-Ft)	Total Nitrogen (lbs)	Total Phosphorus (lbs)	
1/63	None	9388	Same	10800	0	0	0	
2		10050	as	10900	0	0	0	
3		12309	L-8	10400	1909	7938	280	
4		11423	Discharges,	10100	1323	5501	194	
5		8918	}	10600	0	0	0	
6		12383		9700	2683	12104	438	
7		7414		8700	0	0	0	
8		7075		9600	0	0	0	
9		6514		9400	0	0	0	
10		9400		8200	1200	4631	114	
11		2291		8900	0	0	0	
12/63		3205		10400	0	0	0	
1/64	None	17821			9400	8421	35016	1236
2		12783			9200	3583	14899	526
3		7646			10050	0	0	0
4		5867			9600	0	0	0
5		6549		9200	0	0	0	
6		9150		9500	0	0	0	
7		8707		9400	0	0	0	
8		17950		8050	9900	45740	2556	
9		19940		8500	11440	44150	1306	
10		23700		8500	15200	58660	1446	
11		22620		8400	14220	59130	2248	
12/64		21836		8600	13236	55038	1943	
1/65	36	17574	17610	10200	7410	30812	1087	
2	48	12165	12213	10700	1513	6291	222	
3	1872	13619	15491	10400	5091	21169	747	
4	1770	5821	7591	10200	0	0	0	
5	5424	4820	10244	10400	0	0	0	
6	8472	8590	17062	10500	6562	29605	1070*	
7	5118	9802	14920	8100	6826	26900	557	
8	2292	11782	14074	0	14074	65025	3634	
9	1938	10802	12720	8200	4520	17440	516	
10	0	30382	30382	9100	21283	82136	2025	
11	12	27582	27594	7100	20482	85168	3006	
12	1926	15656	17582	8200	9382	39012	1377	

Table 15. (Continued)

Date	Historical M-Canal Demands (Ac-Ft)	Historical L-8 Discharges (Ac-Ft)	Historical L-8 Basin Dis. (Ac-Ft)	Future M-Canal Demands (Ac-Ft)	Future Available L-8 Dis. (Ac-Ft)	Total Nitrogen (lbs)	Total Phosphorus (lbs)
1/66	12	19918	19930	10700	9230	38380	1355
2	0	22417	Same	9500	12917	53711	1896
3	0	21031	as	8850	12181	50651	1788
4	0	7613	L-8	9900	2287	9510	336
5	0	10435	Discharges	9700	735	3056	108
6	0	37773	↓	8650	29123	131389	4749
7	0	41427		7000	34627	136457	2823*
8	0	40717		6900	33817	156242	8731
9	0	42982		7500	35402	136625	4041
10	0	26628	↓	6900	9928	38315	944
11	1920	5355	7275	8450	0	0	0
12	0	8795	8795	10300	0	0	0
1/67	1446	8563	10009	10700	0	0	0
2	7776	4903	12679	10100	1979	8229	290
3	6696	6936	13632	10200	3432	14271	504
4	7824	2737	10561	10200	361	1501	53
5	9528	7888	17416	11000	6416	26679	942
6	6966	7367	14333	11200	3133	14135	511
7	1956	13317	15273	8600	6473	25312	523
8	0	12502	12502	0	12502	57762	2088
9	24	7503	7527	8100	0	0	0
10	12	12823	12835	8900	3935	15186	374
11	426	2870	3296	8500	0	0	0
12/67	6606	4735	11341	9900	1441	5992	211
1/68	3834	5820	9654	10600	0	0	0
2	7752	6881	14633	10400	4233	17602	621
3	5520	3423	8943	10400	0	0	0
4	9186	7139	16325	9800	6525	27132	958
5	6840	6450	13290	10300	2990	12433	439
6	0	51447	51447	9100	42583	191049	6905
7	42	48541	48583	0	48583	191455	3961
8	846	14067	14913	0	14913	68901	3850
9	792	10754	11546	8200	3346	12913	382
10	156	33537	33693	9100	24593	94910	2807
11	990	11948	12938	9100	3838	15959	563
12/68	1986	4473	6459	9700	0	0	0*

Table 15. (Continued)

Date	Historical M-Canal Demands (Ac-Ft)	Historical L-8 Discharges (Ac-Ft)	Historical L-8 Basin Dis. (Ac-Ft)	Future M-Canal Demands (Ac-Ft)	Future Available L-8 Dis. (Ac-Ft)	Total Nitrogen (lbs)	Total Phosphorus (lbs)
1/69	5448	2085	Calculation not necessary	Same as Historical Demands	Same as Histor. Discharges	8670	306
2	7194	4514				18770	662
3	3906	20930				87031	3072
4	5412	4993				22180	734
5	1530	5334				20783	783
6	6882	16431				74129	2679
7	4842	6373				25115	520
8	456	10600				48974	2737
9	1740	10223				39453	1167
10	36	41810				161355	3977
11	36	27106				112712	3978
12/69	36	19228				79954	2822
1/70	2808	14509	60331	2129			
2	3978	16467	68473	2417			
3	4236	43916	182611	6445			
4	282	38541	160261	5656			
5	6624	17484	72702	2566			
6	0	30914	139469	5041			
7	7920	20763	81822	1693			
8	7692	25866	119507	6678			
9	8886	31595	121933	3606			
10	7632	16792	64804	1917			
11	7806	607	2524	89			
12	11418	1704	7086	250			
1/71	8556	1042	4331	153			
2	7656	10	42	2			
3	9552	5963	24799	875			
4	5526	3362	13980	493			
5	9654	318	1322	47			
6	7194	250	1128	41			
7	3720	887	3499	72			
8	8124	137	633	35			
9	1044	12264	47329	1440			
10	7488	819	3261	80			
11	5550	4130	17171	606			
12/71	6468	845	3514	124			

Table 15. (Continued)

Date	Historical M-Canal Demands (Ac-Ft)	Historical L-8 Discharges (Ac-Ft)	Historical L-8 Basin Dis. (Ac-Ft)	Future M-Canal Demands (Ac-Ft)	Future Available L-8 Dis. (Ac-Ft)	Total Nitrogen (lbs)	Total Phosphorus (lbs)
1/72		54	Calculation not necessary	Same as Histor. Demands	Same as Histor. L-8 Discharge	225	8
2	7428	238				990	35
3	5894	224				931	33
4	7074	932				3875	137
5	2160	5617				23357	824
6	0	9551				43089	1557
7	2880	6839				26951	558
8	3326	1113				5142	287
9	3168	958				3697	109
10	8772	280				1079	32
11	7554	2				8	0
12/72	7116	58				241	9
1/73	7656	44				181	6
2	4350	0				0	0
3	3114	0				0	0
4	4890	0				0	0
5	8556	0				0	0
6	4794	236				1065	38
7	5034	9578				37745	1425
8	5472	7113				32864	1836
9	1008	7712				29761	880
10	468	5455				21050	519
11	2940	0				0	0
12/73	8160	224				931	33
1/74	6318	1004				4173	147
2	4908	363				1509	53
3	9258	91				379	13
4	7020	0				0	0
5	5088	0				0	0
6	9192	1527				6889	249
7	6972	11903				46907	970
8	7758	10790				49852	2786
9	7494	2123				8191	242
10	7152	5381				20767	512
11	6156	1337				5560	196
12/74	9624	26				108	4

Table 16 L-8 Quality Measured and Averaged Values

Date or Month	Coding	Total Nitrogen-N (mg/l)	Total Phosphorus-P (mg/l)
6/17/76	BCE-122	1.66	0.060
7/15/76	BCE-259	1.53	0.031
7/29/76	BCE-329	1.38	0.029
8/13/76	BCE-409	1.77	0.047
8/26/76	BCE-484	1.63	0.143
9/9/76	BCE-531	1.42	0.050
9/21/76	BCE-595	1.42	0.034
10/6/76	BCE-664	-	0.035
January		1.53	0.054
February		1.53	0.054
March		1.53	0.054
April		1.53	0.054
May		1.53	0.054
June		1.66	0.060
July		1.45	0.030
August		1.70	0.095
September		1.42	0.042
October		1.42	0.035
November		1.53	0.054
December		1.53	0.054



the sum of the two subbasins. Results for the 1973-74 and plan scenario land uses are presented in Exhibits 7.3 and 7.4, respectively. These predictions represent the maximum quantities available for backpumping, with their corresponding loadings and concentrations. The dates are indicative only of a rainfall record, and are not indicative of historical conditions. These exhibits include the results of the west C-51 basin as calibrated in February 1977 plus the previous (12/76) L-8 calculations. These estimates can be updated with additional L-8 quality data.

#### 4.1.2 SUMMARY

- 1) Available discharges for backpumping and the loadings and concentrations for the West Palm Beach canal backpumping alternative (West C-51 plus L-8) are predicted for 1973-74 and plan scenario land uses.
- 2) Historical discharges are calculated from available USGS surface water data. Future discharges are estimated from these discharges for the same rainfall record with changes in land uses.
- 3) All quality predictions are based on the data base period when the quality data were collected (from 6/74 to 5/75 for the West C-51 basin, and from 6/76 to 10/76 for the L-8 basin).
- 4) The CLAD model is used to predict plan scenario water quantities and qualities and 1973-74 land use water quality from the west C-51 basin for the rainfall/discharge record of 1/63 to 12/74.
- 5) Increased future demands from the west C-51 basin are not included in these predictions. They must be considered in subsequent analyses.
- 6) The L-8 basin analysis assumed there would be no land use changes in this basin. These quantity and quality predictions are done by calculating

- L-8 generated discharges, subtracting present M-Canal demands, and using available quality data to calculate loadings and concentrations.
- 7) Any additional M-Canal demands on the L-8 basin are assumed to be supplied by Lake Okeechobee. Present M-Canal demands, as defined herein, are taken from historical discharges to find the quantities of water available for backpumping from this basin.
  - 8) Maximum M-Canal demands are correlated to the sum of the two preceding months of rainfall. No direct correlations to demands are found. The resultant predicted L-8 discharges available for backpumping are, therefore, minimums. This provides a conservative estimate.
  - 9) Under no circumstances should these flows be used in flood protection analyses. This is because of the conservative L-8 discharge calculations, as above, and more importantly because of the monthly time step.
  - 10) These predictions are done with a fairly consistent level of accuracy. To get better predictions a much more detailed analysis to a greatly expanded data base would be necessary.
  - 11) Shallow groundwater quality in the west C-51 basin was investigated. The results are included.
  - 12) The water quality and quantity effects of grassed swales and detention basins are included in this analysis.
  - 13) There is much uncertainty concerning nonpoint sources of pollution.
  - 14) All model inputs, assumptions, and supporting investigations made on this basin are incorporated in this report.

## 4.2 Western Tamiami Canal (C-4) Basin with Snapper Creek

### 4.2.1 Discussion

In conjunction with the backpumping studies, the west Tamiami basin discharges and nutrient water quality are estimated for two land uses: 1973-74 and pattern scenario. The basin discharge CLAD model is used. Figure 6 shows the west C-4 basin boundaries.

Land uses have been aggregated or expanded for use in the model as shown in Table 17. Future land use projections had one nonurban land use: agriculture and open space. This is divided into three land uses: cultivated, open and water. Both cultivated and water are assumed to be the same area as in the 1973-74 land uses, the remainder is assumed open space.

Pollutant accumulation rates (lbs/acre/day) and depression storages (interception plus surface ponding) are correlated to land uses. Depression storages, as in the WPCF manual of Practice No. 9, are assumed to be 0.1" for urban areas and for nonurban areas; 0.3" for forest; 0.2" for pasture; 0.1" for high intensity (smooth) cultivated; and 0.3" for low intensity cultivated. The area weighted nonurban depression storages are calculated to be 0.24" and 0.30" for 1973-74 and pattern scenario land uses, respectively. The pollutant accumulation rates used in this analysis are listed in Table 18. The nonurban loading rates are area weighted averages. All total phosphorus loading rates have been reduced by approximately a factor of 10. The surface runoff calibration of phosphorus showed excessive amounts of phosphorus relative to what was being discharged. This is probably a result of the high soil transmissivities which allows the phosphorus to chemically react with and get absorbed into the soils.

The exponents for dust and dirt washoffs used are 4.6 and 0.46 for urban and nonurban land uses, respectively. These are arrived at by calibrating

Table 17. West Tamiami Land Uses

	1973-4 LAND COVER		PATTERN SCENARIO	
	Area (Acres)	Percent Imperviousness (Area Weighted)	Area (Acres)	Percent Imperviousness (Area Weighted)
<u>URBAN</u>				
Single Family	7717	34.0	18335	35.0
Multiple Family	854	79.6	1022	65.0
Commercial	142	85.0	690	85.0
Industrial	1391	79.6	3457	61.0
Open or park	3739	5.0	1366	5.0
Total Urban	13843		24870	
<u>NONURBAN</u>				
Cultivated	2354		4930	
Pasture	11488		0	
Woodland	12366		10251	
Total Nonurban	26208		15181	
Total Basin	40051		40051	

Table 18. Pollutant Accumulation Rates (lbs/acre/day) for the Tamiami Basin.

	<u>BOD<sub>5</sub></u>	<u>Total Nitrogen</u>	<u>Total Phosphorus</u>	<u>Suspended Solids</u>
<u>URBAN</u>				
Single Family	0.0446	0.00562	0.000125	0.0
Multiple Family	0.106	0.0234	0.000409	0.0
Commercial	0.488	0.0312	0.001137	0.0
Industrial	0.176	0.0495	0.000735	0.0
Open or Park	0.0122	0.00758	0.000026	0.0
<u>NONURBAN</u>				
Pasture	0.0269	0.0130	0.000078	2.054
Cultivated	0.0440	0.0636	0.000274	10.268
Woodland	0.0122	0.00758	0.000026	0.240
<u>NONURBAN AREA WEIGHTED</u>				
1973-74 Land Use	0.0244	0.0168	0.0000774	1.993
Pattern Scenario	0.0218	0.0254	0.0001052	3.483

STORM's output to the trends and limits in the data base for Total Nitrogen and Total Phosphorus. The following combinations of urban and nonurban exponents were tried: 15,4.6; 15,0.46; 15,0.05; 4.6,4.6; 4.6,0.46; 4.16,0.05; 0.46,4.6; 0.46,0.46; 0.46,0.05.

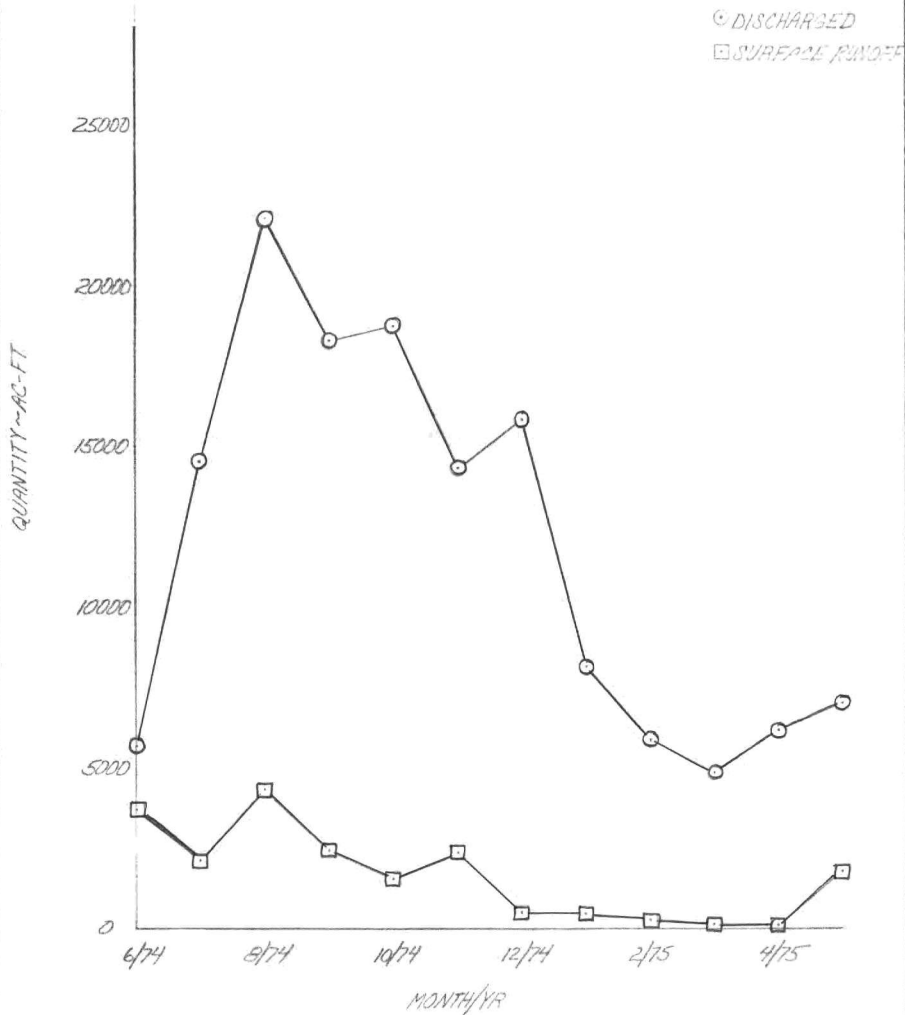
The rainfall data used in this basin's analysis is that of Miami airport. This hourly precipitation data is stored on tape at FSU in Tallahassee (location RI1098, number 7782, file 3), or is available on cards.

The runoff data used in this basin's analysis are 0.10 for urban pervious areas, 0.9 for urban impervious areas, 0.10 for nonurban areas, and 0.40 for urban impervious areas with grassed swale drainage. For the 1973-74 and pattern scenario land uses, the area weighted runoff coefficients are calculated to be 0.181 and 0.245 respectively. The low runoff coefficients are a result of the highly pervious soils. Figure 12 illustrates the resultant proportionment of surface runoff to discharges for the data base period.

When estimating the future urban areas runoff coefficients, ninety percent of future developments are assumed to have grassed swales, the remaining ten percent to have curb and gutter drainage. The area to be developed, calculated from the differences in the pattern scenario and 1973-74 land uses, is 13,400 acres. The resultant impervious runoff coefficient calculated by area weighting is 0.658.

This analysis assumed no abatement measures would be required of nonurban land uses. Two probable abatement measures have been included as nutrient sinks for future urban developments: grassed swales and detention basins. It is assumed that 50% of the newly developed urban areas will be required to have detention basins and 90% will have grassed swales. Removal efficiencies were calculated as before to be 14.7% for Total Nitrogen and Total Phosphorus.

FIGURE 12  
WEST TAMiami BASIN QUANTITIES FOR THE  
DATA BASE PERIOD



Potential evaporation rates are used to calculate future surface water evaporations by assuming detention basins would use 10% of the development's land areas (See Table 11).

Historical discharges (1963-75) from the west Tamiami basin are calculated from available USGS surface water data. This is done simply by adding the discharges as recorded in the Tamiami Canal near Coral Gables (02289500) plus that in the Snapper Creek Canal at Miller Drive (02290610).

Future discharge calculations are made from historical discharges, surface runoff calculations, depression storage evapotranspirations, surface water evapotranspirations and are correlated to the increase in impervious cover. This increased fraction imperviousness is calculated to be 0.145 or 14.5 percent.

Quality calculations are based on one year of bimonthly data from 6/74 to 5/75, see Table 19. Monthly nutrient values are obtained by simply averaging all collection stations. Alternative approaches are possible, but as before, this simple average should suffice.

The quality calculations are made with a mass balance approach. Yearly discharged nutrients from the CLAD model are equated to the calculated loadings from the data base. Table 20 and Figures 13 and 14 present the resultant model outputs with the quality data for the calibration period (6/75-5/75). The total discharged pollutants are equated to the sum of those in surface runoff plus those from other nonpoint sources and sinks. These other nonpoint concentrations are set to match yearly and monthly loadings. These concentrations aren't well understood, they are therefore assumed constant in this analysis.

Any point sources must be included external to the program. Future point source contributions are assumed to be zero.

These future discharge calculations don't include increased demands. These increases are considered elsewhere in the backpumping evaluations.



Table 19. West Tamiami Basin Surface Water Quality Data

Date	TKN (mg/l)	No. TKN Samples	NO <sub>3</sub> -N (mg/l)	No. NO <sub>3</sub> Samples	NO <sub>2</sub> -N (mg/l)	No. NO <sub>2</sub> Samples	Total N = TKN+NO <sub>x</sub> (mg/l)	Total P (mg/l)	No. TP Samples
June 74'	1.11	6	0.091	6	0.008	6	1.21	0.019	6
July	1.84	3	0.039	3	0.010	3	1.89	0.013	3
August	1.79	2	0.097	4	0.011	4	1.90	0.010	4
September	1.29	4	0.080	7	0.020	7	1.39	0.014	7
October	1.62	9	0.141	9	0.011	9	1.77	0.021	9
November	1.39	6	0.499	6	0.013	6	1.90	0.010	6
December	1.10	3	0.121	3	0.007	3	1.23	0.002	3
January 75'	1.31	6	0.194	6	0.020	6	1.52	0.019	6
February	1.19	3	0.371	3	0.032	3	1.59	0.085	3
March	1.08	5	0.183	5	0.020	5	1.28	0.081	5
April	1.27	9	0.065	9	0.006	9	1.34	0.011	9
May	1.50	6	0.073	6	0.009	6	1.58	0.015	6

Table 20. West Tamiami Basin Quantities and Quality Data Base Period

DATE	DISCHARGE (Ac-Ft)	DATA BASE			MODELED				
		Total Nitrogen Loading Conc. (lbs) (mg/l)	Total Phosphorus Loading Conc. (lbs) (mg/l)	Total Nitrogen Loading Conc. (lbs) (mg/l)	Total Phosphorus Loading Conc. (lbs) (mg/l)	Total Nitrogen Loading Conc. (lbs) (mg/l)	Total Phosphorus Loading Conc. (lbs) (mg/l)		
June 74'	5740	18876	1.21	296	0.019	18843	1.21	298	0.019
July	14464	74296	1.89	511	0.013	74255	1.89	510	0.013
August	22120	114223	1.90	782	0.010	114200	1.90	796	0.013
September	18332	69253	1.39	698	0.014	69005	1.39	702	0.014
October	18766	90273	1.77	1071	0.021	89998	1.76	1053	0.021
November	14339	74043	1.90	390	0.010	74096	1.90	380	0.010
December	15840	52951	1.23	86	0.002	52907	1.23	100	0.002
January 75'	8150	33668	1.52	421	0.019	33666	1.52	419	0.019
February	5890	25452	1.59	1361	0.085	25376	1.59	1365	0.085
March	4920	17115	1.28	1083	0.081	17107	1.28	1079	0.081
April	6217	22641	1.34	186	0.011	22621	1.34	184	0.011
May	7060	30316	1.58	288	0.015	30204	1.57	282	0.015
Total (Avg)	141838	623107	(1.62)	7173	(0.019)	622278	(1.61)	7168	(0.019)

FIGURE 13  
 WEST TAMPA MIAMI BASIN  
 TOTAL NITROGEN LOADINGS FOR THE  
 DATA BASE PERIOD

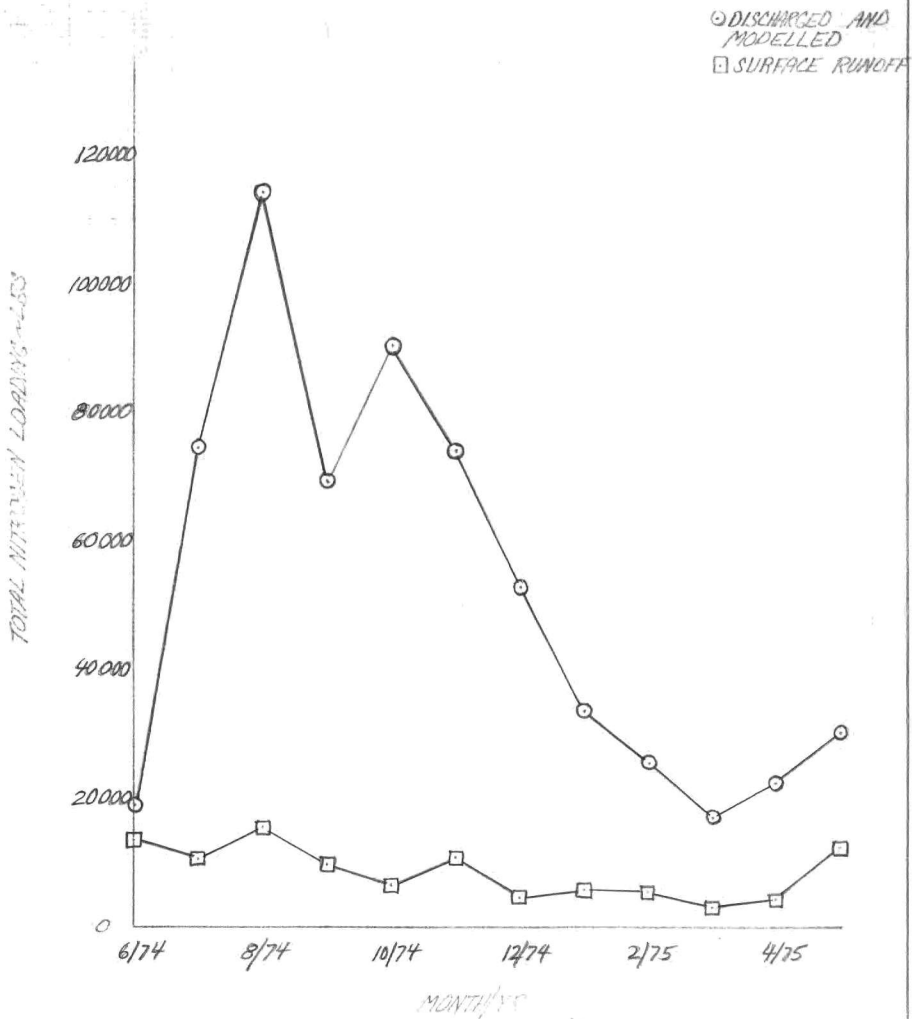
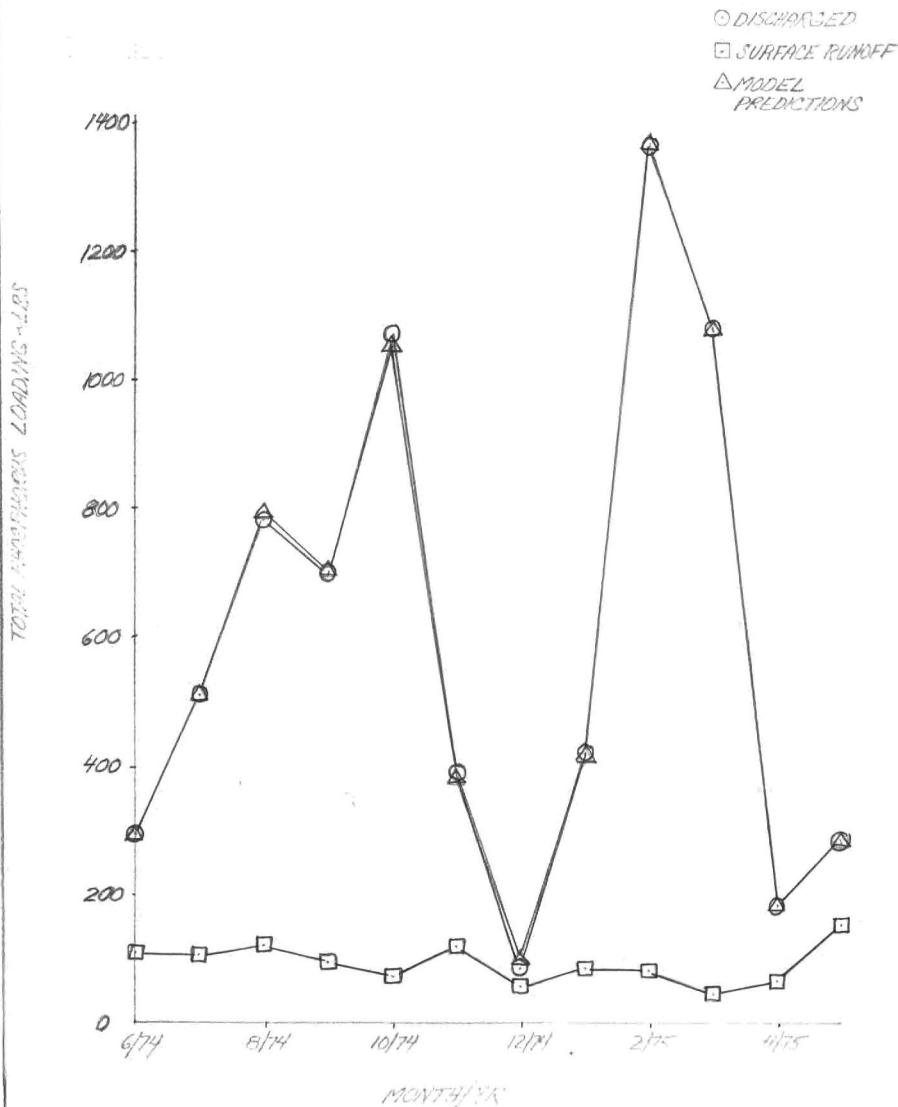


FIGURE 14  
 WEST TAMPA BAY BASIN  
 TOTAL PHOSPHORUS LOADINGS FOR THE  
 DATA BASE PERIOD



All west Tamiami model inputs and their results are given in Exhibits 7.6, 7.7, 7.8 and 7.9 for the 1973-74 and plan scenario land uses.

#### 4.2.2 Summpar for C-4 Basin

- 1) Estimates of the available discharges, their loadings and concentrations for the west Tamiami backpumping alternative for 1973-74 and pattern scenario are made with the use of the CLAD model.
- 2) All quality predictions are based on the data base. Quality data were collected from 6/74 to 5/75 for the west C-4 basin.
- 3) The CLAD model is used to predict pattern scenario water quantities and nutrient quality, and 1973-74 land use nutrient quality from the west Tamiami basin for the rainfall/discharge record of 1/63 to 12/74.

#### 4.3 Hillsboro Canal (C-14) Basin

##### 4.3.1 Discussion

In conjunction with the backpumping studies, the west Hillsboro plus C-14 basin discharges and nutrient water quality are estimated for two land uses: 1973-74 and plan scenario (see Figure 10). The basin discharge CLAD model is used.

The land uses have been aggregated for use in the model as shown in Table 21. Pollutant accumulation rates (lbs/acre/day) and depression storages (interception plus surface ponding) are correlated to land uses. Depression storages, as in the WPCF manual of Practice No. 9, are assumed to be 0.1" for high intensity (smooth) cultivated, and 0.3" for low intensity cultivated. The area weighted nonurban depression storages were calculated to be 0.23" and 0.30" for 1973-74 and plan scenario land uses, respectively. The pollutant accumulation rates used in this analysis are listed in Table 22. These loading rates are half of those as in Table 2. The surface runoff calibration gave a better correlation

Table 21. Hillsboro + C-14

	1973-74 LAND COVER		PLAN SCENARIO	
	Area (Acres)	Percent Imperviousness (Area Weighted)	Area (Acres)	Percent Imperviousness (Area Weighted)
<u>URBAN</u>				
Single Family	5727	39.2	64543	22.7
Multiple Family	546	70.8	2544	65.0
Commercial	289	87.1	1513	84.6
Industrial	2620	10.8	3065	65.6
Open or park	19540	5.0	3253	19.6
Total Urban	<u>28722</u>		<u>74918</u>	
<u>NONURBAN</u>				
Cultivated	17390		1740	
Pasture	14329			
Woodland	19718		3501	
Total Nonurban	<u>51437</u>		<u>5241</u>	
Total Basin	80159		80159	

Table 22. Pollutant Accumulation Rates (lbs/acre/day)  
 Hillsboro plus C-14 Basin

<u>URBAN</u>	<u>BOD<sub>5</sub></u>	<u>Total Nitrogen</u>	<u>Total Phosphorus</u>	<u>Suspended Solids</u>
Single Family	0.0223	0.00281	0.000585	0.0
<b>Multiple Family</b>	0.0530	0.0117	0.001915	0.0
Commercial	0.244	0.0156	0.00535	0.0
Industrial	0.0880	0.02475	0.003445	0.0
Open or Park	0.0061	0.00379	0.000122	0.0
 <u>NONURBAN</u>				
Pasture	0.01345	0.00650	0.0003665	1.027
Cultivated	0.0220	0.0318	0.001285	5.134
Woodland	0.0061	0.00379	0.000122	0.120
 <u>NONURBAN AREA WEIGHTED</u>				
<b>1973-74</b> Land Uses	0.0135	0.01401	0.000583	4.136
Plan Scenario	0.0114	0.01309	0.000508	3.569

to the discharged loadings with these reduced loading rates. These pollutant accumulation rates were input to STORM in lbs/acre/day as previously explained.

The exponents for dust and dirt washoffs used are 4.6 and 0.46 for urban and nonurban land uses, respectively. These are arrived at by calibrating STORM's output to the trends and limits in the data base for Total Nitrogen and Total Phosphorus. The following combinations of urban and nonurban exponents were tried: 14,4.6; 15,0.46; 15,0.05; 4.6,4.6; 4.6,0.46; 4.6,0.05; 0.46,4.6; 0.46,0.46; 0.46,0.05.

The rainfall data used in this basin analysis is that of the Boca Raton station. This hourly precipitation data is stored on tape at FSU in Tallahassee (location RI1098, number 7782, file 4), or is available on cards.

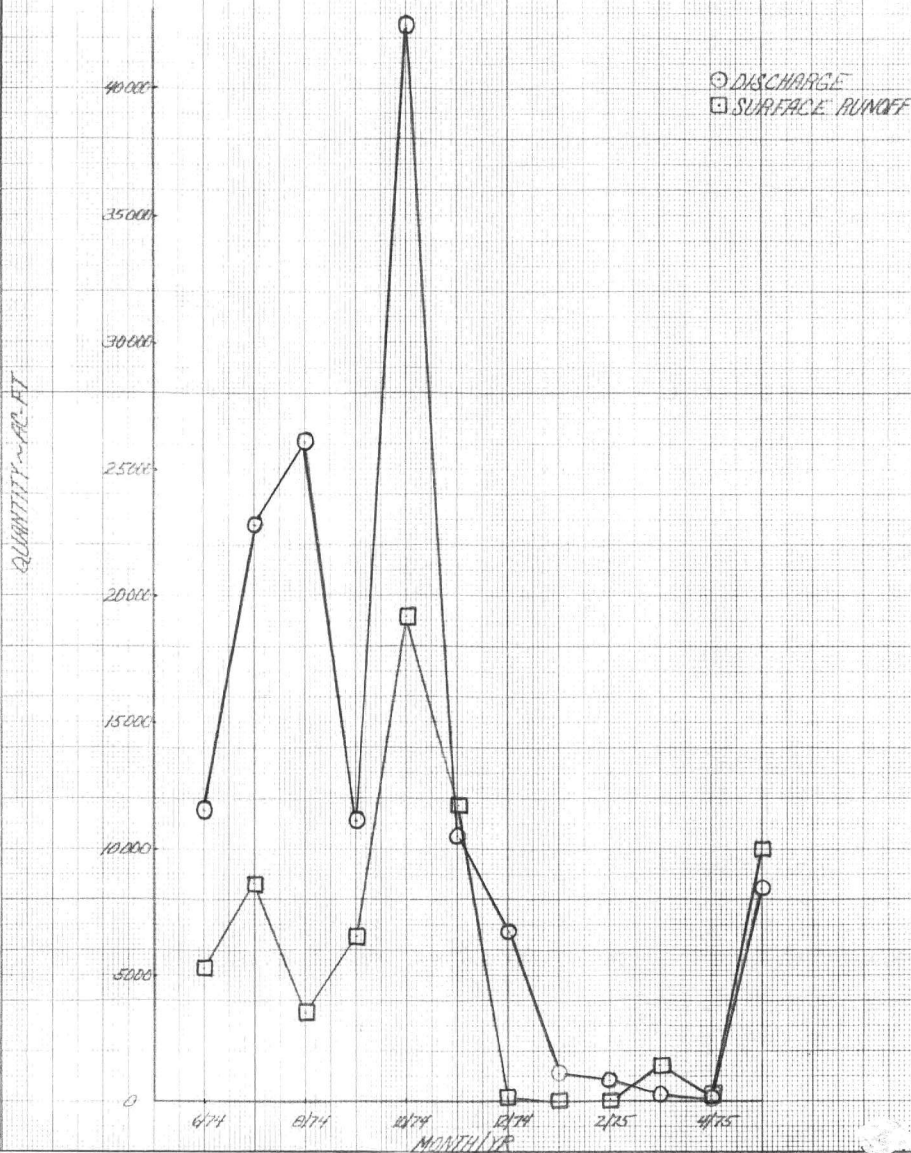
The runoff coefficients used in this analysis are: 0.20 for urban pervious areas, 0.90 for urban impervious areas, 0.23 for nonurban areas, and 0.40 for urban impervious areas with grassed swale drainage. For the 1973-74 and plan scenario land uses, the area weighted runoff coefficients are calculated to be 0.255 and 0.284, respectively. Figure 15 illustrates the resultant proportionment of surface runoff to discharges for the data base period.

When estimating the future urban areas runoff coefficients, ninety percent of future developments are assumed to have grassed swales, the remaining ten percent to have curb and gutter drainage. The area to be developed, calculated from the differences in the plan scenario and 1973-74 land uses, is 62483 acres. The resultant impervious runoff coefficient is 0.525.

This analysis assumed no abatement measure would be required for nonurban land uses. Two probable abatement measures are included as nutrient sinks for future urban developments: grassed swales and detention basins. It is assumed that 50% of the newly developed urban areas will be required to have detention basins and 90% will have grassed swales. Removal efficiencies are calculated to be 22.7% for Total Nitrogen and Total Phosphorus.



FIGURE 15  
 HILLSBORD + C-14 BASIN QUANTITIES OF THE  
 DATA BASE PERIOD



Potential evaporation rates of Table 11 are used to calculate future surface water evaporations by assuming detention basins would use 10% of the new developments land area.

Historical discharges are calculated by the Water Resources Division using the positive differences in flow between the Deerfield Locks (02281500, Hillsboro Canal near Deerfield Beach) and S39 (Hillsboro near Deerfield) plus the positive differences in flow between S37A (02282100, Cypress Creek Canal) and S-38 (Conservation Area 2). This is done on a daily basis.

Future discharge calculations are made from historical discharges, surface runoff calculations, depression storage evapotranspiration, and surface water evapotranspiration and are correlated to the increase in impervious cover. This increased fraction imperviousness is calculated as 0.144 or 14.4 percent.

Quality calculations are based on one year of bimonthly data from 6/74 to 5/75, see Table 23. Monthly nutrient values are obtained by simply averaging the 3 collection stations.

The quality calculations are made with a mass balance approach. Yearly discharged nutrients from the CLAD model are equated to the calculated loadings from the data base. Table 24 and Figures 16 and 17 present the resultant model outputs with the quality data for the calibration period (6/75 - 5/75). Total discharged pollutants are equated to the sum of those in surface runoff plus those from other nonpoint sources and sinks. These other nonpoint concentrations are set to match yearly and monthly loadings.

All Hillsboro plus C-14 model inputs and their results are given in Exhibits 7.10, 7.11, 7.12 and 7.13 for the 1973-74 and plan scenario land uses.

#### 4.3.2 Summary

- 1) Estimates of the available discharges, and their loadings and concentrations for the Hillsboro plus C-14 backpumping alternative for 1973-74 and plan scenario land uses are made with the use of the CLAD model.

Table 23. Hillsboro + C-14 Surface Water Quality Data

Date	TKN (mg/l)	No. TKN Samples	NO <sub>3</sub> -N (mg/l)	No. NO <sub>3</sub> Samples	NO <sub>2</sub> -N (mg/l)	No. NO <sub>2</sub> Samples	Total N = TKN+NO <sub>x</sub> (mg/l)	Total P (mg/l)	No. TP Samples
June 74'	1.29	6	0.046	6	0.010	6	1.35	0.035	6
July'	2.19	3	0.052	3	0.010	3	2.25	0.069	3
August	2.08	6	0.048	6	0.009	6	2.14	0.250	6
September	1.36	3	0.032	6	0.006	6	1.40	0.124	6
October	1.40	9	0.048	9	0.011	9	1.46	0.251	9
November	0.92	6	0.138	5	0.011	6	1.07	0.109	6
December	1.06	3	0.270	3	0.019	3	1.35	0.186	3
January 75'	1.24	6	0.057	6	0.015	6	1.31	0.056	6
February	1.26	3	0.017	3	0.019	3	1.30	0.042	3
March	1.13	6	0.039	5	0.010	6	1.18	0.042	6
April	1.39	6	0.012	6	0.005	6	1.41	0.028	6
May	1.80	9	0.045	9	0.009	9	1.85	0.048	9

FIGURE 16  
 HILLSBORO+C-14 TOTAL NITROGEN LOADINGS OF THE  
 DATA BASE PERIOD

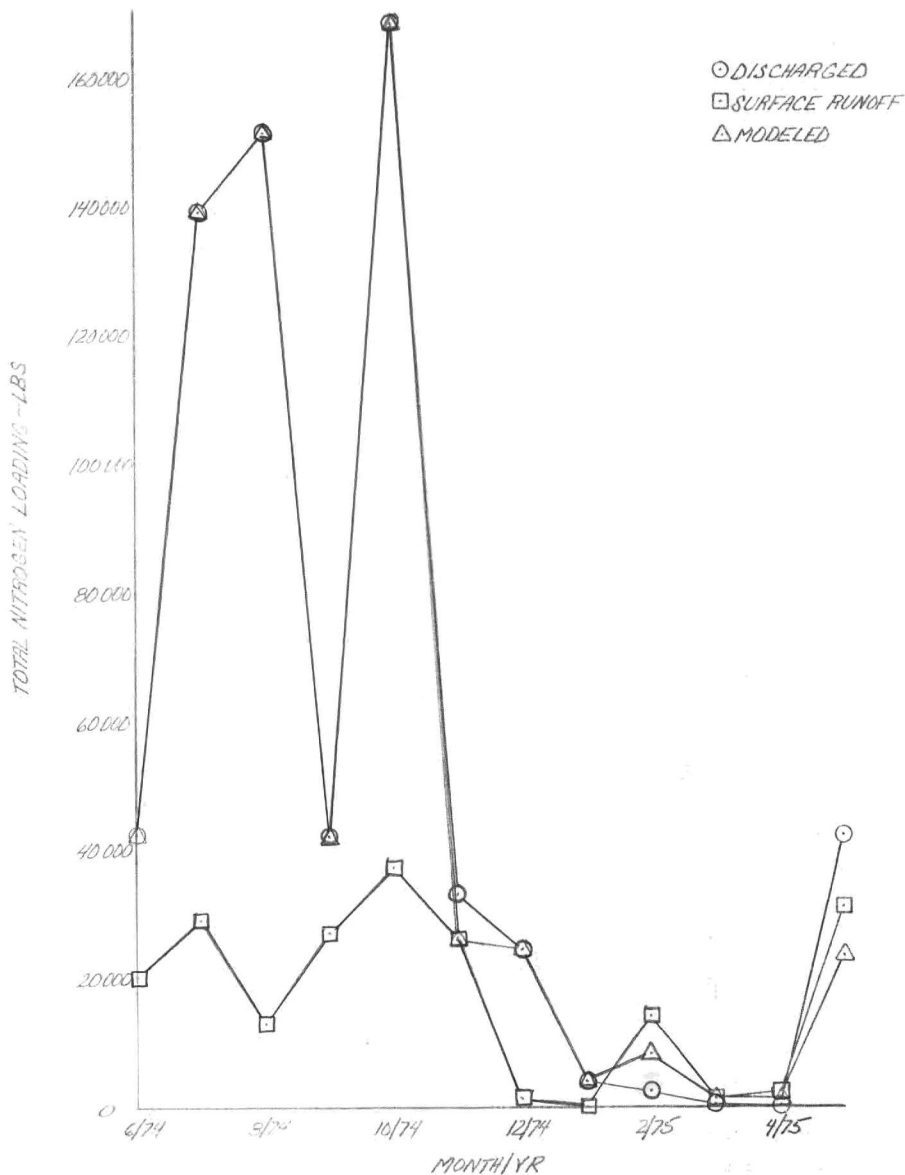


FIGURE 17  
 HILLSBORO + C-14 TOTAL PHOSPHORUS LOADINGS  
 DATA BASE PERIOD

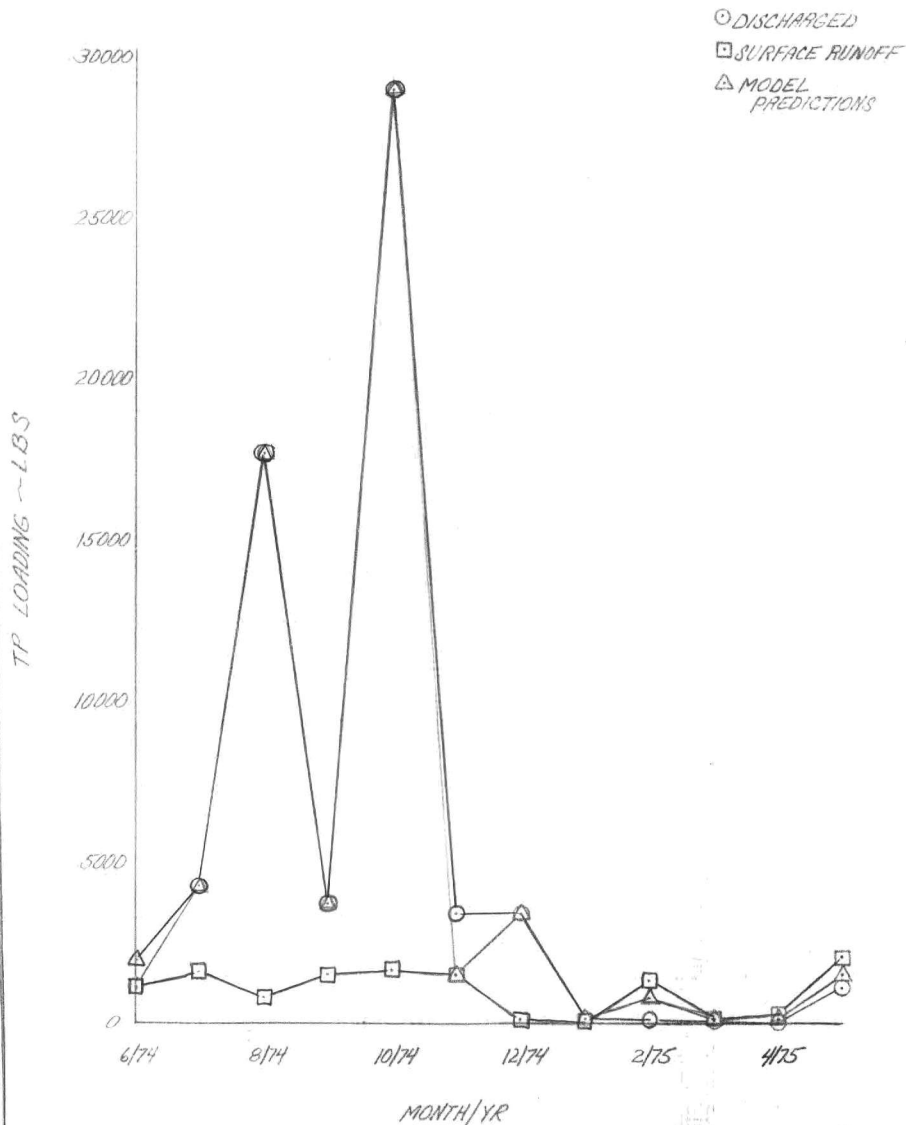


Table 24. Hillsboro + C-14 Basin Quantities and Quality Data Base Period

Date	Discharge (Ac-Ft.)	D A T A		B A S E		M O D E L E D			
		Total Nitrogen Loading (lbs)	Conc. (mg/l)	Total Phosphorus Loading (lbs)	Conc. (mg/l)	Total Nitrogen Loading (lbs)	Conc. (mg/l)	Total Phosphorus Loading (lbs)	Conc. (mg/l)
June 1974	11566	42436	1.35	1100	0.035	42505	1.35	1942	0.062
July	22806	139456	2.25	4277	0.069	139518	2.25	4263	0.069
August	26075	151653	2.14	17716	0.250	151602	2.14	17717	0.250
September	11103	42246	1.40	3742	0.124	42230	1.40	3740	0.124
October	42500	168634	1.46	28992	0.251	168821	1.46	29005	0.251
November	11480	33384	1.07	3401	0.109	26064	0.84	1535	0.049
December	6742	24736	1.35	3408	0.186	24662	1.35	3404	0.186
January 1975	1177	4190	1.31	179	0.056	4197	1.31	178	0.056
February	823	2908	1.30	94	0.042	8394	3.75	799	0.357
March	240	737	1.13	27	0.042	1753	2.69	167	0.257
April	40	151	1.39	3	0.028	1711	15.74	179	1.648
May	8438	42425	1.85	1101	0.048	23816	1.04	1554	0.068
Total (Avg.)	142990	652956	(1.68)	64040	(0.165)	635273	(1.63)	64483	(0.166)

- 2) All quality predictions are based on the data base period from 6/74 to 5/75.
- 3) The CLAD model is used to predict plan scenario water quantity and nutrient quality, and 1973-74 land use nutrient quality for the rainfall/discharge record of 1/63 to 12/74.
- 4) Nonpoint source pollution is ill defined. The nutrient pollutant accumulation rates are halved in the data calibration from those previously used in the west C-51 basin.

## 5. CONCLUSIONS AND RECOMMENDATIONS

### CONCLUSIONS

1. The CLAD model estimates the quantity and quality of water discharged from a basin for some projected land use on a monthly basis.
2. Both quantity and quality computations of the model are based on mass balance principles with the levels of details being consistent with input data accuracy and the desired output.
3. Land use cover analysis, projected land uses, hourly rainfall, historical discharge records, land use pollutant accumulation rates and general basin description parameters are the major input requirements of the model.
4. Discharge predictions do not consider increased water demands within the basin because such aspects are separately handled by a contemporary optimization model.
5. The model predicts water quality using at least one year of historical data (monthly or more frequent) coupled with the STORM model of the Corps of Engineers.

6. Nonpoint sources of pollution other than surface runoff are ill defined, making future quality projections difficult. The CLAD model assumes constant monthly concentrations of other nonpoint sources and sinks from year to year.
7. No mixing effects are presently considered in the model. Although stored stream or canal waters can have a significant effect on water quality during periods of low rainfall and low discharge conditions, these periods are of minimum concern in the backpumping analyses for which the model is primarily developed.
8. Point sources are considered but they are external to the model.
9. In a natural stream as opposed to canal drainage (as in our case), the variability and extent of the sink term should be assessed with additional program calibrations and/or modifications.
10. This model cannot be used to estimate peak discharges or peak pollutant concentrations. The model outputs are average monthly pollutant concentrations and discharges.
11. Future surface runoff abatement schemes for urban land uses can be simulated using the overall treatment efficiency estimations.

#### RECOMMENDATIONS

1. Stream or canal mixing effects should be incorporated in the CLAD model to make quality predictions of the dry season more accurate.
2. The model should be updated with more knowledge concerning other nonpoint sources and sinks with a better definition of the groundwater balance.



3. While applying the CLAD model to a natural watershed as opposed to canal drainage, several model verification and modification procedures may be necessary.
4. The CLAD model should be updated with the latest version of the STORM model so that land use loading rates in lbs/acre/day can be directly used and the SCS method of calculating runoff can be incorporated.

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EXHIBIT 7.1: Input Set for Western C-51





CS1WEST 66	6131	17303	44524	6077	35824
CS1WEST 67	4360	5387	1476	0	169
CS1WEST 67	10524	14162	40056	11770	5820
CS1WEST 68	1708	3820	4788	75	20828
CS1WEST 68	22963	23623	44430	14162	2239
CS1WEST 69	7900	3342	12902	4661	15539
CS1WEST 69	22340	24801	42046	32338	15812
CS1WEST 70	11480	15423	45546	16330	20949
CS1WEST 70	17687	14505	17179	2053	194
CS1WEST 70	17687	14505	17179	2053	194
CS1WEST 71	670	272	0	26	3130
CS1WEST 71	11845	19620	9503	33767	10161
CS1WEST 72	9098	6619	2747	12081	43137
CS1WEST 72	18664	12266	6657	10449	5897
CS1WEST 73	4181	2908	2410	1303	4026
CS1WEST 73	29603	41619	29849	9366	9146
CS1WEST 74	58415	5349	1934	52	26
CS1WEST 74	27868	21697	26031	11677	13127
CS1WEST 75	3695	936	450	0	0
CS1WEST 75	0	0	0	0	0

CS1WEST					
CS1WEST					
CS1WEST					
CS1WEST	.52	.72	.40	.40	1.21
CS1WEST	1.91	1.52	1.77	.41	2.69
CS1WEST	.148	.040	.040	.040	.040
CS1WEST	.080	.074	.121	.150	.108
CS1WEST	0.0	0.0	.247	.247	

11.12 0NPSCP 3.66  
.121 0NPSCP .256  
REF

ADYBFD 77/02/15.FLORIDA STATE UNIVERSITY KRONOS  
ADYBFD 77/02/15.FLORIDA STATE UNIVERSITY KRONOS

17.03.04 JGF.T50.CM120000.H0. FDY  
17.03.07 ACCOUNT  
17.03.08 STAGE1.R11098.7782/TAPE11.  
17.04.13 MTS1.ASSIGNED TO STAGEIN, VSN=\*\*\*31.  
17.04.22 STAGING COMPLETE  
17.04.22 CBR,CARDS  
17.04.22 COPY COMPLETE  
17.04.23 CBR,CARD2  
17.04.23 COPY COMPLETE  
17.04.23 CBR,IPI  
17.04.23 COPY COMPLETE  
17.04.23 CBR,IPI2  
17.04.23 COPY COMPLETE  
17.04.23 CBR,IPI3  
17.04.23 COPY COMPLETE  
17.04.24 G.STORM.SUMMB  
17.04.46 CALL (PROG2(LEN=LAND.NAME=IPI))  
17.04.49 RA.INPUT  
17.04.50 ASSICN.MS.OUTPUT  
17.04.50 D100.ASSIGNED TO OUTPUT  
17.16.24 STORM(IPI)  
19.03.45 STOP  
19.03.45 RENAME.QUAL=TAPE13  
19.03.45 RENAME.OUT=OUTPUT  
19.03.45 RA.INPUT  
19.16.03 SUMMB  
19.18.39 STOP  
19.18.39 RENAME.LAND=QUALSUM

EXHIBIT 7.2: CLADM Hydrologic Output for Western C-51 Using 1973-74  
Land Uses and Planned Scenario

Note: SWET, DSET, NGWL are defined in the Report and  
these notations are also used in subsequent  
Exhibits No. 7.7 and 7.11



73-74 LAND USES

RAINFALL DISCHARGE RUNOFF

63 1	4678	3469	187
63 2	4678	3469	187
63 3	19024	7053	3056
63 4	12662	6109	1934
63 5	0	547	0
63 6	44099	12939	8109
63 7	30813	4553	30813
63 8	16280	2999	2121
63 9	5496	5496	16280
63 10	32842	9543	94
63 11	14221	25225	1435
63 12	10354	1185	10354
64 1	42290	8864	9231
64 2	284493	115722	46656
64 3	284493	115722	46656

50	50	50	50
21	4810	6937	8424
385	385	385	385
79	19149	4944	8462
79	4709	18393	7360
88	2183	7894	886
100	11546	41253	36365
1028	11627	2058	21831
1066	11103	59319	12873
94	13145	18610	3244
75	7455	31524	28447
60	4701	3954	10997
40	6018	3844	3844
40	6018	3844	3844
856	99359	102819	83281

62	4292	2308	2308
3905	4746	20958	3905
0	6674	0	437
0	15906	0	2332
811	6736	811	811
12213	84955	12213	1000
32319	69259	17413	17413
1068	20872	19630	1068
4298	35741	4298	4298
11014	85327	18650	75
374	42722	374	374
374	42722	374	374
6014	8171	6014	998
359717	187754	65120	65120

50	2947	-4081	-4854
21	5038	11153	9994
38	1674	1789	998
79	3324	12188	10921
88	3344	3304	2961
100	12923	59972	57358
105	17363	17484	17484
1068	9832	-9296	-10374
94	15123	9510	8322
75	6062	23902	20522
804	41216	-41216	-45997
804	41216	-41216	-45997
60	3995	-1878	-2036
856	87448	83859	62722

50	9288	13159	11791
21	3760	4963	4447
38	6492	-10600	936
79	5980	25646	8359
88	10374	18339	18433
100	16228	34614	20446
105	18425	-21233	34614
106	14892	22224	-33698
94	16015	20628	18484
94	16015	20628	18484
75	4973	-6560	-7321
60	5381	-8593	-6242
60	6479	815	730
856	118527	100415	80303

50	3923	-2844	-3174
50	3923	-2844	-3174
374	4360	7	561
5489	4360	7	3288

SCENARIO LAND USES

RUNOFF DSET SWEET DISCHARGE

437	2966	692	4073
437	2966	692	4073
3930	3614	291	9992
2433	3152	516	7283
9544	6674	1208	16794
5801	10933	1369	10946
2807	5273	1437	4400
6986	8994	1455	11093
11103	9291	1287	28603
2058	6149	1035	29508
1622	3994	931	11261
1930	544	15184	15184
57013	9992	11753	147534
57013	9992	11753	147534

1934	4393	692	16292
5052	3255	291	13387
4054	3250	516	6921
7360	5630	1088	9382
8757	1208	1369	11093
3306	8987	1437	15009
19312	8685	1455	19182
3244	9239	1287	27712
14534	5097	1035	27712
2682	3579	931	9544
3359	3359	544	13614
2682	3359	544	13614
87645	87645	11753	205832

250	1389	692	4841
4242	4325	291	6348
998	2760	516	1795
3555	1983	1088	1934
1123	2334	1208	1508
19461	8637	1369	21211
17484	12794	1437	17584
3618	6083	1455	23106
8322	6300	1287	18986
20646	5362	1035	59408
437	658	931	46878
437	658	931	46878
2301	2301	544	7422
76536	76536	11753	225658

9882	5383	692	22740
11791	4447	291	21191
936	4128	516	14983
8359	3389	1088	8709
3046	1297	1369	13813
20446	10748	1437	56321
34614	18433	1455	19182
15968	10733	1455	41251

67	3	49	1476	1499	38	2902	574	514	873	1566	516	2394
67	4	0	0	0	79	0	-79	-86	0	0	1088	0
67	5	3493	169	62	88	3232	34567	33977	187	2759	1208	0
67	6	72105	16253	12163	100	2823	37987	4	14731	14378	1369	23978
67	7	69423	20432	13972	103	10963	37993	33981	15686	8027	1437	25978
67	8	23328	10524	3181	106	10018	2680	2401	4304	6450	1455	17022
67	9	23328	10524	3181	106	10018	2680	2401	4304	6450	1455	17022
67	10	45658	14162	8109	94	11730	19672	17627	2666	7629	1385	18245
67	11	34181	40056	5239	75	12330	-18209	-20521	6736	1431	630	12685
67	12	43661	11770	561	60	2017	-7481	-13681	2932	2351	544	12685
67	13	13847	5820	4191	3799	85352	68134	68134	85352	11753	11753	163249
67	14	130381	130381	51333	856	85352	68134	68134	85352	11753	11753	163249
68	1	4429	1708	624	50	1819	882	767	811	1249	692	1725
68	2	3368	3820	4117	21	3680	10252	9186	4179	3364	291	6912
68	3	20883	4798	4117	38	3608	12389	11101	4741	516	516	6973
68	4	4366	758	125	79	3844	368	330	437	2854	1088	284
68	5	53081	20828	9044	88	12338	16957	15169	19216	10567	1088	26470
68	6	121833	90365	26821	100	14359	21795	19477	23676	14367	1437	55323
68	7	59693	51749	11165	105	12377	-5158	-574	13037	8970	1437	55323
68	8	59693	51749	11165	105	12377	-5158	-574	13037	8970	1437	55323
68	9	30598	22869	4533	106	11886	-4053	-419	5933	7845	1455	26028
68	10	29379	23625	3867	94	13198	-7539	5260	9326	8932	1287	27672
68	11	35622	44430	5926	75	7829	-1914	-2892	6737	5804	1035	47382
68	12	18213	14162	3555	60	3337	18754	586	4117	2669	831	14327
68	13	2239	2239	0	40	0	-2239	0	0	544	1389	0
68	14	280768	73165	80556	856	94375	24511	13454	85707	64419	11753	310684
69	1	11976	7900	1996	50	3624	462	360	3720	2681	692	8243
69	2	11539	3342	2058	21	2927	526	4703	2485	1295	291	4790
69	3	28890	12902	5177	38	7219	8722	7815	6307	4174	516	1573
69	4	8233	4661	1123	79	3536	-148	0	8957	2167	1088	4830
69	5	43912	15339	4233	88	18255	18459	5262	28264	9178	1208	19700
69	6	107035	31234	21519	100	18936	86758	52007	11987	1369	1369	41180
69	7	27507	18067	3867	103	11326	-1391	-2422	24561	11683	1437	41180
69	8	28282	4064	4054	106	15908	-5482	-6118	16612	7839	1455	26997
69	9	51147	24801	8046	94	17480	8772	7860	9835	12300	1631	59500
69	10	73977	42046	14284	75	14211	17693	15811	1112	833	46109	0
69	11	25750	33338	5364	60	5125	-10933	-12224	6930	3649	544	35100
69	12	7984	15812	1247	7984	22664	-10632	-11865	3649	3649	544	17436
70	1	14159	11480	1622	50	7374	-4784	70393	85744	73909	11753	270467
70	2	15032	15032	2495	21	4293	-5078	-5895	3485	4375	692	14387
70	3	82004	45546	18775	38	6648	32974	29343	27079	7391	291	17038
70	4	4366	16330	686	79	1495	-13108	936	936	1088	516	11119
70	5	33117	7077	6612	88	7453	20493	18468	2336	657	1088	17689
70	6	38988	27856	10292	100	18226	15136	13863	17547	5356	1366	10931
70	7	62994	20949	6090	105	14379	4261	3818	1855	9474	1437	253545
70	8	27320	17687	3930	106	10878	-1331	-1508	1508	7782	1437	19513
70	9	46656	14505	6612	94	18992	13063	11107	9483	13353	1635	20232
70	10	19710	17179	2557	75	9910	-6534	7314	3493	6012	935	19577
70	11	0	2083	0	60	0	-2113	-2358	0	215	544	1537
70	12	4366	1894	249	80	3322	53435	40555	56	931	544	1537
70	13	196231	59880	97370	856	97370	53435	40555	72168	65104	11753	230700
71	1	10916	670	1684	50	3969	6337	5669	3121	2539	692	1936
71	2	3177	272	374	21	3811	1273	1141	749	2242	291	1593
71	3	2058	0	62	58	1197	237	200	250	1080	516	242
71	4	10292	26	1372	38	1437	5573	500	250	1080	516	242
71	5	28131	3130	1572	66	15927	5927	16895	2658	2230	1088	1933
71	6	31439	11232	8609	106	15443	24648	22118	4298	3620	1208	2468
71	7	5143	0	0	106	15443	24648	22118	18633	8898	1387	19074
71	8	5143	0	0	106	15443	24648	22118	18633	8898	1387	19074

71	8	2856	11845	3742	18909	3708	3233	5302	7726	1455	1087	6214	12515
71	9	3791	19620	5926	13193	5079	4551	7485	7485	1035	4837	7532	25051
71	10	3713	9503	3738	13103	14432	12352	8949	8949	1035	4837	7532	25051
71	11	3367	33767	11539	60	5360	12593	12593	12593	544	11401	11401	11401
71	12	18089	10161	3493	3874	4414	3953	66618	62297	11753	11753	133134	133134
72	1	32338	115326	53316	93614	107512	96364						
72	2	1237	9098	1185	7579	-4190	-4576	3181	3976	692	12515		
72	3	8296	686	686	5925	-3769	-4206	1248	3404	8807	8807		
72	4	8296	6619	6619	5925	-3769	-4206	1248	3404	291	291		
72	5	2574	2747	3239	3851	19138	4706	4706	4706	1113	6796		
72	6	58757	12081	11477	10736	33681	32134	17149	7634	1088	17901		
72	7	61003	43137	10354	18779	99	89	18375	11837	1208	47619		
72	8	77532	37354	14009	17545	2833	2339	1884	12222	1369	61402		
72	9	37051	21967	5676	13301	1678	1304	1684	9658	1437	24455		
72	10	18664	1684	1684	15037	-11724	-13068	1771	3950	1455	21104		
72	11	6837	1746	811	5839	-8968	-10008	3772	4053	1035	74745		
72	12	10449	10449	686	6041	-7638	-8244	2058	3467	544	7002		
73	1	11539	5837	1359	5015	587	3246	2058	3467	544	7002		
73	2	34496	206936	59512	112222	24482	13956	68725	74266	11753	244591		
73	3	31437	4181	5801	7165	20041	17858	6737	5019	692	7768		
73	4	31437	4181	5801	7165	20041	17858	6737	5019	692	7768		
73	5	14908	2908	2245	2191	6467	5795	7445	4145	291	4657		
73	6	14159	2410	2308	4503	7208	6459	2932	2682	316	1847		
73	7	4366	374	374	2800	184	165	686	1856	1088	4854		
73	8	15331	4036	15331	883	6064	3533	1832	7494	1369	21576		
73	9	47530	16733	8608	11314	18183	1780	1872	9891	1437	45747		
73	10	64683	40932	11851	10596	8490	1080	15972	1730	1285	35305		
73	11	52457	29693	7734	1065	20995	2653	9620	9620	1285	48527		
73	12	47343	41619	7797	94	14720	-3090	4746	2732	1035	34349		
73	1	26322	29849	3355	11446	-15048	-12784	4746	2732	1035	34349		
73	2	10167	9386	1622	60	3382	-8641	1996	2447	831	9943		
73	3	19648	9146	3368	40	3555	4307	4179	3239	544	11448		
73	4	348551	192136	57636	107141	48418	37495	70736	71167	11753	228136		
74	1	34868	28415	7235	4593	1810	1822	8109	3089	692	29485		
74	2	3056	5349	125	21	-1846	-5476	2078	291	6097	6097		
74	3	11103	1934	2245	38	7404	6534	839	516	3124	3124		
74	4	1687	52	811	79	3594	3262	1185	1839	1088	637		
74	5	16467	36	2121	88	7594	17539	2007	5400	1308	1950		
74	6	44598	11466	7485	100	13820	17839	9569	8641	1369	16889		
74	7	73727	22746	13161	105	18659	32317	28868	15266	2731	31091		
74	8	26896	27868	3493	106	12081	-19359	4492	916	1435	32044		
74	9	42353	21697	6487	94	15210	-19359	4492	916	1435	32044		
74	10	18401	26591	3493	75	3783	-19359	4492	916	1435	32044		
74	11	26010	11677	4429	60	7480	-6097	5177	5708	831	27955		
74	12	11976	13127	2121	40	3103	-4534	2433	2436	544	13788		
74	1	11976	13127	2121	40	3103	-4534	2433	2436	544	13788		
74	2	315742	170428	53206	93120	51536	38521	64685	62084	11753	203984		
75	1	1372	3685	0	50	1372	-4179	62	1128	692	3731		
75	2	425	950	0	21	1622	-1090	62	1377	291	1044		
75	3	425	950	0	38	2863	1078	966	224	1983	516	964	
75	4	4853	4407	125	79	4031	443	437	2841	1088	227	2841	
75	5	25761	4407	3056	12973	8293	7431	4179	9372	1308	7750		
75	6	0	0	0	100	100	-100	0	1369	0	1369		
75	7	0	0	0	105	0	-112	0	1437	0	1437		
75	8	0	0	0	106	0	-118	0	1455	0	1455		
75	9	0	0	0	94	0	-94	0	1035	0	1035		
75	10	0	0	0	75	0	-75	0	1035	0	1035		
75	11	0	0	0	60	0	-60	0	544	0	544		
75	12	0	0	0	40	0	-40	0	544	0	544		
75	1	37737	9508	3555	22861	4512	2877	5364	16701	11753	13717		

EXHIBIT 7.3: CLADM Quality Output for Western C-51  
Using 1973-74 Land Uses.

TLSS = Total Loading for Suspended Solids.

TLBOD = Total Loading for Biochemical Oxygen Demand (BOD)

TLN = Total Loading for Nitrogen

TLP = Total Loading for Phosphorus

TCSS = Total Concentration for Suspended Solids

TCBOD = Total Concentration for BOD

TCN = Total Concentration for Nitrogen

TCP = Total Concentration for Phosphorus

The same notations are used in subsequent exhibits No. 7.4, 7.8, 7.9,  
7.12 and 7.13.



64	8	22	41	47909	46053	2021	64.73	1.37	1.32	.058
64	9	19305	4814	97384	30	1.53	0.98	30	1.53	.076
64	10	50550	44448	91596	71	1.31	14.53	71	1.31	.077
64	11	377967	13755	25759	349	1.40	17.63	349	1.40	.140
64	12	3168546	76134	3196	54	2.50	16.93	54	2.50	.105
		324152	745304	42811	72	1.66	29.12	72	1.66	.096
65	1	13334	10043	2013	0.00	1.14	0.00	1.14	.86	.173
65	2	23220	15843	806	102.91	1.80	1.23	1.80	1.23	.063
65	3	0	0	0	0	1	1	1	1	1
65	4	0	0	0	1	1	1	1	1	1
65	5	0	0	0	1	1	1	1	1	1
65	6	3158144	68409	2484	97.16	2.10	1.82	2.10	1.82	.076
65	7	3781984	48354	15526	39.64	55	2.69	55	2.69	.177
65	8	3861984	48454	15526	39.64	55	2.69	55	2.69	.177
65	9	1646444	18231	98492	4246	34	1.85	34	1.85	.080
65	10	174828	27691	42653	58.39	32	1.42	32	1.42	.070
65	11	1213242	46512	211226	8.13	1.41	1.41	1.41	1.41	.091
65	12	37316	4727	17289	0.91	49	4.41	49	4.41	.149
65	13	28557	46251	2161	10.26	1.75	2.83	1.75	2.83	.132
65	14	11921166	747404	60171	23.36	54	1.50	54	1.50	.118
66	1	1328019	30354	5017	31.05	48	.61	48	.61	.102
66	2	54048	18977	38640	.39	35	.71	35	.71	.039
66	3	20468	14324	17374	1.93	44	.53	44	.53	.049
66	4	175206	15981	9189	13.50	70	.70	70	.70	.036
66	5	1353781	24134	25112	16.63	69	.92	69	.92	.040
66	6	2156110	38096	7257	52.13	38	5.33	38	5.33	.074
66	7	1028308	21539	35923	8.38	33	3.30	33	3.30	.229
66	8	2438310	31581	13749	24.03	33	1.40	33	1.40	.060
66	9	1563806	23839	53346	40.40	49	1.10	49	1.10	.052
66	10	1658606	23839	53346	40.40	49	1.10	49	1.10	.052
66	11	181969	20438	106667	12.44	31	1.62	31	1.62	.109
66	12	11056	12851	2884	94	1.2	.62	1.2	.62	.161
66	13	308226	12851	2884	21.04	1.24	2.38	1.24	2.38	.108
66	14	1122048	258077	64890	18.72	.41	2.26	.41	2.26	.102
67	1	73733	18662	11534	6.39	1.52	.97	1.52	.97	.172
67	2	216442	29305	21513	83.09	2.00	1.47	2.00	1.47	.069
67	3	193663	7237	16342	48.28	4.22	1.80	4.22	1.80	.131
67	4	0	0	0	1	1	1	1	1	1
67	5	0	0	0	48.30	15.49	1.57	48.30	15.49	1.157
67	6	460467	7114	532	0.00	1.25	3.71	1.25	3.71	.072
67	7	273855	33933	3181	194.42	1.30	1.66	1.30	1.66	.102
67	8	250991	92100	5689	42.74	.61	1.73	.61	1.73	.079
67	9	2509389	40463	43622	287.00	1.85	1.42	1.85	1.42	.067
67	10	2113220	2563	59572	59.87	1.93	.56	1.93	.56	.114
67	11	501352	187652	12380	20.37	38	1.72	38	1.72	.153
67	12	12125	17759	4891	9.43	38	1.56	38	1.56	.153
67	13	301352	12125	17759	9.43	38	1.56	38	1.56	.153
67	14	363182	29254	41714	1881	1.85	2.64	1.85	2.64	.153
67	15	1473344	308899	634371	40.85	.87	1.85	.87	1.85	.104
68	1	437447	9235	6628	94.22	1.99	1.43	1.99	1.43	.152
68	2	143467	26010	1296	138.85	3.2	2.51	3.2	2.51	.125
68	3	34398	22901	1032	42.18	2.13	1.73	2.13	1.73	.079
68	4	44465	74326	271	0.00	56.74	1.30	56.74	1.30	.328
68	5	318200	44465	2851	56.21	.80	1.31	.80	1.31	.050
68	6	303770	52426	22320	15.63	8.01	.093	8.01	.093	.093
68	7	1325872	24662	1968014	10.93	1.9	2.98	1.9	2.98	.207
68	8	143614	2466	23044	10.93	1.9	2.98	1.9	2.98	.207
68	9	1409292	19435	4749	22.58	3.9	1.77	22.58	3.9	.076
68	10	503168	24470	4648	18.34	.35	1.48	.35	1.48	.072

68 11	96	15817	4813	25 50	41	57	125
68 12	0	16369	657	0 00	0 00	2 69	109
		395310	86458	20 28	40	3 89	117
		15477268	2966934	20 28	40	3 89	113
		15477268	86458				
69 1	486485	19657	3109	22 66	1 34	1 92	185
69 2	57276	12332	734	36 06	2 47	1 36	84
69 3	1292809	26885	1626	36 87	2 33	1 77	57
69 4	128012	10005	17 21	1 30	1 30	0 83	53
69 5	1348991	40695	1579	31 94	54	3 26	37
69 6	3619821	325348	4619	42 34	50	3 83	37
69 7	828221	151744	16 87	16 87	41	3 99	23
69 8	937900	105635	4536	15 45	31	1 74	65
69 9	1879613	87649	4259	27 89	42	1 50	65
69 10	1673314	157536	10225	14 64	29	1 38	69
69 11	64571	37739	11881	7 13	19	1 51	84
69 12	28397	7428	4481	6 14	17	2 26	44
	1376760	1083799	58238	21 84	45	1 72	62
70 1	54544	24939	4658	17 48	86	1 80	149
70 2	1055514	35633	1905	25 18	38	1 85	105
70 3	1967009	51758	4791	15 89	44	1 58	63
70 4	88721	18944	1825	2 00	11	1 43	58
70 5	1557939	38329	1728	81 00	2 77	1 87	43
70 6	2345855	559441	7021	31 02	48	1 39	99
70 7	1882373	166665	11259	33 06	50	1 98	233
70 8	125373	84801	3666	26 18	47	1 76	106
70 9	322623	33542	2652	58 92	85	1 99	67
70 10	787424	19009	90241	16 87	41	1 72	115
70 11	0 00	4288	937	0 00	0 00	1 50	41
70 12	56279	21930	6979	106 74	41 59	1 89	989
	13867544	317096	46212	26 00	59	1 24	989
71 1	397055	6534	201	218 05	3 59	2 33	110
71 2	95992	11613	284	129 31	15 71	5 46	385
71 3	0 00	0	0	1	1	1	1
71 4	20628	602	291	291 93	8 52	4 12	235
71 5	807090	2373	21180	94 88	2 98	2 49	106
71 6	3856835	57420	905	94 88	2 98	2 49	106
71 7	1661743	122137	2792	186 35	1 88	4 00	931
71 8	1393380	33191	119731	39 96	80	2 80	187
71 9	1807857	24929	2315	43 28	77	1 77	678
71 10	1618104	74008	3588	33 90	49	1 39	106
71 11	1946475	34762	2065	62 65	1 04	1 35	980
71 12	81618	26194	10833	21 46	23	2 23	109
	13709377	267873	32955	2 36	1 84	2 23	109
				43 66	85	1 75	105
72 1	457896	18688	3681	18 52	76	78	149
72 2	340123	11227	16807	18 91	82	53	657
72 3	1018992	24625	14929	186 09	3 03	2 05	676
72 4	994667	44014	34906	30 29	1 34	1 15	648
72 5	1763735	34499	4706	15 04	23	8 47	697
72 6	2529520	30135	132049	16 23	19	2 91	201
72 7	957070	11978	173893	16 03	38	2 51	201
72 8	352797	22480	11978	16 03	38	2 51	201
72 9	248407	15785	94794	6 36	31	1 87	681
72 10	429840	12882	32543	7 45	39	1 58	677
72 11	739860	32997	2121	42 51	97	1 82	152
72 12	239880	15457	16843	8 45	54	1 54	154

10310902	264692	1950914	53774	18.33	47	3.47	0.96
73 1	842791	15496	752	74.17	2.12	1.36	.066
73 2	815715	15588	536	103.21	1.97	1.30	.066
73 3	987382	12345	674	150.75	3.55	1.88	.103
73 4	188370	15619	489	53.16	4.41	1.91	.138
73 5	709371	6783	892	64.83	2.01	1.91	.082
73 6	3208660	59222	290787	70.55	1.30	6.39	.193
73 7	1129334	45599	21952	10.14	4.1	2.92	.156
73 8	131851	32484	21842	16.36	4.0	1.88	.07
73 9	1817872	4060	5796	16.07	2.1	1.38	.066
73 10	1063115	19518	7585	16.07	2.1	1.38	.067
73 11	456471	16209	3591	17.15	64	1.70	.114
73 12	861874	20915	3291	34.67	1.84	2.14	.092
	13376914	318566	58268	25.62	.61	2.26	.112
74 1	787888	25091	9323	10.20	.32	.61	.121
74 2	12749	14109	866	0.00	.88	.97	.060
74 3	347036	634	391	65.35	2.80	1.19	.074
74 4	7139	908	22	50.51	6.43	2.22	.157
74 5	5736	287	7	81.18	4.07	1.66	.103
74 6	1828869	28093	2187	58.69	.90	4.44	.070
74 7	3153337	37480	7924	50.72	.61	1.99	.158
74 8	605434	15699	3741	7.99	.21	1.79	.089
74 9	1772279	59334	3959	30.06	.50	1.37	.070
74 10	941557	12409	7822	13.30	.58	1.06	.131
74 11	2298762	39484	4197	72.43	1.24	1.01	.181
74 12	1201301	16679	3766	33.67	.47	2.37	.106
	12931279	233075	46166	27.92	.50	1.70	.100
75 1	0	10037	1722	0.00	1.00	.83	.172
75 2	0	6990	268	0.00	2.69	1.54	.103
75 3	184811	23395	8179	151.11	19.13	6.69	.474
75 4	0	79.4	0	1	1	1	1
75 5	692068	28708	1024	57.78	2.40	1.84	.085
75 6	0	0	0	1	1	1	1
75 7	0	0	0	1	1	1	1
75 8	0	0	0	1	1	1	1
75 9	0	0	0	1	1	1	1
75 10	0	0	0	1	1	1	1
75 11	0	0	0	1	1	1	1
75 12	0	0	0	1	1	1	1
	876879	69150	3593	33.93	2.68	1.64	.139

RJVBEB. 18.14.30. 77/02/12.

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THIS IS D I S P O S E D O U T P U T .

IT WILL NOT HAVE A CARD DECK.

PLEASE PUT OUT FOR USER 9364003



EXHIBIT 7.4: CLADM Quality Output for Western C-51 Using  
Planned Scenario

Note: Notations Used in This Exhibit is the same in Exhibit 7.3



64 8	2382410	74024	4215	45 81	1 82	1 42	981
64 9	1 87	114970	6548	15 21	1 97	1 53	087
64 10	2935023	108316	7339	39 24	1 38	1 44	097
64 11	644001	30282	8756	11 46	1 19	1 54	156
64 12	970156	68449	4772	25 84	1 92	2 50	127
	17866754	1023793	64036	31 94	1 71	1 83	114
65 1	46084	12077	9242	3 50	4 19	92	234
65 2	1943636	7228	5231	112 66	5 14	1 46	137
65 3	348169	7128	1127	71 37	10 22	1 58	231
65 4	322839	13866	1366	61 42	10 99	2 84	289
65 5	170695	2250	282	20 36	20 36	3 55	445
65 6	3336270	126537	4838	57 87	2 29	2 20	084
65 7	3346270	132115	126537	57 87	2 29	2 20	084
65 8	3346270	132115	126537	57 87	2 29	2 20	084
65 9	3346270	132115	126537	57 87	2 29	2 20	084
65 10	119718	114307	18673	35 22	1 90	2 61	183
65 11	9787	3756	17 83	17 83	1 08	1 82	092
65 12	2376287	58736	63 49	2 97	2 97	1 82	087
66 1	2300266	231335	15709	14 25	1 81	1 81	087
66 2	89776	52471	18987	47 70	4 71	4 71	237
66 3	935440	62709	47 37	2 11	2 11	3 41	237
66 4	45648	80473	27 40	1 28	1 59	1 59	131
66 5	1680102	974462					
66 6	3822669	56364	8015	62 34	1 40	91	139
66 7	386987	58132	3721	5 84	1 17	97	058
66 8	176722	22913	2905	4 34	1 68	1 56	071
66 9	8771	24999	2176	32 68	3 62	1 06	082
66 10	2197202	45311	12640	58 11	2 21	5 97	062
66 11	2847259	77233	13 72	13 72	3 72	3 72	232
66 12	1615058	446642	31778	11 74	5 6	3 72	232
67 1	2491016	159844	7699	22 22	1 74	1 83	069
67 2	2491016	159844	7699	22 22	1 74	1 83	069
67 3	2263940	16970	3703	35 78	8 5	1 10	082
67 4	74644	117483	9750	13 21	7 05	1 77	184
67 5	971968	35960	5784	57 82	4 28	2 83	137
67 6	271938	3746	5746	23 14	1 17	2 37	116
67 7	973287	1014421	89598	24 51			
67 8	18782515						
67 9	303210	15981	3419	23 82	6 82	1 26	289
67 10	82134	36634	2609	37 30	3 56	1 67	278
67 11	475259	12146	1814	73 05	12 25	1 67	278
67 12	0	0	0	0	1	1	1
67 13	0	0	0	0	1	1	1
67 14	0	0	0	0	1	1	1
67 15	0	0	0	0	1	1	1
67 16	5712879	344914	5679	87 93	2 55	5 31	118
67 17	1622813	137245	3140	26 81	1 94	1 94	139
67 18	1498807	92314	41 79	2 72	1 79	1 79	114
67 19	2252266	52254	9350	61 79	1 65	1 65	087
67 20	2847342	21421	14435	23 15	1 55	1 76	118
67 21	2847342	211032	14634	23 15	5 55	1 70	118
67 22	472066	28832	3760	12 39	1 51	1 51	137
67 23	1167424	105176	3778	36 89	5 31	2 59	164
67 24	18464934	56887	5768	41 62	2 02	2 19	159
67 25	894970	970564	57489				
68 1	641019	9298	1131	136 73	7 14	1 77	241
68 2	104952	12375	3575	6 54	3 54	1 67	171
68 3	104952	12375	3575	6 54	3 54	1 67	171
68 4	137375	2910	1621	53 34	3 02	1 78	068
68 5	351076	1270	168 16	76 64	8 38	1 53	539
68 6	244382	10170	45 21	1 57	1 80	1 78	070
68 7	244382	10170	45 21	1 57	1 80	1 78	070
68 8	244382	10170	45 21	1 57	1 80	1 78	070
68 9	244382	10170	45 21	1 57	1 80	1 78	070
68 10	1935061	31333	443795	12 86	5 4	2 33	268
68 11	1665042	121080	6163	23 55	1 08	1 22	087
68 12	75459	11985	6394	26 24	1 06	1 43	083
68 13	197377	7431	11950	9 75	1 52	1 72	113
68 14	120737	22021	6394	9 75	1 52	1 72	113

68 11	5285	49412	25554	5544	13 02	1 23	1 23	134
68 11	5285	49412	25554	5544	13 02	1 23	1 23	134
68 11	5285	49412	25554	5544	13 02	1 23	1 23	134
68 12	19010102	835571	3161476	102632	22 50	0 00	0 00	108
69 1	822951	75455	32111	5328	36 73	1 58	1 43	238
69 2	76005	101107	24616	3527	58 38	7 77	1 89	194
69 3	2717802	102643	42763	3717	61 07	2 31	0 77	084
69 4	541824	16403	2096	16403	64 13	6 17	1 25	160
69 5	371178	84180	68336	3540	44 30	1 57	1 30	066
69 6	4142737	563478	8827	563478	36 66	9 6	5 0	079
69 7	132231	18571	12428	18571	24 95	1 39	3 04	225
69 8	3353356	5253	6430	5253	21 24	1 87	1 72	084
69 9	374768	113137	6403	113137	48 80	1 15	1 41	080
69 10	332428	172904	12209	172904	26 71	1 67	1 42	098
69 11	193224	51443	15591	15591	11 14	7 5	5 4	142
69 12	242513	122457	56458	122457	12 34	6 4	2 53	113
70 1	242513	931187	1507838	82150	31 90	1 27	1 05	112
70 2	242513	931187	1507838	82150	31 90	1 27	2 05	112
70 3	1081621	119749	34791	7322	27 92	3 06	0 89	187
70 4	148822	45739	40605	2656	32 14	9 7	8 8	057
70 5	2120745	112631	80024	6513	15 26	8 1	5 8	047
70 6	26502	21935	21935	21935	4 26	4 6	4 5	048
70 7	2156084	50179	47114	3698	79 17	1 84	1 73	143
70 8	3329219	73625	648774	8564	37 67	8 3	7 35	100
70 9	3103478	84995	205608	14493	44 67	1 22	2 92	209
70 10	1104673	72363	93831	4946	20 72	1 36	1 79	093
70 11	2307251	70944	77544	4814	41 88	1 76	1 41	087
70 12	1201810	70944	93221	7014	22 14	1 31	1 72	129
71 1	274502	0	1702	623	0 00	0 00	0 41	150
71 2	18382621	133435	108449	2785	0 00	52 74	6 80	1 101
71 3	1281607	54400	12796	1278	240 98	10 33	2 11	240
71 4	43158	74009	1456	1456	110 34	10 23	2 4	240
71 5	146122	26227	1820	1820	17 85	2 73	0 73	390
71 6	1514932	122666	2843	2843	226 48	41 61	5 37	860
71 7	3343760	52598	33201	2661	278 13	23 54	3 31	509
71 8	2375791	72847	291378	6004	89 07	3 98	1 35	121
71 9	5461913	85951	159900	11344	81 84	2 41	5 82	116
71 10	1633588	92385	92385	92385	41 84	1 37	2 81	199
71 11	1633588	92385	92385	92385	41 84	1 37	2 81	199
71 12	20575086	118702	45865	118702	49 69	1 11	1 44	080
72 1	1182953	4997	23676	4997	56 57	1 97	1 80	102
72 2	770995	44997	1833	1833	42 21	1 88	1 88	077
72 3	866445	124951	35444	3146	46 91	6 77	1 92	170
72 4	855161	89127	42495	3065	17 58	1 83	0 63	063
72 5	3201449	81569	142921	5963	16 92	6 3	1 10	046
72 6	2906333	67126	173962	16507	17 42	4 0	8 25	099
72 7	1198706	83205	188761	13966	18 04	1 24	2 94	210
72 8	748807	68028	119586	6011	11 43	1 04	1 83	092
72 9	508084	59604	61337	3919	13 28	1 56	1 60	100
72 10	1112395	64654	38552	3221	52 88	3 07	1 84	153
72 11	484173	70849	21725	5374	15 09	2 20	5 87	182
72 12	154296	154296	78576	3187	8 11	50 52	1 67	167
73 1	13992353	914308	2130731	72591	19 55	1 38	2 21	1 38

73 1	2208327	104731	38359	3155	104.60	4.96	1.72	150
73 2	1395205	53971	17208	1498	892.76	4.25	1.35	118
73 3	1044621	89234	22383	2260	83.02	7.26	1.82	184
73 4	1044621	89234	22383	2260	83.02	7.26	1.82	184
73 5	443311	17916	10362	1601	113.52	18.41	2.65	402
73 6	1194128	52752	24338	1601	90.52	4.00	1.84	121
73 7	3542335	131139	393553	7362	60.46	2.24	6.72	156
73 8	2936461	97384	36043	2480	23.62	2.90	2.90	201
73 9	2691778	91852	162076	9311	28.05	.96	1.69	082
73 10	1541913	64312	157718	9120	21.78	1.50	1.38	072
73 11	843778	70477	41254	4765	31.22	2.61	.76	176
73 12	1186312	83239	74055	4126	38.13	2.68	2.38	133
	21781728	974588	1454008	79604	35.13	1.57	2.35	128
74 1	1700590	75310	59280	10677	21.22	.94	.74	133
74 2	53109	51420	16715	1639	3.21	3.10	1.01	100
74 3	63354	93109	19156	2153	74.62	10.97	2.26	254
74 4	437422	36328	6082	787	252.67	20.98	3.51	454
74 5	1457846	80586	16336	1816	275.08	15.15	3.08	343
74 6	3821542	99951	27256	3444	83.26	2.18	6.04	119
74 7	4708238	100152	50726	13789	55.72	1.19	2.40	163
74 8	1463665	60570	156194	7366	16.81	1.70	1.79	085
74 9	3789195	100258	108494	6309	51.74	1.37	1.48	085
74 10	659161	34392	127766	8784	8.68	.45	1.68	116
74 11	1031872	123399	38916	8784	28.37	3.39	1.07	172
74 12	427793	44863	93756	4667	11.42	1.50	2.56	119
	20182974	900048	1124674	69496	36.51	1.63	2.03	126
75 1	0	34398	8504	2154	0.00	3.39	.84	.212
75 2	0	26359	4464	627	0.00	1.87	0.21	.221
75 3	330223	30492	14905	2665	126.04	11.64	5.89	1.017
75 4	53118	48801	5021	2865	86.10	79.10	8.14	1.575
75 5	173793	104409	37948	2867	82.51	4.96	1.80	1.137
75 6	0	0	0	0	1	1	1	1
75 7	0	0	0	0	1	1	1	1
75 8	0	0	0	0	1	1	1	1
75 9	0	0	0	0	1	1	1	1
75 10	0	0	0	0	1	1	1	1
75 11	0	0	0	0	1	1	1	1
75 12	0	0	0	0	1	1	1	1
	2121276	244459	70842	9306	56.90	6.56	1.90	250

AJYBFD. 23.53.31. 77/02/15.

\*\*\*\*\*  
 THIS IS D I S P O S E D OUTPUT.  
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IT WILL NOT HAVE A CARD DECK.

EXHIBIT 7.5: Discharges, Nutrient Loadings and Concentrations for An  
Alternate of Backpumping C-51 and L-8 Using 1973-74  
Land Uses and Planned Scenario.

L-8 Basin Available Backpumped Quantities and Nutrient Loadings

Date	Historical M-Canal Demands (Ac-Ft)	Historical L-8 Discharges (Ac-Ft)	Historical L-8 Basin Dis. (Ac-Ft)	Future M-Canal Demands (Ac-Ft)	Future Available L-8 Dis. (Ac-Ft)	Total Nitrogen (lbs)	Total Phosphorus (lbs)	
1/63	None	9388	Same	10800	0	0	0	
2		10050	as	10900	0	0	0	
3		12309	L-8	10400	1909	7938	280	
4		11423	Discharges	10100	1323	5501	194	
5		8918	}	10600	0	0	0	
6		12383		9700	2683	12104	438	
7		7414		8700	0	0	0	
8		7075		9600	0	0	0	
9		6514		9400	0	0	0	
10		9400		8200	1200	4631	114	
11		2291		8900	0	0	0	
12/63		3205		10400	0	0	0	
1/64	None	17821			9400	8421	35016	1236
2		12783			9200	3583	14899	526
3		7646			10050	0	0	0
4		5867			9600	0	0	0
5		6549		9200	0	0	0	
6		9150		9500	0	0	0	
7		8707		9400	0	0	0	
8		17950		8050	9900	45740	2556	
9		19940		8500	11440	44150	1306	
10		23700		8500	15200	58660	1446	
11		22620		8400	14220	59130	2248	
12/64		21836		8600	13236	55038	1943	
1/65	36	17574	17610	10200	7410	30812	1087	
2	48	12165	12213	10700	1513	6291	222	
3	1872	13619	15491	10400	5091	21169	747	
4	1770	5821	7591	10200	0	0	0	
5	5424	4820	10244	10400	0	0	0	
6	8472	8590	17062	10500	6562	29605	1070*	
7	5118	9802	14920	8100	6826	26900	557	
8	2292	11782	14074	0	14074	65025	3634	
9	1938	10802	12720	8200	4520	17440	516	
10	0	30382	30382	9100	21283	82136	2025	
11	12	27582	27594	7100	20482	85168	3006	
12	1926	15656	17582	8200	9382	39012	1377	

Date	Historical M-Canal Demands (Ac-Ft)	Historical L-8 Discharges (Ac-Ft)	Historical L-8 Basin Dis. (Ac-Ft)	Future M-Canal Demands (Ac-Ft)	Future Available L-8 Dis. (Ac-Ft)	Total Nitrogen (lbs)	Total Phosphorus (lbs)
1/66	12	19918	19930	10700	9230	38380	1355
2	0	22417	Same	9500	12917	53711	1896
3	0	21031	as	8850	12181	50651	1788
4	0	7613	L-8	9900	2287	9510	336
5	0	10435	Discharges	9700	735	3056	108
6	0	37773	↓	8650	29123	131389	4749
7	0	41427		7000	34627	136457	2823*
8	0	40717		6900	33817	156242	8731
9	0	42982		7500	35402	136625	4041
10	0	26628	↓	6900	9928	38315	944
11	1920	5355	7275	8450	0	0	0
12	0	8795	8795	10300	0	0	0
1/67	1446	8563	10009	10700	0	0	0
2	7776	4903	12679	10100	1979	8229	290
3	6696	6936	13632	10200	3432	14271	504
4	7824	2737	10561	10200	361	1501	53
5	9528	7888	17416	11000	6416	26679	942
6	6966	7367	14333	11200	3133	14135	511
7	1956	13317	15273	8600	6473	25312	523
8	0	12502	12502	0	12502	57762	2088
9	24	7503	7527	8100	0	0	0
10	12	12823	12835	8900	3935	15186	374
11	426	2870	3296	8500	0	0	0
12/67	6606	4735	11341	9900	1441	5992	211
1/68	3834	5820	9654	10600	0	0	0
2	7752	6881	14633	10400	4233	17602	621
3	5520	3423	8943	10400	0	0	0
4	9186	7139	16325	9800	6525	27132	958
5	6840	6450	13290	10300	2990	12433	439
6	0	51447	51447	9100	42583	191049	6905
7	42	48541	48583	0	48583	191455	3961
8	846	14067	14913	0	14913	68901	3850
9	792	10754	11546	8200	3346	12913	382
10	156	33537	33693	9100	24593	94910	2807
11	990	11948	12938	9100	3838	15959	563
12/68	1986	4473	6459	9700	0	0	0*



(Continued)

Date	Historical M-Canal Demands (Ac-Ft)	Historical L-8 Discharges (Ac-Ft)	Historical L-8 Basin Dis. (Ac-Ft)	Future M-Canal Demands (Ac-Ft)	Future Available L-8 Dis. (Ac-Ft)	Total Nitrogen (lbs)	Total Phosphorus (lbs)
1/69	5448	2085	Calculation	Same	Same	8670	306
2	7194	4514	not	as	as	18770	662
3	3906	20930	necessary	Historical	Histor.	87031	3072
4	5412	4993		Demands	Discharges	20783	734
5	1530	5334				22180	783
6	6882	16431				74129	2679
7	4842	6373				25115	520
8	456	10600				48974	2737
9	1740	10223				39453	1167
10	36	41810				161355	3977
11	36	27106				112712	3978
12/69	36	19228				79954	2822
1/70	2808	14509				60331	2129
2	3978	16467				68473	2417
3	4236	43916				182611	6445
4	282	38541				160261	5656
5	6624	17484				72702	2566
6	0	30914				139469	5041
7	7920	20763				81822	1693
8	7692	25866				119507	6678
9	8886	31595				121933	3606
10	7632	16792				64804	1917
11	7806	607				2524	89
12	11418	1704				7086	250
1/71	8556	1042				4331	153
2	7656	10				42	2
3	9552	5963				24799	875
4	5526	3362				13980	493
5	9654	318				1322	47
6	7194	250				1128	41
7	3720	887				3499	72
8	8124	137				633	35
9	1044	12264				47329	1440
10	7488	819				3261	80
11	5550	4130				17171	606
12/71	6468	845				3514	124

Date	Historical M-Canal Demands (Ac-Ft)	Historical L-8 Discharges (Ac-Ft)	Historical L-8 Basin Dis. (Ac-Ft)	Future M-Canal Demands (Ac-Ft)	Future Available L-8 Dis. (Ac-Ft)	Total Nitrogen (lbs)	Total Phosphorus (lbs)
1/72		54	Calculation	Same	Same	225	8
2	7428	238	not	as	as	990	35
3	5894	224	necessary	Histor.	Histor.	931	33
4	7074	932		Demands	L-8	3875	137
5	2160	5617			Discharge	23357	824
6	0	9551				43089	1557
7	2880	6839				26951	558
8	3326	1113				5142	287
9	3168	958				3697	109
10	8772	280				1079	32
11	7554	2				8	0
12/72	7116	58				241	9
1/73	7656	44				181	6
2	4350	0				0	0
3	3114	0				0	0
4	4890	0				0	0
5	8556	0				0	0
6	4794	236				1065	38
7	5034	9578				37745	1425
8	5472	7113				32864	1836
9	1008	7712				29761	880
10	468	5455				21050	519
11	2940	0				0	0
12/73	8160	224				931	33
1/74	6318	1004				4173	147
2	4908	363				1509	53
3	9258	91				379	13
4	7020	0				0	0
5	5088	0				0	0
6	9192	1527				6889	249
7	6972	11903				46907	970
8	7758	10790				49852	2786
9	7494	2123				8191	242
10	7152	5381				20767	512
11	6156	1337				5560	196
12/74	9624	26				108	4

Figure 21 1973-4 Land Uses West Palm Beach Backpumping Alternative  
West C-51 Plus L-8 Basins.

Date	Discharge (Ac-Ft)	TOTAL NITROGEN Loading (lbs)	Concentrations (mg/l)	TOTAL PHOSPHORUS Loading (lbs)	Concentrations (mg/l)
1/63	3469	8268	0.88	1599	0.170
2	7053	14414	0.75	880	0.046
3	8018	21799	1.00	1263	0.058
4	1870	6096	1.20	253	0.050
5	12599	39971	1.17	1801	0.053
6	9992	108573	4.00	2008	0.074
7	2999	16610	2.04	1023	0.125
8	5496	20100	1.35	1003	0.067
9	25718	101170	1.45	4776	0.068
10	26725	126587	1.74	8374	0.115
11	10034	17751	0.65	4056	0.149
12	8864	38717	1.61	1780	0.074
1/64	22276	59493	0.98	6678	0.110
2	14994	43637	1.07	2023	0.050
3	4350	17814	1.51	940	0.080
4	4709	20184	1.58	946	0.074
5	9804	35045	1.31	1346	0.050
6	19456	189124	3.58	3391	0.064
7	11627	102997	3.26	7120	0.225
8	22773	91773	1.48	4577	0.074
9	34829	141534	1.50	6120	0.065
10	38147	140256	1.35	6217	0.060
11	33410	84889	0.93	9574	0.105
12	24466	131192	1.97	5139	0.077
1/65	11702	40855	1.28	3100	0.097
2	6259	22134	1.30	1028	0.060
3	5091	21169	1.53	747	0.054
4	0	0	-	0	-
5	0	0	-	0	-
6	18522**	88669	1.76	3554	0.071**
7	39145	263053	2.47	16083	0.151
8	33704	163517	1.79	7880	0.086
9	15534	60093	1.42	2597	0.062
10	76340	293362	1.41	15589	0.075
11	63204	132895	0.77	20295	0.118
12/65	15396	85263	2.04	3538	0.085

(Continued)

Date	Discharge (Ac-Ft)	TOTAL NITROGEN		TOTAL PHOSPHORUS	
		Loading (lbs)	Concentrations (mg/l)	Loading (lbs)	Concentrations (mg/l)
1/66	27339	68634	0.92	6372	0.086
2	32988	92551	1.03	3999	0.045
3	24048	67658	1.04	3382	0.052
4	7097	18709	0.97	809	0.042
5	10755	28068	0.96	1188	0.041
6	65557	718489	4.03	12116	0.068
7	79245**	536380	2.49	30592	0.142**
8	69948	293733	1.55	14592	0.077
9	53305	189971	1.31	6580	0.045
10	34160	144982	1.56	8097	0.087
11	6577	11056	0.62	2884	0.161
12/66	3582	23195	2.38	1049	0.108
1/67	4360	11534	0.97	2036	0.172
2	7366	29742	1.49	1301	0.065
3	4908	21508	1.61	1030	0.077
4	361	1501	1.53	53	0.054
5	6585	33793	1.89	1474	0.082
6	19358	177688	3.38	3692	0.070
7	26855	117412	1.61	6212	0.085
8	23026	107384	1.72	4339	0.069
9	14162	54572	1.42	2563	0.067
10	43991	191587	1.60	12754	0.107
11	11770	17759	0.56	4891	0.153
12/67	7261	43155	2.19	2092	0.106
1/68	1708	6628	1.43	705	0.152
2	8053	43612	1.99	1917	0.088
3	4798	22501	1.73	1032	0.079
4	6608	30658	1.71	1229	0.068
5	23818	86863	1.34	3290	0.051
6	132712	2159063	5.99	29825	0.083
7	100332	611269	2.24	33005	0.121
8	37882	179336	1.74	8599	0.084
9	26971	107724	1.47	5030	0.069
10	69023	297536	1.59	16279	0.087
11	18000	37719	0.77	5376	0.110
12/68	2239**	16369	2.69	657	0.108**

(Continued)

Date	Discharge (Ac-Ft)	TOTAL NITROGEN Loading (lbs)	Concentrations (mg/l)	TOTAL PHOSPHORUS Loading (lbs)	Concentrations (mg/l)
1/69	9985	28327	1.04	3415	0.126
2	7856	31102	1.46	1396	0.065
3	33832	110367	1.20	4698	0.051
4	9659	30788	1.17	1531	0.058
5	20823	62875	1.11	2362	0.042
6	47665	399477	3.08	7298	0.056
7	24440	174859	2.63	10974	0.165
8	33569	154609	1.69	7273	0.080
9	35024	127102	1.34	5426	0.057
10	83856	318891	1.40	14202	0.062
11	60444	152451	0.93	15859	0.097
12/69	35080	190077	1.99	7303	0.077
1/70	25989	85270	1.21	6787	0.096
2	31892	104106	1.20	4322	0.050
3	89462	255310	1.05	11236	0.046
4	54871	179205	1.20	7481	0.050
5	24561	109031	1.63	4294	0.064
6	58740	697910	4.37	12062	0.076
7	41712	248487	2.19	12952	0.114
8	43553	204308	1.73	10344	0.087
9	46100	176874	1.41	6258	0.050
10	33971	145045	1.57	7265	0.079
11	2660	4812	0.67	926	0.128
12/70	1898	14065	2.73	771	0.149
1/71	1712	8394	1.80	354	0.076
2	282	4081	5.32	286	0.373
3	5963	24799	1.53	875	0.054
4	3388	14271	1.55	510	0.055
5	3448	22502	2.40	952	0.102
6	11482	123265	3.95	2833	0.091
7	16187	123230	2.80	7866	0.178
8	11982	57561	1.77	2550	0.078
9	31884	121337	1.40	4988	0.058
10	10322	38023	1.36	2145	0.076
11	37897	65412	0.64	10639	0.103
12/71	11006	66683	2.23	2886	0.096

(Continued)

Date	Discharge (Ac-Ft)	TOTAL NITROGEN		TOTAL PHOSPHORUS	
		Loading (lbs)	Concentrations (mg/l)	Loading (lbs)	Concentrations (mg/l)
1/72	9152	19548	0.79	3689	0.143
2	6857	17797	0.95	985	0.053
3	2971	15860	1.96	749	0.093
4	13013	38781	1.10	1715	0.048
5	48754	156094	1.18	5530	0.042
6	66905	1363338	7.50	16691	0.092
7	28806	200844	2.57	12536	0.160
8	19777	99936	1.86	4392	0.082
9	13224	56240	1.56	2744	0.076
10	6937	34076	1.81	2153	0.114
11	10451	16851	0.59	4372	0.154
12/72	5955	41133	2.54	1807	0.112
1/73	4225	15677	1.37	758	0.066
2	2908	10303	1.30	536	0.068
3	2410	12345	1.88	674	0.103
4	1303	6753	1.91	489	0.138
5	4026	20845	1.91	892	0.082
6	16969	291832	6.33	4725	0.102
7	50570	363053	2.64	23267	0.169
8	36716	168365	1.69	7632	0.076
9	49331	186296	1.39	8465	0.063
10	35305	159030	1.66	9753	0.102
11	9366	15871	0.62	3591	0.141
12/73	9370	54044	2.12	2324	0.091
1/74	29419	51079	0.64	9470	0.118
2	5712	15618	1.01	919	0.059
3	2045	6723	1.21	404	0.073
4	52	314	2.22	22	0.157
5	26	118	1.66	7	0.105
6	12993	145302	4.11	2436	0.069
7	34649	170027	1.81	8894	0.094
8	38658	184326	1.75	8527	0.081
9	23820	89207	1.38	4201	0.065
10	31432	137974	1.62	8334	0.098
11	13014	37660	1.06	4353	0.123
12/74	13153	91919	2.57	3770	0.105

Plan Scenario Land Uses West Palm Beach Backpumping  
Alternative West C-51 Plus L-8 Basins

Date	Discharge (Ac-Ft)	TOTAL NITROGEN Loading (lbs)	Concentrations (mg/l)	TOTAL PHOSPHORUS Loading (lbs)	Concentrations (mg/l)
1/63	4073	10819	0.98	2578	0.233
2	9990	27152	1.00	2632	0.097
3	9192	27455	1.10	2509	0.100
4	1323	5501	1.53	194	0.054
5	16794	74212	1.63	5026	0.110
6	13629	192409	5.19	4119	0.111
7	4400	29365	2.46	2337	0.195
8	11083	51760	1.72	3547	0.118
9	29603	117218	1.46	6467	0.080
10	30108	142452	1.74	9974	0.121
11	11261	22462	0.73	5375	0.176
12/63	13184	64761	1.81	4854	0.135
1/64	24713	65274	0.97	8240	0.123
2	16980	51491	1.12	3274	0.071
3	6921	23705	1.26	2259	0.120
4	9382	32188	1.26	2766	0.108
5	10440	37641	1.33	2189	0.077
6	25264	312101	4.55	5683	0.083
7	15009	129814	3.18	9757	0.239
8	29082	119764	1.52	6771	0.086
9	39177	159120	1.49	7854	0.074
10	42912	167176	1.43	8785	0.075
11	34904	89412	0.94	11004	0.116
12/64	27050	148741	2.02	6715	0.091
1/65	12251	42889	1.29	4029	0.121
2	7861	30419	1.42	2513	0.118
3	6886	28897	1.54	1874	0.100
4	1934	13886	2.64	1366	0.260
5	233	2250	3.55	282	0.445
6	27773*	156142	2.07	5908	0.078
7	44410	293381	2.43	19230	0.159
8	37180	179332	1.77	9390	0.093
9	19416	76193	1.44	4312	0.102
10	80691	315271	1.44	17733	0.081
11	67360	137639	0.75	21993	0.120
12/65	16804	101721	2.23	6084	0.133

(Continued)

Date	Discharge (Ac-Ft)	TOTAL NITROGEN Loading (lbs)	Concentrations (mg/l)	TOTAL PHOSPHORUS Loading (lbs)	Concentrations (mg/l)
1/66	31970	94744	1.09	9370	0.108
2	34108	103843	1.12	5217	0.056
3	27164	73564	1.00	4693	0.064
4	10996	34509	1.15	2512	0.084
5	14648	43367	1.09	2748	0.069
6	74105	903926	4.49	15267	0.076
7	85262*	585099	2.52	34796	0.150**
8	75068	316086	1.55	16430	0.081
9	58681	205996	1.29	7944	0.050
10	37005	155798	1.55	9694	0.096
11	8102	16080	0.73	4384	0.199
12/66	5086	35746	2.59	2314	0.167
1/67	4683	15981	1.26	3419	0.269
2	10552	44883	1.57	2899	0.101
3	5826	26417	1.67	2318	0.146
4	361	1501	1.53	53	0.054
5	6416	26679	1.53	942	0.054
6	27040	359049	4.89	8190	0.111
7	32401	162557	1.85	9663	0.110
8	25524	121016	1.74	6118	0.088
9	18755	72217	1.42	4425	0.087
10	49638	226218	1.68	15008	0.111
11	12685	20832	0.60	5960	0.173
12/67	8992	62679	2.56	3989	0.163
1/68	1725	8298	1.77	1131	0.241
2	11145	52756	1.74	3832	0.127
3	6973	25919	1.37	1861	0.098
4	6819	33832	1.83	2188	0.118
5	29420	116738	1.46	5450	0.068
6	137670	2236435	5.98	31803	0.085
7	104003	632248	2.24	35354	0.125
8	40941	190781	1.71	10013	0.090
9	31018	124871	1.48	6776	0.080
10	71975	315826	1.61	18017	0.092
11	18565	41513	0.82	6107	0.121
12/68	1999*	14614	2.69	587	0.108**



Date	Discharge (Ac-Ft)	TOTAL NITROGEN Loading (lbs)	Concentrations (mg/l)	TOTAL PHOSPHORUS Loading (lbs)	Concentrations (mg/l)
1/69	10328	40781	1.45	5634	0.201
2	9304	43386	1.72	3189	0.126
3	37305	129794	1.28	6789	0.067
4	9828	37186	1.39	2830	0.106
5	25034	91716	1.35	4323	0.064
6	57611	637607	4.07	11506	0.073
7	26726	193486	2.66	12948	0.178
8	37523	174593	1.71	8867	0.087
9	39723	152590	1.41	7570	0.070
10	87829	339259	1.42	16186	0.068
11	62226	164155	0.97	17569	0.104
12/69	36664	202411	2.03	8177	0.082
1/70	28896	95122	1.21	9451	0.120
2	33505	109078	1.20	5073	0.056
3	95065	262635	1.02	12858	0.050
4	56230	181797	1.19	7943	0.052
5	27505	119816	1.60	6464	0.086
6	63436	789243	4.58	13905	0.081
7	46328	284430	2.26	16186	0.129
8	45486	214838	1.74	11624	0.094
9	51867	199477	1.42	8420	0.060
10	36769	158025	1.58	8931	0.089
11	2134	4226	0.73	712	0.123
12/70	2635	24281	3.39	3035	0.424
1/71	2998	17127	2.10	1431	0.176
2	1513	11212	2.73	1596	0.388
3	6225	28620	1.69	1487	0.088
4	5295	34523	2.40	3167	0.220
5	6576	34523	1.93	2108	0.118
6	19324	292506	5.57	6045	0.115
7	21815	163399	2.76	11416	0.193
8	16151	79038	1.80	4455	0.101
9	35779	139098	1.43	6533	0.067
10	15716	63960	1.50	4804	0.112
11	39512	67458	0.63	11172	0.104
12/71	12246	80930	2.43	4883	0.147

(Continued)

Date	Discharge (Ac-Ft)	TOTAL NITROGEN		TOTAL PHOSPHORUS	
		Loading (lbs)	Concentrations (mg/l)	Loading (lbs)	Concentrations (mg/l)
1/72	12599	29869	0.87	6008	0.175
2	9045	24666	1.00	1868	0.076
3	7034	36375	1.90	3179	0.166
4	18833	46370	0.91	3202	0.063
5	53486	166278	1.14	6787	0.047
6	70953	1419051	7.36	18064	0.094
7	31294	215712	2.54	14524	0.171
8	25217	124728	1.82	6298	0.092
9	15060	65034	1.59	3927	0.096
10	8050	39731	1.82	3253	0.149
11	11853	21733	0.67	5874	0.182
12/72	7060	50768	2.65	3428	0.179
1/73	7812	36540	1.72	3162	0.149
2	4677	17208	1.35	1498	0.118
3	4521	22383	1.82	2260	0.184
4	1437	10367	2.65	1571	0.402
5	4854	24338	1.84	1601	0.121
6	21794	394618	6.66	7400	0.125
7	55325	398188	2.65	26405	0.176
8	42418	194940	1.69	9747	0.085
9	54239	204643	1.39	10000	0.068
10	39804	178768	1.65	11773	0.109
11	9943	20626	0.76	4765	0.176
12/73	11672	74986	2.36	4159	0.131
1/74	30489	63453	0.77	10824	0.131
2	6460	18224	1.04	1712	0.098
3	3215	19535	2.24	2166	0.248
4	637	6082	3.51	787	0.455
5	1950	16336	3.08	1818	0.343
6	18416	284145	5.68	5693	0.114
7	42994	249628	2.14	14759	0.126
8	42834	206048	1.77	10152	0.087
9	29062	116685	1.48	6551	0.083
10	33336	148533	1.64	9296	0.103
11	14721	33376	1.11	6463	0.162
12/74	13814	95864	2.55	4451	0.119

Exhibit 7.6: Input Set For C-4 Basin



C-AMEST 72	25482	17530	25068	13633			DISH	5836	18211
C-AMEST 73	12492	9674	4396	3848				5836	18211
B-AMEST 73	12492	9674	4396	3848			DISH		
C-AMEST 74	20494	13520	11941	11941				5740	14464
C-AMEST 74	11935	8291	5936	4965			DISH		
C-AMEST 74	22150	18332	14339	15840				0	0
C-AMEST 75	8150	5890	4950	7060			DISH	0	0
C-AMEST 75	0	0	0	0					

C-AMEST							ONPSCSS		
C-AMEST							ONPSCBDD	0.96	1.91
C-AMEST							ONPSCN	.034	.012
C-AMEST							ONPSCP		REF
C-AMEST									

RAYORVE 77/02/19 FLORIDA STATE UNIVERSITY #61085

16.12.10 JCF.T550.CH120000.No F0Y  
 16.12.11 ACCOUNT 3364003782\*2.TAPE11  
 16.12.13 TRGET ASSIGNED TO STAGEIN, VSN=\*\*\*51.  
 16.12.14 STAGPRGZ COMPLETE

16.12.24 CALL PRGZ  
 16.12.25 EPP,CARD3  
 16.14.25 COPY COMPLETE.  
 16.14.25 CBR,CARD2  
 16.14.25 COPY COMPLETE.  
 16.14.25 CBR,IP1  
 16.14.25 COPY COMPLETE.  
 16.14.26 CBR,IP2  
 16.14.26 COPY COMPLETE.  
 16.14.26 CBR,IP3  
 16.14.26 COPY COMPLETE.  
 16.14.26 B-STORM,SUMMB  
 16.14.28 CALL (PROGZ(LFN=LAND,NAME=IP1)  
 16.14.28 RP,INPUT  
 16.14.28 ASSIGN,MS-OUTPUT  
 16.14.28 DI00, ASSIGNED TO OUTPUT.  
 16.14.29 STORM(IP1)  
 16.16.17 STOP  
 16.16.17 REMAME,QUAL=TAPE13  
 16.16.17 REMAME,OUT=OUTPUT  
 16.16.17 RP,INPUT  
 16.16.17 SUMB.  
 16.16.17 STOP  
 16.17.15 REMAME,LAN0=QUALSUM  
 16.17.15 DISPOSE,QUAL=PRZEI=9364003.  
 16.17.15 CALL (PROGZ(LFN=SCENAR,NAME=IP2)  
 16.17.16 RP,INPUT  
 16.17.16 ASSIGH,MS OUTPUT  
 16.17.16 DI00, ASSIGNED TO OUTPUT

Exhibit 7.7: CLADM Hydrologic Output for Western C-4 Using  
1973-74 Land Uses and Planned Scenario.







66 7	28369	3671	493	8951	724	632	5173	7228	868	18641
66 8	23362	3701	493	6592	2598	2249	4606	5792	878	14493
66 9	26177	3741	442	7491	4771	4642	4839	6924	777	18338
66 10	36177	5674	355	4912	12701	11033	7377	4124	625	20471
66 11	36117	5744	355	4912	12701	11033	7377	4124	625	20471
66 12	2470	1802	187	2842	-4043	-4639	2470	2723	502	14220
67 1	9934	5234	187	1177	-7828	-8913	334	1106	329	9998
67 2	57382	40683	4033	52045	60557	47933	55504	47060	7097	17162
67 3	9178	1135	237	2898	-2206	-2526	1402	2631	418	8655
67 4	7243	1234	100	1958	-5395	-6232	501	1759	176	8162
67 5	12015	6312	177	2984	2562	2238	236	2468	312	8997
67 6	4978	33	373	316	-5127	-5870	33	364	657	3550
67 7	2640	768	415	1359	993	867	1068	1243	278	5768
67 8	11742	8977	470	8634	32489	28355	11477	6188	826	19446
67 9	18324	2503	493	4670	315	275	371	4739	668	13042
67 10	57375	57375	493	4670	315	275	371	4739	668	13042
67 11	27175	3578	493	7555	10155	8859	506	6673	878	1713
67 12	6145	4572	442	5334	18718	16348	6341	4724	777	8790
67 13	30839	6145	442	5334	18718	16348	6341	4724	777	8790
67 14	42868	1476	355	24665	24665	21541	9378	5071	623	15151
67 15	12716	1736	285	3111	900	796	2436	2759	502	8669
67 16	6653	601	187	1248	-3316	-4036	834	1163	329	7106
67 17	96990	31707	4033	45539	74453	46385	43353	41384	7097	111949
68 1	6408	768	237	2160	-10040	-11496	1101	1907	418	13579
68 2	13688	1235	100	2411	-6954	-7932	1816	2016	176	10115
68 3	2337	11437	177	1459	-10136	-11606	367	1437	312	17394
68 4	4259	567	373	1059	-3675	-4208	834	829	657	8961
68 5	61879	24691	415	8128	28645	25017	13183	8003	729	28130
68 6	74828	48761	470	9241	18156	15837	16121	8750	826	49195
68 7	39113	2603	493	6119	-25199	-28385	3405	8796	868	42715
68 8	20826	3972	499	5855	-6348	-7268	5141	4785	29440	
68 9	27829	3372	499	5855	-6348	-7268	5141	4785	29440	
68 10	27835	3372	499	5855	-6348	-7268	5141	4785	29440	
68 11	37081	32577	442	4736	-694	-795	8110	3937	777	33162
68 12	29070	4038	355	6700	-21565	-24632	5140	4429	655	46708
68 13	4388	434	285	1637	-22887	-23900	367	1720	502	28136
68 14	21039	434	187	434	-17426	-19933	6933	4297	339	19761
68 15	27820	302491	4033	50019	-78223	-102278	56371	43906	7097	22295
69 1	22228	21166	237	3203	-2378	-2723	4339	3660	418	21673
69 2	6442	14832	100	4827	-8557	-9912	1335	468	176	16510
69 3	6608	11978	177	2545	-8092	-9265	1688	3244	312	13317
69 4	15453	13177	373	3631	-688	-788	3004	3178	657	12406
69 5	58115	3922	415	5314	-14378	-15322	5701	5081	23079	
69 6	26830	5494	470	4873	-14378	-15322	5701	5081	23079	
69 7	26866	3738	493	7615	-7491	-8577	5240	8889	868	46558
69 8	28303	37384	493	7615	-7491	-8577	5240	8889	868	29123
69 9	14385	1535	499	5638	-22445	-21518	2270	3435	878	34455
69 10	27592	3892	442	6075	-4864	-5569	5732	5951	777	26432
69 11	31742	7142	355	5733	7431	6490	9812	5191	635	32885
69 12	33631	1670	285	2447	-33192	-39005	3900	2143	502	38731
69 13	3838	5678	187	168	-18370	-21034	768	701	339	23842
69 14	28669	29816	4033	51491	-115737	-13194	46732	47379	7097	33821
70 1	8811	18651	237	2716	-14648	-1635	1635	2128	418	20313
70 2	5968	14706	100	1474	-11876	-1407	1101	1407	176	16001
70 3	8711	13843	177	2616	-7925	-9074	1635	2028	312	15445
70 4	3147	4473	373	593	-14427	-1635	634	579	637	16363
70 5	56647	17311	415	3768	14553	13710	8173	3330	709	19376
70 6	18457	29660	470	4973	-16046	-13373	3471	4272	836	31332

70 6	18457	20660	2436	470	4973	-16046	-18373	3471	4272	866	31732
70 7	14952	22967	1702	493	5532	-14940	-16076	2370	5268	886	24972
70 8	12015	22834	1402	499	5532	-15075	-17833	2669	3953	777	73917
70 9	29671	32139	4072	442	7136	-10046	-11503	5874	6463	655	29691
70 10	10046	868	355	524	524	-21307	-24337	1362	4721	562	19465
70 11	300	17191	0	285	0	-17176	-19667	0	567	323	15275
70 12	13528	18991	18991	4033	38868	-13715	-15704	0	567	323	15275
71 1	149256	243397	19891	4033	38868	-137042	-160866	28968	37249	7097	268776
71 2	1702	11742	200	237	1594	-10871	-12447	267	611	418	13120
71 3	2670	9057	267	100	1152	-6679	-7647	367	1170	176	16977
71 4	6390	33	33	177	1150	-6392	-6994	67	1062	176	7955
71 5	1335	3854	0	373	0	-3993	-4572	0	657	414	4149
71 6	13784	4473	1936	415	3071	5825	5087	2770	2464	723	5504
71 7	13784	4473	1936	415	3071	5825	5087	2770	2464	723	5504
71 8	13784	4473	1936	415	3071	5825	5087	2770	2464	723	5504
71 9	13784	4473	1936	415	3071	5825	5087	2770	2464	723	5504
71 10	13784	4473	1936	415	3071	5825	5087	2770	2464	723	5504
71 11	13784	4473	1936	415	3071	5825	5087	2770	2464	723	5504
71 12	13784	4473	1936	415	3071	5825	5087	2770	2464	723	5504
72 1	5340	11016	567	237	2200	-8113	-9289	768	2203	418	12008
72 2	9045	1235	100	2211	3931	-1736	-1970	1736	1932	116	19367
72 3	10046	9057	1936	177	1479	-1292	-1292	1760	860	312	19367
72 4	8911	9323	567	373	5771	-6556	-7507	868	5365	637	10396
72 5	45758	23497	7042	415	6784	-15062	-13158	9746	5931	723	59943
72 6	36350	22350	5273	470	7195	-2054	-2054	7333	823	868	21770
72 7	2377	20864	3171	493	6249	-3869	-4361	4472	5920	888	21770
72 8	21661	28966	2804	499	6145	-13849	-15857	4095	5294	878	31946
72 9	16955	25482	2002	442	14941	-16933	-16933	2837	4361	777	27810
72 10	9545	17530	935	355	4374	-12714	-14558	1302	4826	633	19323
72 11	9245	25068	1101	3150	3150	-19458	-2050	1959	502	27959	27959
72 12	13951	13633	1936	187	3238	-3107	-3958	2732	2767	323	14413
73 1	210634	216451	28070	4033	55222	-62372	-77638	40032	46962	7097	234213
73 2	113381	12492	1702	237	1961	-3309	-3789	1870	1870	418	12492
73 3	7376	9674	868	100	2574	-4972	-5693	1235	2239	176	16977
73 4	5874	8011	734	177	1810	-4124	-4722	1039	1846	312	8038
73 5	376	8011	734	177	1810	-4124	-4722	1039	1846	312	8038
73 6	376	8011	734	177	1810	-4124	-4722	1039	1846	312	8038
73 7	376	8011	734	177	1810	-4124	-4722	1039	1846	312	8038
73 8	376	8011	734	177	1810	-4124	-4722	1039	1846	312	8038
73 9	376	8011	734	177	1810	-4124	-4722	1039	1846	312	8038
73 10	376	8011	734	177	1810	-4124	-4722	1039	1846	312	8038
73 11	376	8011	734	177	1810	-4124	-4722	1039	1846	312	8038
73 12	376	8011	734	177	1810	-4124	-4722	1039	1846	312	8038
74 1	8477	11935	1168	237	2013	-5708	-6536	1692	1931	418	12664
74 2	334	8391	0	100	0	-8037	-9253	0	0	176	9383
74 3	7576	5839	1135	177	1236	-464	-535	1335	1302	312	5557
74 4	7042	5996	935	373	1870	-1197	-1371	1332	1332	657	6033
74 5	8778	4365	848	415	3975	-577	-661	1202	3868	729	4842

74 6	27101	5740	3705	470	5598	14293	12483	5173	5960	826	7032
74 7	20366	24464	4792	499	6809	-3125	-3590	3071	7778	868	15270
74 8	31056	15172	2436	442	7810	1578	1378	6074	6182	878	22568
74 9	15262	18266	1559	353	3601	-5230	-6057	3538	6836	777	19738
74 10	15266	14379	2305	285	2305	-10440	-11954	2203	3280	625	20331
74 11	3955	15940	534	187	950	-1509	-1728	3237	2189	502	14457
74 12	163591	146427	21228	4033	45731	-13072	-14967	734	904	329	17639
						-32650	-41821	25671	41353	7097	156312
75 1	4639	8150	467	337	2053	-5801	-6642	634	2048	418	8815
75 2	3653	8150	467	337	2053	-5801	-6642	634	2048	418	8815
75 3	3084	5890	267	100	1526	-4512	-5166	491	1367	176	6227
75 4	2086	4820	157	177	1112	-4173	-4778	287	345	312	5857
75 5	1768	5617	157	177	1036	-5831	-6699	167	1087	657	6724
75 6	16488	7060	1802	415	6513	2500	2183	2670	5376	729	8000
75 7	0	0	0	492	0	-470	-538	0	0	826	0
75 8	0	0	0	493	0	-493	-571	0	0	878	0
75 9	0	0	0	442	0	-442	-506	0	0	777	0
75 10	0	0	0	355	0	-355	-406	0	0	625	0
75 11	0	0	0	285	0	-285	-326	0	0	502	0
75 12	0	0	0	187	0	-187	-214	0	0	329	0
	27936	32337	2837	4033	12234	-20568	-24229	4139	11023	7097	35723

ALUQUE, 16.24.05. 77/02/19.

\*\*\*\*\*  
 THIS IS D I S P O S E D O U T P U T .  
 THIS IS D I S P O S E D O U T P U T .  
 IT WILL NOT HAVE A CARD DECK.  
 PLEASE PUT OUT FOR USER 9364003  
 \*\*\*\*\*

Exhibit 7.8: CLADM Quality Output for Western C-4 Using  
1973-74 Land Uses.

1973-4 LAND LINES  
WEST PAPUA CAMP RAIN

	TLSS	TLBOD	TLN	TLF	TCSS	TCROD	TCH	TCP
53 1	0	32583	33188	424	0 00	1 62	1 65	0 21
53 2	33497	48462	44550	2371	1 09	1 57	1 44	0 77
53 3	35811	24565	31013	1981	1 47	3 10	1 01	0 81
53 4	35811	24565	31013	1981	1 47	1 01	1 27	0 81
53 5	2803	2407	10412	71	31	27	1 05	0 08
53 6	593141	55881	17701	202	56 45	5 32	1 16	0 19
53 7	599911	28246	33645	951	18 22	1 86	1 02	0 29
53 8	105080	18324	22567	174	9 69	1 69	2 08	0 16
53 9	532682	31770	29686	238	36 83	2 12	1 98	0 16
53 10	1441254	41818	55861	539	33 24	1 96	1 29	0 12
53 11	385808	20096	91076	1064	7 30	1 38	1 72	0 20
53 12	82937	20225	37058	260	4 54	1 12	2 05	0 11
	472554	43205	21994	151	31 82	2 91	1 48	0 10
	4304558	367582	428792	8354	15 22	1 30	1 52	0 30
54 1	29326	7491	32054	389	1 26	3 32	1 38	0 17
54 2	245415	37571	22926	1004	18 72	1 75	1 75	0 77
54 3	45073	41390	13896	1939	1 99	1 26	1 33	0 82
54 4	52473	3788	17527	179	50 43	4 79	1 92	0 20
54 5	52473	3788	17527	179	111 23	4 96	1 69	0 16
54 6	149370	5335	7964	75	111 23	4 96	1 69	0 16
54 7	149370	5335	35984	725	47 44	1 26	1 08	0 23
54 8	149370	5335	37734	404	15 39	1 95	1 85	0 13
54 9	110787	5589	60950	253	43 67	1 37	1 52	0 11
54 10	42462	42462	28354	236	16 66	1 09	1 39	0 15
54 11	318208	2937	38753	422	35 36	1 47	1 41	0 15
54 12	75377	28536	50980	265	8 42	1 02	1 93	0 10
	674552	34866	36459	100	22 09	1 72	1 11	0 03
			37587	5011	26 01	1 34	1 48	0 20
55 1	151562	34662	35551	444	6 79	1 55	1 59	0 20
55 2	37975	27482	32200	3054	10 01	3 59	1 36	0 78
55 3	426385	35082	252	252	17 31	1 22	1 22	0 71
55 4	180259	23061	20192	167	12 39	1 38	1 39	0 11
55 5	685027	43440	13937	166	0 00	1 45	1 50	0 14
55 6	791159	17640	17640	258	77 07	3 81	1 53	0 22
55 7	751189	34700	40638	282	35 03	1 54	1 80	0 12
55 8	519327	25726	40638	282	35 03	1 54	1 80	0 12
55 9	1434571	40583	26809	162	44 36	2 23	1 81	0 15
55 10	2024410	50307	66837	232	63 97	1 81	1 19	0 10
55 11	37294	13369	90576	619	43 26	1 08	1 30	0 13
55 12	31183	19413	33947	362	1 39	3 33	1 99	0 09
	7061228	357270	449417	8385	23 31	1 16	1 30	0 03
56 1	446614	41493	48920	592	12 49	1 25	1 47	0 18
56 2	192425	37216	1256	1256	8 11	1 40	1 33	0 52
56 3	426877	31482	31482	178	17 08	1 28	1 26	0 70
56 4	332246	13127	23728	168	11 60	1 66	1 19	0 08
56 5	822258	43861	30318	283	40 18	2 14	1 48	0 13

66	6	1541336	43202	774	32.05	1.13	90	.016
66	7	568046	89500	574	19.44	.57	1.73	.012
66	8	536056	77040	551	12.40	.38	1.80	.013
66	9	32479	68014	685	15.18	.44	1.34	.013
66	9	771601	68014	685	24.19	.67	1.34	.017
66	10	1206036	32570	75399	8.22	.26	1.56	.003
66	11	306930	22776	839	1.22	.03	1.56	.003
66	12	23609	18374	78	16.55	.88	1.45	.018
		7074714	377361	7860				
67	1	173039	34811	436	7.72	1.72	1.55	.019
67	2	45872	1631	28053	2.33	.82	1.55	.083
67	3	333346	32594	1142	19.43	2.21	1.58	.067
67	4	0	15247	102	0.00	.21	1.38	.067
67	5	142502	39283	1846	18.46	5.09	2.6	.068
67	6	150261	43321	489	47.09	1.45	0.23	.083
67	7	341158	21066	61138	9.62	1.53	1.59	.015
67	8	49483	40449	322	20.40	1.48	1.42	.012
67	9	675598	16141	155	40.45	1.67	1.67	.013
67	10	806640	38557	417	25.98	1.87	1.7	.010
67	11	213308	41272	220	9.32	1.06	1.84	.012
67	11	213308	22836	220	9.32	1.00	1.84	.010
67	12	81128	26734	25155	4.49	1.48	1.39	.066
		4884235	345555	5616	18.53	1.31	1.39	.021
68	1	140720	22508	653	3.68	.59	1.40	.017
68	2	291433	52198	2945	7.93	.83	1.40	.079
68	3	40571	35880	5475	9.21	1.45	1.16	.080
68	4	169111	2856	237	39.65	2.17	1.51	.014
68	5	2660789	539	7522	39.65	.80	1.45	.089
68	6	1977445	44210	3375	15.56	.39	.88	.027
68	7	324655	19583	1259	3.05	.20	1.84	.012
68	8	674037	12853	871	8.71	1.90	1.90	.013
68	9	117276	114520	1014	12.74	.43	1.29	.013
68	10	779341	201480	544	6.98	.23	1.70	.050
68	11	64033	10643	571	0.00	.06	1.34	.089
68	12	824997	327731	16615	10.04	.41	1.17	.001
		824997	327731	16615	10.04	.41	1.46	.050
69	1	918532	68415	8396	15.97	1.21	1.46	.017
69	2	19574	19574	5056	8.95	.49	1.35	.079
69	3	23959	40841	2546	16.67	.79	1.23	.078
69	4	60970	40385	6097	17.93	.29	1.22	.089
69	5	1113178	56019	563	10.55	.31	1.84	.089
69	6	1288882	36922	3703	10.55	.31	.57	.031
69	7	736941	31840	895	10.05	.22	1.80	.012
69	8	270005	135418	3225	3.25	.22	2.92	.014
69	9	788865	94012	1184	11.23	.56	2.92	.014
69	10	1649566	42899	953	11.23	.50	1.35	.014
69	11	3681	137516	50	18.84	.04	1.97	.018
69	12	121063	186766	783	2.09	.17	1.20	.002
		8048025	1199983	16781	9.92	.48	1.48	.021
70	1	315379	73801	897	6.23	.80	1.46	.018
70	2	240013	59266	3231	6.93	.44	1.36	.081

70 2	24913	17508	54266	3231	6 03	44	1 36	081
70 3	35170	3174	2874	2874	9 35	1 23	1 23	076
70 4	14469	1094	4609	309	3 60	1 14	3 60	068
70 5	168584	6277	6277	501	34 22	1 31	1 29	010
70 6	57684	4773	6774	2540	7 31	31	99	032
70 7	410115	3192	119467	119467	6 57	51	1 91	013
70 8	38492	2701	127317	903	11 44	2 05	2 05	015
70 9	110831	3402	118127	1177	12 69	39	1 35	013
70 10	17451	5402	126453	1499	2 49	1 81	1 81	021
70 11	0	0	90639	374	0 00	0 00	1 94	008
70 12	0	2415	43184	45	0 00	0 07	1 17	001
	308815	394482	986130	15148	8 12	1 49	1 49	023

71 1	37375	49857	52374	666	1 17	1 56	1 64	021
71 2	45062	28745	38003	1873	2 06	1 31	1 54	086
71 3	0	1767	2420	1571	0 00	0 93	1 27	083
71 4	0	0	11522	773	0 00	0 00	0 07	040
71 5	602927	89685	28522	291	49 60	5 73	2 18	054
71 6	602929	89665	28522	291	49 60	5 73	2 18	054
71 7	1714802	50273	33539	621	58 93	6 21	1 15	051
71 8	472036	39475	47673	339	18 48	1 15	1 82	013
71 9	58889	3017	63576	468	17 51	1 96	1 96	014
71 10	1201511	34778	108036	1072	14 95	4 3	1 34	013
71 11	94092	35383	121313	1395	13 13	50	1 73	050
71 12	16656	3559	106043	446	31	07	1 95	008
	582934	45023	79535	205	8 82	71	1 25	003
	6143115	394482	708057	9020	13 61	87	1 57	050

72 1	13709	17800	42328	513	4 13	1 60	1 41	017
72 2	31789	28972	38064	2042	11 98	1 09	1 43	077
72 3	58641	41438	33074	1683	24 23	1 68	1 34	068
72 4	13511	2030	31789	243	5 33	1 25	1 91	010
72 5	1911366	46533	7515	552	29 93	7 3	1 18	009
72 6	1103508	31489	57616	1679	18 17	52	95	028
72 7	74991	32491	103701	693	13 31	63	1 83	012
72 8	74991	32491	103701	693	13 31	63	1 83	012
72 9	74738	34689	156144	1095	19 37	40	1 99	014
72 10	526214	23951	93921	977	7 55	1 37	1 39	014
72 11	39884	1383	87385	1036	6 38	56	1 83	052
72 12	68089	34588	132240	584	4 55	28	1 94	009
	7374539	362113	47462	141	16 41	91	1 28	004
			901149	11239	12 54	62	1 53	019

73 1	486661	28377	47611	562	13 45	83	1 40	017
73 2	237135	24746	37836	2093	9 02	1 44	1 44	080
73 3	29339	28366	1676	1676	9 61	1 30	1 31	077
73 4	347463	2181	19590	169	25 59	2 15	1 44	012
73 5	12997	17394	15167	135	1 24	1 32	1 32	013
73 6	1218319	48282	2030	325	76 81	3 04	1 39	021
73 7	761948	26071	90769	592	15 39	53	1 83	012
73 8	2007616	53479	12811	893	28 62	76	1 83	013
73 9	594972	24503	115440	1171	7 00	30	1 36	014
73 10	594972	24503	115440	1171	7 00	30	1 36	014
73 11	212932	24490	108559	1193	3 82	46	1 81	021
73 12	5746	4298	71864	306	16	1 96	1 96	008
	343791	42294	44831	168	10 59	1 30	1 38	005
	6408820	350471	723232	9284	14 20	1 78	1 60	021

74 1	320370	27832	46423	559	9 88	86	1 44	017
74 2	0	0	29253	1893	0 00	0 00	1 30	084
74 3	353600	46249	24974	1131	23 07	3 02	1 63	074
74 4	299501	29038	22965	191	18 38	1 76	1 41	012
74 5	226980	33840	21959	211	16 82	2 51	1 63	016
74 6	1091584	34067	18843	286	69 97	2 18	1 21	018
74 7	552222	33830	74255	510	14 06	85	1 89	012
74 8	1277034	37399	114200	796	21 24	62	1 90	017
74 9	610799	29779	69005	1702	12 26	60	1 39	014
74 10	377294	21937	1053	1053	7 40	43	1 76	021
74 11	577458	36327	74096	380	14 82	93	1 90	010
74 12	577458	36327	74096	380	14 82	93	1 90	010
74 13	157413	17817	52907	100	3 66	41	1 23	002
74 14	584475	347815	639158	7825	14 89	87	1 61	020

75 1	97632	25432	33666	419	4 41	1 15	1 52	019
75 2	62990	24558	25376	1365	3 93	1 53	1 56	085
75 3	43050	13374	17107	1079	3 22	1 04	1 28	081
75 4	18154	20687	22621	184	1 97	1 22	1 34	011
75 5	307325	46790	30604	282	26 44	2 44	1 57	015
75 6	0	0	0	0	1	1	1	1
75 7	0	0	0	0	1	1	1	1
75 8	0	0	0	0	1	1	1	1
75 9	0	0	0	0	1	1	1	1
75 10	0	0	0	0	1	1	1	1
75 11	0	0	0	0	1	1	1	1
75 12	0	0	0	0	1	1	1	1
75 13	729151	131341	128974	3329	8 32	1 50	1 47	038

AVYQIDX, 02.01.21. 77/02/19.

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 THIS IS D I S P O S E D OUTPUT.  
 IT WILL NOT HAVE A CARD DECK.  
 PLEASE PUT OUT FOR USER 9364003  
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EXHIBIT 7.9: CLADM Quality Output for Western C-4  
Using Planned Scenario.



66 6	2188621	77430	988	34.36	1.22	.72	.015
66 7	489420	63901	87008	9.17	1.20	1.62	.012
66 8	472793	52296	75323	10.55	1.17	1.68	.014
66 9	724953	68078	66487	14.09	1.32	1.52	.014
66 9	724953	68078	66487	14.09	1.32	1.52	.014
66 10	1152064	59060	76431	20.71	1.96	1.37	.016
66 11	286310	53725	47157	7.41	1.39	1.87	.015
66 12	7055106	38402	35877	1.41	1.32	1.52	.009
		781638	8856	15.11	1.67	1.37	.015
67 1	157998	104900	40884	6.72	4.46	1.74	.025
67 2	37849	38885	38885	1.71	1.75	1.71	.027
67 3	306536	98874	129201	16.12	5.20	1.79	.062
67 4	0	3721	117	0.00	.39	1.51	.009
67 5	126731	102971	20562	32.1	13.69	2.73	.012
67 6	1464057	87001	34124	33.78	2.91	1.79	.016
67 7	329944	46616	58193	9.31	1.32	1.84	.012
67 8	473322	89703	46596	16.33	2.94	1.81	.015
67 9	672072	65490	22418	28.13	1.22	1.82	.015
67 10	890313	52142	44188	20.90	1.22	1.82	.015
67 11	205781	41530	53582	8.73	3.27	1.72	.012
67 12	65680	68457	29576	3.40	3.34	1.87	.011
	4732303	810342	416389	15.55	2.86	1.37	.023
68 1	93138	60721	61553	2.20	1.47	1.85	.019
68 2	207153	76266	58583	5.08	1.67	1.44	.079
68 3	22225	34476	41343	7.84	5.2	1.19	.080
68 4	143361	100135	32973	34.97	7.88	1.71	.021
68 5	2473566	77909	609	1.02	1.02	1.01	.000
68 6	2000580	67488	108411	14.96	50	1.61	.020
68 7	297112	45005	211097	2.36	1.62	1.62	.012
68 8	486364	69528	145252	6.08	5.7	1.22	.011
68 9	929504	79926	110211	10.31	8.7	1.52	.013
68 10	678689	52005	210650	5.33	7.4	1.52	.020
68 11	52459	26105	149273	8.4	6.9	1.12	.009
68 12	0	5936	63009	0.00	1.1	1.1	.001
	7286151	295500	1269494	8.32	9.32	1.47	.020
	7866151	18010	1693500	78	1.78	1.43	.020
69 1	786817	167358	89225	13.34	2.84	1.51	.020
69 2	311656	43259	59074	7.16	9.9	1.36	.068
69 3	164822	78641	47789	4.53	2.17	1.32	.080
69 4	332904	74077	383	15.93	2.20	1.24	.010
69 5	1009809	67417	74662	16.10	1.07	1.54	.070
69 6	1180005	64753	117649	9.39	5.2	1.71	.070
69 7	689014	67353	969	8.71	8.5	1.74	.014
69 8	237026	47126	187956	1.32	.80	2.00	.014
69 9	731012	80875	94237	10.21	1.13	1.32	.014
69 10	1373275	72741	132194	17.85	1.47	1.47	.017
69 11	36172	207583	933	1.00	3.4	1.37	.009
69 12	110308	79897	191	1.70	1.23	1.23	.009
	7328448	846897	18317	8.47	.98	1.47	.021
70 1	278710	101027	85319	4.90	1.78	1.50	.020
70 2	230961	41829	60568	3.25	.95	1.38	.081

10 2	41828	60568	3564	5.25	1.38	.681
70 3	23061	53025	3312	7.88	1.80	.077
70 4	13264	51754	377	3.01	1.26	.068
70 5	167869	67706	663	2.39	1.25	.012
70 6	60247	84056	2759	5.83	.97	.032
70 7	324855	74427	129199	4.80	1.00	.015
70 8	323735	63217	1663	4.72	2.04	.015
70 9	1917424	62286	120227	11.94	1.30	.015
70 10	135531	57147	143136	17.42	1.81	.022
70 11	0	0	102629	0.00	1.24	.008
70 12	0	0	49169	0.00	1.18	.001
495990	5086	1097595	55	6.78	1.49	.024
690497	17170	882	74	3.35	1.77	.025
1196116	63019	2195	1.40	3.49	1.73	.020
85018	42648	1830	0.00	1.97	1.34	.085
42630	28994	12404	0.00	0.00	1.10	.007
0	0	79	0.00	0.00	1.00	.007
0	0	12404	0.00	0.00	2.61	.040
91490	39005	591	38.47	6.12	1.61	.040
1563009	90892	37941	41.31	2.40	1.00	.021
423062	65771	46280	16.69	2.60	1.83	.016
479362	66864	533	14.25	1.99	0.87	.016
1105194	60017	107043	13.22	.72	1.28	.013
1123247	73886	1504	10.88	.99	1.68	.020
6197	7517	518	1.10	1.12	1.94	.008
499077	108962	87114	7.34	1.60	1.28	.005
812663	773928	10818	11.19	1.57	1.57	.052
97418	39891	46721	2.99	1.22	1.43	.018
240422	73359	4222	8.80	2.60	1.50	.077
54975	98715	1717	21.70	3.90	1.44	.088
1108542	36859	335	3.91	1.08	1.30	.012
1920854	629	77068	25.83	1.09	1.08	.009
55166	56919	1668	16.67	.86	.89	.026
1020478	55166	1668	16.67	.86	.89	.026
320848	104033	776	10.06	1.28	1.76	.013
389959	8339	1225	6.11	.77	1.93	.014
55507	164636	164636	4.88	1.73	1.36	.013
45309	102962	102962	3.42	1.22	1.85	.023
179173	96711	1200	2.95	1.60	1.93	.009
242311	48309	146787	699	1.92	1.92	.008
569366	59147	50385	241	13.00	1.92	.008
6294746	960758	12369	9.89	1.23	1.51	.013
781138	630	48911	11.12	1.80	1.41	.018
396178	63283	4795	6.32	2.20	1.49	.080
181430	7242	33412	7.54	3.10	1.82	.073
176939	70662	1852	25.24	5.47	1.65	.020
328996	71291	21533	0.00	2.75	1.52	.016
0	17274	180	0.00	4.62	1.26	.024
1105401	103483	28154	49.38	4.62	1.26	.024
694246	48993	90595	13.46	.97	1.76	.012
1889361	91793	125069	25.22	1.23	1.67	.013
1889361	91793	125069	25.22	1.23	1.67	.013
549451	52532	122269	6.01	.58	1.34	.044
169338	61227	112623	1385	2.72	.98	.022
0	10288	361	0.00	1.96	1.96	.009
272899	108443	329	7.74	3.10	1.49	.080
5752219	777072	10724	11.72	1.58	1.58	.022

71 1	26501	882	74	3.35	1.77	.025	
71 2	34241	2195	1.40	3.49	1.73	.020	
71 3	0	1830	0.00	1.97	1.34	.085	
71 4	0	12404	0.00	0.00	1.10	.007	
71 5	0	79	0.00	0.00	1.00	.007	
71 6	475471	39005	591	38.47	6.12	.040	
71 7	1563009	90892	37941	41.31	2.40	.021	
71 8	423062	65771	46280	16.69	2.60	.016	
71 9	479362	66864	533	14.25	1.99	.016	
71 10	1105194	60017	107043	13.22	.72	1.28	.013
71 11	1123247	73886	1504	10.88	.99	1.68	.020
71 12	6197	7517	518	1.10	1.12	1.94	.008
499077	108962	87114	7.34	1.60	1.28	.005	
812663	773928	10818	11.19	1.57	1.57	.052	
97418	39891	46721	2.99	1.22	1.43	.018	
240422	73359	4222	8.80	2.60	1.50	.077	
54975	98715	1717	21.70	3.90	1.44	.088	
1108542	36859	335	3.91	1.08	1.30	.012	
1920854	629	77068	25.83	1.09	1.08	.009	
55166	56919	1668	16.67	.86	.89	.026	
1020478	55166	1668	16.67	.86	.89	.026	
320848	104033	776	10.06	1.28	1.76	.013	
389959	8339	1225	6.11	.77	1.93	.014	
55507	164636	164636	4.88	1.73	1.36	.013	
45309	102962	102962	3.42	1.22	1.85	.023	
179173	96711	1200	2.95	1.60	1.93	.009	
242311	48309	146787	699	1.92	1.92	.008	
569366	59147	50385	241	13.00	1.92	.008	
6294746	960758	12369	9.89	1.23	1.51	.013	
781138	630	48911	11.12	1.80	1.41	.018	
396178	63283	4795	6.32	2.20	1.49	.080	
181430	7242	33412	7.54	3.10	1.82	.073	
176939	70662	1852	25.24	5.47	1.65	.020	
328996	71291	21533	0.00	2.75	1.52	.016	
0	17274	180	0.00	4.62	1.26	.024	
1105401	103483	28154	49.38	4.62	1.26	.024	
694246	48993	90595	13.46	.97	1.76	.012	
1889361	91793	125069	25.22	1.23	1.67	.013	
1889361	91793	125069	25.22	1.23	1.67	.013	
549451	52532	122269	6.01	.58	1.34	.044	
169338	61227	112623	1385	2.72	.98	.022	
0	10288	361	0.00	1.96	1.96	.009	
272899	108443	329	7.74	3.10	1.49	.080	
5752219	777072	10724	11.72	1.58	1.58	.022	

72 1	97418	39891	46721	2.99	1.22	1.43	.018
72 2	240422	73359	4222	8.80	2.60	1.50	.077
72 3	54975	98715	1717	21.70	3.90	1.44	.088
72 4	1108542	36859	335	3.91	1.08	1.30	.012
72 5	1920854	629	77068	25.83	1.09	1.08	.009
72 6	55166	56919	1668	16.67	.86	.89	.026
72 7	1020478	55166	1668	16.67	.86	.89	.026
72 8	320848	104033	776	10.06	1.28	1.76	.013
72 9	389959	8339	1225	6.11	.77	1.93	.014
72 10	55507	164636	164636	4.88	1.73	1.36	.013
72 11	45309	102962	102962	3.42	1.22	1.85	.023
72 12	179173	96711	1200	2.95	1.60	1.93	.009
569366	59147	50385	241	13.00	1.92	.008	
6294746	960758	12369	9.89	1.23	1.51	.013	
781138	630	48911	11.12	1.80	1.41	.018	
396178	63283	4795	6.32	2.20	1.49	.080	
181430	7242	33412	7.54	3.10	1.82	.073	
176939	70662	1852	25.24	5.47	1.65	.020	
328996	71291	21533	0.00	2.75	1.52	.016	
0	17274	180	0.00	4.62	1.26	.024	
1105401	103483	28154	49.38	4.62	1.26	.024	
694246	48993	90595	13.46	.97	1.76	.012	
1889361	91793	125069	25.22	1.23	1.67	.013	
1889361	91793	125069	25.22	1.23	1.67	.013	
549451	52532	122269	6.01	.58	1.34	.044	
169338	61227	112623	1385	2.72	.98	.022	
0	10288	361	0.00	1.96	1.96	.009	
272899	108443	329	7.74	3.10	1.49	.080	
5752219	777072	10724	11.72	1.58	1.58	.022	

73 1	97418	39891	46721	2.99	1.22	1.43	.018
73 2	240422	73359	4222	8.80	2.60	1.50	.077
73 3	54975	98715	1717	21.70	3.90	1.44	.088
73 4	1108542	36859	335	3.91	1.08	1.30	.012
73 5	1920854	629	77068	25.83	1.09	1.08	.009
73 6	55166	56919	1668	16.67	.86	.89	.026
73 7	1020478	55166	1668	16.67	.86	.89	.026
73 8	320848	104033	776	10.06	1.28	1.76	.013
73 9	389959	8339	1225	6.11	.77	1.93	.014
73 10	55507	164636	164636	4.88	1.73	1.36	.013
73 11	45309	102962	102962	3.42	1.22	1.85	.023
73 12	179173	96711	1200	2.95	1.60	1.93	.009
569366	59147	50385	241	13.00	1.92	.008	
6294746	960758	12369	9.89	1.23	1.51	.013	
781138	630	48911	11.12	1.80	1.41	.018	
396178	63283	4795	6.32	2.20	1.49	.080	
181430	7242	33412	7.54	3.10	1.82	.073	
176939	70662	1852	25.24	5.47	1.65	.020	
328996	71291	21533	0.00	2.75	1.52	.016	
0	17274	180	0.00	4.62	1.26	.024	
1105401	103483	28154	49.38	4.62	1.26	.024	
694246	48993	90595	13.46	.97	1.76	.012	
1889361	91793	125069	25.22	1.23	1.67	.013	
1889361	91793	125069	25.22	1.23	1.67	.013	
549451	52532	122269	6.01	.58	1.34	.044	
169338	61227	112623	1385	2.72	.98	.022	
0	10288	361	0.00	1.96	1.96	.009	
272899	108443	329	7.74	3.10	1.49	.080	
5752219	777072	10724	11.72	1.58	1.58	.022	

74 1	97418	39891	46721	2.99	1.22	1.43	.018
74 2	240422	73359	4222	8.80	2.60	1.50	.077
74 3	54975	98715	1717	21.70	3.90	1.44	.088
74 4	1108542	36859	335	3.91	1.08	1.30	.012
74 5	1920854	629	77068	25.83	1.09	1.08	.009
74 6	55166	56919	1668	16.67	.86	.89	.026
74 7	1020478	55166	1668	16.67	.86	.89	.026
74 8	320848	104033	776	10.06	1.28	1.76	.013
74 9	389959	8339	1225	6.11	.77	1.93	.014
74 10	55507	164636	164636	4.88	1.73	1.36	.013
74 11	45309	102962					

74 1	271875	64750	59607	7 90	1 88	1 47	0 19
74 2	35671	118097	33151	0 00	1 30	0 00	0 84
74 3	295175	71215	1196	17 00	7 82	1 96	0 79
74 4	187487	84153	25769	4 34	4 34	1 57	0 17
74 5	1053656	97222	24947	14 25	6 47	1 90	0 24
74 6	48454	7705	470	49 60	2 95	1 05	0 20
74 7	1169708	63222	77076	11 63	1 82	1 82	0 15
74 8	540779	6978	108402	18 07	1 97	1 77	0 13
74 9	338225	46307	72702	12 09	1 64	1 74	0 21
74 10	338225	46307	86218	6 12	1 74	1 74	0 21
74 11	33935	89234	1164	17 74	2 31	1 90	0 12
74 12	145132	42819	486	7 03	1 59	1 59	0 03
74 13	5278260	786213	60957	12 42	1 85	1 59	0 21
74 14			9983				
75 1	8282	6369	38817	3 43	2 66	1 62	0 22
75 2	4389	3521	1860	2 74	3 88	1 72	0 88
75 3	3548	3823	1348	2 02	2 38	1 37	0 83
75 4	3332	49336	2826	29	3 21	1 45	0 14
75 5	446550	126101	477	20 54	5 00	1 74	0 22
75 6	0	0	0	1	1	1	1
75 7	0	0	0	1	1	1	1
75 8	0	0	0	1	1	1	1
75 9	0	0	0	1	1	1	1
75 10	0	0	0	1	1	1	1
75 11	0	0	0	1	1	1	1
75 12	0	0	0	1	1	1	1
75 13	614103	337880	154621	6 33	3 48	1 59	0 42
75 14			4101				

RJVPJAYE. 16.24.06. 77/02/19.

\*\*\*\*\*  
 THIS IS DISPOSED OUTPUT.  
 IT WILL NOT HAVE A CARD DECK.  
 PLEASE PUT OUT FOR USER 9364003  
 \*\*\*\*\*

EXHIBIT 7.10: Input Set for C-14 Basin







ONPSCSS

ONPSCBDD

ONPSCNN

ONPSCNP

REFF

1.24 1.20 1.20 1.20  
 2.26 1.21 2.07 1.28  
 .048 .050 .050 .050  
 .276 .431 .179 .431  
 0.0 0.0 .227 .227

1.24 1.20 1.20 1.20  
 2.26 1.21 2.07 1.28  
 .048 .050 .050 .050  
 .276 .431 .179 .431  
 0.0 0.0 .227 .227

1.24 1.20 1.20 1.20  
 2.26 1.21 2.07 1.28  
 .048 .050 .050 .050  
 .276 .431 .179 .431  
 0.0 0.0 .227 .227

1.24 1.20 1.20 1.20  
 2.26 1.21 2.07 1.28  
 .048 .050 .050 .050  
 .276 .431 .179 .431  
 0.0 0.0 .227 .227

AYBMCL 76/12/04 FLORIDA STATE UNIVERSITY KRONOS

16.50.13	JGF.T550.CM120000.MO. FOY
16.50.13	ACCOUNT.9364003.
16.50.13	STAGE1.R1098.7782/*3.TAPE11.
16.54.36	NTS1.ASSIGNED TO STAGEIN. VSN*****51.
16.54.34	STAGING COMPLETE.
16.54.34	CALL.PROGI.
16.54.35	CBR.CARDS.
16.54.36	COPY COMPLETE.
16.54.36	CBR.CARD2.
16.54.36	COPY COMPLETE.
16.54.36	CBR.IP1.
16.54.36	COPY COMPLETE.
16.54.36	CBR.IP2.
16.54.36	CBR.IP2.
16.54.36	COPY COMPLETE.
16.54.36	CBR.IP3.
16.54.36	COPY COMPLETE.
16.54.36	STORM.SUMMB.
16.54.41	CALL (PROG2(LFN=LAND.NAME=IPI)
16.54.42	KA.INPUT.
16.54.42	ASSIGN.MS.OUTPUT.
16.54.42	D100.ASSIGNED TO OUTPUT.
16.54.43	STORM(IPI)
17.00.33	STOP
17.00.33	RENAME.QUAL=TAPE13.
17.00.33	RENAME.QUAL=PR/EI=9364003.
17.00.33	RENAME.QUAL=PR/EI=9364003.
17.00.33	KA.INPUT.
17.00.34	SUMMB
17.03.01	STOP
17.03.02	RENAME.LAND=QUALSUN.
17.03.02	DISPOSE.QUAL=PR/EI=9364003.
17.03.03	RT.OUTPUT.
17.03.03	CALL (PROG2(LFN=SCENARU.NAME=IP2)
17.03.03	KA.INPUT.
17.03.04	ASSIGN.MS.OUTPUT.
17.03.04	D100.ASSIGNED TO OUTPUT.
17.03.05	STORM(IP2)
17.06.07	STOP
17.06.07	RENAME.QUAL=TAPE13.
17.06.07	RENAME.QUAL=PR/EI=9364003.
17.06.07	KA.INPUT.
17.06.36	SUMMB.
17.08.21	STOP
17.08.22	RENAME.SCENARU=QUALSUN.
17.08.22	DISPOSE.QUAL=PR/EI=9364003.
17.08.23	RT.OUTPUT.
17.08.23	CALL (PROG2(LFN=SCENARU.NAME=IP3)
17.08.23	CALL (PROG2(LFN=SCENARU.NAME=IP3)
17.08.24	KA.INPUT.
17.08.25	ASSIGN.MS.OUTPUT.
17.08.25	D100.ASSIGNED TO OUTPUT.

EXHIBIT 7.11: CLADM Hydrologic Output for Western C-14  
Using 1973-74 Land Uses and Planned Scenario.



16 8	41	15786	216	15131	9149	8483	11411	18899
66 9	53	26158	191	13735	17403	12768	10739	18899
66 9	53	16988	154	13735	17403	12768	10739	18899
66 10	53	49425	7460	15326	17532	11623	5499	1756
66 11	42	9989	124	4772	7769	868	4023	1134
66 11	42	6281	81	4372	7769	868	4023	1134
66 12	43	2380	334	5372	1111	1340	3957	3421
66 12	43	28888	1768	108946	35515	101200	78957	16031
67 1	16099	8303	103	7730	-37	2939	5750	944
67 2	7397	2872	43	4386	3895	3474	3400	397
67 2	18633	4776	77	5280	13714	11988	5611	704
67 3	28847	4743	162	0	-376	0	1484	7065
67 4	182	9204	180	15198	8263	7223	1648	134
67 5	186	15664	207	18292	755	18971	12425	1867
67 6	5882	78224	193	11569	4476	9024	1960	5802
67 7	2782	3273	214	11969	-14224	4476	9024	1960
67 8	5053	5273	214	11969	-14224	4476	9024	1960
67 9	24582	7615	216	15912	7470	6330	9886	10834
67 9	45924	16172	191	15240	17291	15115	10755	11756
67 9	32328	8751	191	15240	17291	15115	10755	11756
67 10	28785	45832	154	9531	-19312	102893	32823	1411
67 10	6978	5910	124	5169	10380	10380	3614	9054
67 11	21682	5062	1603	11890	1040	5271	742	6215
67 12	34660	60587	1748	103419	33136	20599	74552	16031
68 1	8417	2198	193	3187	2929	1670	2537	944
68 2	12762	2872	43	6123	9157	7130	4667	397
68 2	13260	3045	77	4207	7825	3006	2776	704
68 3	8291	330	1002	2089	3533	1269	1543	1484
68 4	1601	1620	180	17454	16005	13990	12953	1648
68 5	49139	16700	180	10512	11469	28586	7151	80276
68 6	106733	22046	203	10512	11469	28586	7151	80276
68 7	140231	49485	214	6886	19619	12148	4741	1960
68 7	44251	19936	216	10586	12013	10501	11553	1984
68 8	85175	37900	191	14429	35655	34663	10557	1756
68 10	43415	87939	154	9162	-32996	-3747	2084	1411
68 11	1403	1603	124	3543	1234	3440	223	1134
68 11	3340	1426	81	1509	1079	179	762	10032
68 12	460246	310080	1748	89687	59761	11289	64866	16031
69 1	11355	6680	193	5245	14693	12844	7949	3496
69 2	11356	5645	43	1418	4280	3741	3006	772
69 2	4079	18571	77	8698	1733	11130	9619	6210
69 3	8016	5314	162	5924	-6594	-6594	1069	423
69 4	7654	3140	180	12425	-9584	-1094	4275	9662
69 5	2416	21695	180	12425	-9584	-1094	4275	9662
69 5	2416	21695	180	12425	-9584	-1094	4275	9662
69 6	92183	44373	203	16984	31609	27630	11957	1867
69 6	53479	29573	214	15782	11936	10434	11337	1960
69 7	22732	32358	216	12334	16070	17834	6546	1984
69 8	22732	32358	216	12334	16070	17834	6546	1984
69 8	67467	12224	191	19511	20442	14963	14781	33061
69 9	32572	30773	154	10682	-20701	-33682	8139	36854
69 10	49980	1603	124	3543	34826	-3983	2138	1134
69 11	9619	534	181	1548	-23369	-9902	735	742
69 12	3340	1748	1748	112994	-16623	-44842	83735	16031
70 1	27988	19365	103	5421	9499	6680	3887	944
70 2	2212	4810	43	3883	3174	2774	2249	397
70 3	64127	52042	177	7118	4890	16833	4855	704
70 3	64127	52042	177	7118	4890	16833	4855	704
70 4	16934	16934	162	10996	-42579	0	1484	11095
70 5	30728	6012	180	7192	6092	5355	6347	6266
70 6	92163	35601	203	15216	31443	20173	11131	17489
70 7	38588	9018	214	6713	-4498	10487	5089	1860
70 8	33466	10863	216	8100	14287	12489	7592	1984
70 9	18570	5611	191	11433	3205	4551	1756	15866
70 10	16032	22931	154	1603	-11809	-19299	2138	8505
70 11	4406	347	124	174	52	45	401	1134
70 12	3407	174	181	2834	366	401	1693	232

71 1	9611	40	1670	103	3681	6395	5890	3204	944	1228
71 2	284	1569	43	4383	4662	4862	4075	1604	397	1879
81 2	9352	284	1569	43	4383	4662	4075	1604	397	1879
71 3	2672	0	134	77	2149	245	730	734	1486	82
71 4	4676	0	668	162	10361	2753	2174	935	1383	0
71 5	36740	5919	6747	180	10361	2753	2174	935	1383	0
71 6	34068	2999	4810	203	13839	1827	13660	6813	10782	1867
71 7	18036	1482	2204	214	9746	19857	29379	29379	13660	2310
71 8	26052	3661	3674	216	11682	1827	6059	4943	8646	6238
71 9	46091	12700	8684	191	11682	1827	14484	10487	9164	20717
71 10	39412	18629	7081	154	11891	5835	7817	18417	9070	21118
71 11	22044	21471	4142	124	3930	5281	5116	4810	5109	1434
71 12	17368	5169	3340	81	4582	5281	6818	4408	3285	4530
266130	76884	44423	1748	92223	81839	92745	81839	55374	16031	99245
72 1	15364	4911	2338	103	6211	4139	3618	3006	4780	944
72 2	15364	4911	2338	103	6211	4139	3618	3006	4780	944
72 3	17368	6627	3340	43	4282	5281	5281	4142	2785	977
72 4	37408	4645	8751	77	3190	2856	2856	10020	704	8759
72 5	18704	11272	2856	162	18903	1827	1827	3540	6238	184
72 6	36072	20892	5144	180	13935	1827	1827	7014	11375	1848
72 7	74815	24967	18188	203	21867	18188	15809	16767	13778	1867
72 8	62123	32670	12024	214	15091	14582	12402	14429	10613	1360
72 9	18704	25433	2071	216	10397	14582	16636	3073	7884	28472
72 10	18036	15372	2271	191	9194	1867	9638	7415	4620	1811
72 11	30228	18233	6146	154	5689	1981	1981	11489	5636	1134
72 12	46091	16120	9933	124	4156	2372	4291	1937	5203	1920
387437	191850	69673	1748	114653	81839	81839	81839	85304	84961	16031
387437	191850	69673	1748	114653	81839	81839	81839	85304	84961	16031
73 1	11356	5996	1670	103	4818	439	384	2204	3594	6434
73 2	19706	3596	3474	43	6107	2980	8724	4409	4182	397
73 3	13360	4149	2338	77	4207	4327	4327	3006	2776	704
73 4	7348	238	601	162	6394	1354	1354	1116	7349	184
73 5	19372	732	2872	203	12585	10353	9032	7241	6200	602
73 6	49765	10693	9552	280	12585	26590	23147	11856	9075	1867
73 7	54775	36847	10795	214	12672	5942	5942	13026	6910	1960
73 8	88175	46640	26653	216	16167	58086	51154	31128	21431	1984
73 9	61455	44364	3808	191	46349	28321	33062	5478	42168	56498
73 10	36072	17387	5878	154	13039	14372	14372	7548	4849	20385
73 11	15364	22945	3006	74	7237	14362	11703	3006	4790	2687
73 12	16032	6272	3096	81	4264	5415	4733	3741	2860	742
16032	6272	3096	81	4264	5415	4733	4733	3741	2860	742
332780	198131	72678	1748	108236	81839	81839	62147	89379	75956	16031
74 1	78957	33160	18937	103	5211	40863	33387	21443	3455	39171
74 2	0	3441	0	43	3484	3286	3286	2806	1477	397
74 3	11356	579	2405	77	1942	8758	1248	2806	1477	704
74 4	4676	502	534	162	2584	1828	1828	7668	4510	1484
74 5	18704	863	2739	180	2792	9679	9679	6800	9231	2357
74 6	34068	11566	5277	203	13408	8891	9772	6800	9231	14568
74 7	20806	8617	22806	214	17033	10714	9363	10982	12749	27249
74 8	42177	26075	33940	191	8317	12311	12311	4209	15948	1984
74 9	36740	11103	6546	216	11112	19521	19521	8616	12915	28466
74 10	80199	42500	19171	154	3106	32399	28221	31843	3346	1756
74 11	54775	11480	11690	124	9011	28280	28280	13937	6688	47161
14 11	54775	11480	11690	124	9011	28280	28280	13937	6688	1134
74 12	2672	134	2672	81	2149	3160	2267	13937	6688	1742
395051	170817	79490	1748	83651	113186	113186	62147	89379	75956	16031

EXHIBIT 7.12: CLADM Quality Output for Western C-14 Using  
1973-74 Land Uses

ИДЕНТИФИКАЦИОННЫЙ КОД КОМПОНЕНТА ИЛИ ПОДКОМПОНЕНТА ПОСРЕДСТВОМ КОТОРОГО ПОЛУЧАЮТ КОМПОНЕНТ ИЛИ ПОДКОМПОНЕНТ

73-74 КАНД. УСС  
ИДЕНТИФИКАЦИОННЫЙ КОД КОМПОНЕНТА ИЛИ ПОДКОМПОНЕНТА ПОСРЕДСТВОМ КОТОРОГО ПОЛУЧАЮТ КОМПОНЕНТ ИЛИ ПОДКОМПОНЕНТ

	TLSS	TLBDD	TLN	TLP	TGSS	TCBDD	TCN	TCP
62 1	193614	28457	1822	18 21	2 68	1 30	101	
63 1	193614	28457	1822	18 21	2 68	1 30	101	
63 2	1198745	21202	1364	31 34	1 55	56	036	
63 3	1027948	20211	10294	70 71	1 39	71	078	
63 4	289933	7325	3628	76 13	1 95	37	033	
63 5	544631	18510	8412	38 87	3 96	60	033	
63 6	2145541	21607	11510	96 46	3 97	32	088	
63 7	149899	15706	43560	9 34	1 98	2 71	068	
63 8	850401	21578	1821	39 73	1 01	21	068	
63 9	3005926	34128	31488	53 48	61	1 36	272	
63 10	598857	15586	100473	8 14	22	1 38	089	
63 11	921730	15646	25749	39 35	57	1 37	074	
63 12	560662	25260	10485	51 64	2 38	59	074	
	11474908	240215	299812	37 77	79	99	107	
64 1	813419	13992	66122	14 89	2 6	1 21	051	
64 2	2139841	24309	46472	49 54	3 6	1 31	052	
64 3	1045801	25108	18070	1 029	1 62	1 17	066	
64 4	1045801	25108	18070	67 49	1 82	1 17	066	
64 5	1412287	32905	19401	1168	96 71	1 33	086	
64 6	3485612	28447	37406	1809	94 23	1 01	048	
64 7	2895974	32914	70939	43 08	4 9	1 95	046	
64 8	1163323	24400	16321	69 15	1 85	3 77	054	
64 9	1746328	38600	82801	30 80	1 8	1 6	149	
64 10	2108157	26183	41447	50 37	63	1 29	278	
64 11	3015315	37388	178601	33257	1 27	1 24	104	
64 12	170664	7837	52517	4422	18	1 31	172	
	20352251	317858	25775	47182	72	1 31	172	
			67279	37 30	58	1 24	129	
65 1	91187	6866	3909	34 39	2 60	1 48	106	
65 2	1116940	33240	18285	48 87	1 45	1 80	054	
65 3	144570	13144	11878	17 17	1 56	1 84	086	
65 4	447421	20524	7321	173 29	7 95	2 84	253	
65 5	181716	3756	1535	213 62	4 42	1 80	143	
65 6	181716	3756	1535	213 62	4 42	1 80	143	
65 7	1275186	45173	33992	36 95	1 31	1 90	050	
65 8	3963378	36478	125949	51 03	2 01	1 62	049	
65 9	186758	17001	11998	15 89	37	2 01	239	
65 10	1242140	44681	6001	29 22	1 16	1 05	141	
65 11	1518834	38045	187325	7 22	16	1 89	168	
65 12	816669	14807	35285	7 31	1 09	1 09	091	
	18768	26118	9349	15 66	1 04	1 45	189	
	11876541	266481	674379	20 70	46	1 18	130	
66 1	1229632	23278	61047	24 28	46	1 21	054	
66 2	1466238	24460	62136	2825	32 53	1 97	044	
66 3	924734	15892	33439	1623	12 30	1 20	059	
66 4	622476	22853	8757	1743	4 55	1 74	148	
66 5	3032293	59320	22689	145 13	1 40	1 09	062	
66 6	2534689	43211	163183	6259	1 45	1 24	037	
66 7	759356	17959	430502	18 98	1 11	2 71	068	
66 8	759356	17959	430502	16 95	1 11	2 71	068	
66 9	2527100	22239	74715	55 33	1 64	1 64	183	
66 10	3998756	32251	35609	72 32	49	1 96	106	
66 11	1259634	28625	56724	6 32	1 39	1 82	359	
66 12	1345068	15123	35379	56 19	56	1 30	111	
	18113	15123	35379	4 35	56	1 30	111	
	172236	18113	15123	11 09	2 78	1 94	240	
			1564	1854	1 54	1 54	1 54	

67	1	1150794	21777	1514	51.00	.97	1.33	.067
67	2	725089	25068	1344	36.51	1.11	1.26	.068
67	3	17488	30633	1091	113.79	2.36	1.35	.083
67	4	0	0	23	0.00	0.00	1.20	.050
67	5	94204	1360	186.35	6.29	2.69	2.06	.206
67	6	472472	57794	201911	36	1.24	29.04	.051
67	7	1856467	19130	178549	28	21.41	6.69	.051
67	8	4132203	33015	108798	68.72	68.72	1.81	.201
67	9	2680509	30390	46636	58.80	67	1.02	.110
67	10	2680509	30390	46636	58.80	67	1.02	.110
67	11	137611	19198	234161	18.72	1.88	1.02	.374
67	12	459901	24895	20412	7.31	1.02	.91	.063
67	13	19460593	284490	891584	40.42	1.83	1.50	.180
67	14	0	0	84305	35.39	.52	1.60	.153
68	1	622700	11723	7830	104.34	1.96	1.31	.083
68	2	1827749	27915	12371	184.61	3.36	1.49	.113
68	3	186107	2569	1820	193.99	2.69	1.25	.090
68	4	21464	944	327	197.44	8.68	3.00	.272
68	5	5017055	48902	6279	37.33	37	1.06	.047
68	6	3221473	25654	210450	15.41	12	1.01	.040
68	7	888888	7617	300178	6.88	06	2.32	.057
68	8	1004782	30513	83302	18.54	56	1.54	.180
68	9	3170890	33672	71930	34.42	37	3.78	.093
68	10	616496	14588	336348	3.38	08	1.84	.378
68	11	204930	13151	29334	8.08	52	1.16	.099
68	12	351285	19072	6321	179.19	13.60	4.51	.437
68	13	16733819	235920	113844	19.86	.28	1.43	.135
69	1	1764393	33429	34649	57.17	1.08	1.12	.058
69	2	6924	21589	1158	1.41	1.39	1.00	.076
69	3	1793100	39115	57479	35.53	.77	1.14	.056
69	4	222886	13348	2772	1388	10.66	1.33	.066
69	5	2206566	26515	73600	37.43	45	1.25	.058
69	6	4112559	51608	159889	34.17	43	1.08	.045
69	7	3959550	32320	141655	51.86	47	2.04	.059
69	8	4387410	23959	20371	13.75	24	2.06	.245
69	9	4387410	23959	75765	59.31	1.02	6.51	.118
69	10	1611998	19035	35230	18.21	.22	1.98	.398
69	11	792821	10179	13314	7.12	09	1.20	.099
69	12	3755605	14862	98665	5.05	1.33	1.33	.182
69	13	2224334	324146	112799	27.34	40	1.44	.139
69	14	2224334	324146	112799	27.34	40	1.44	.139
70	1	1557336	42594	72283	29.60	81	1.37	.063
70	2	1636133	31886	55801	38.56	75	1.32	.062
70	3	1603082	59791	167812	11.90	42	1.19	.052
70	4	0	0	35333	0.00	0.00	1.20	.050
70	5	759021	53941	66415	16.18	1.15	1.42	.073
70	6	2438320	49179	102671	25.20	51	1.06	.046
70	7	1266387	18655	23321	12.07	18	2.32	.060
70	8	1430478	17156	35394	38.68	58	1.20	.131
70	9	9994289	28397	46777	22.20	3	1.04	.138
70	10	483968	10517	154232	7.77	1.99	2.83	.406
70	11	0	6780	2665	0.00	17.19	2.83	.280
70	12	1225434	317866	982544	18.79	.49	1.46	.099



71	1	10400	749	243	23	35	5	24	213
71	2	621	3527	1176	110	86	85	1	153
71	3	621	3527	1176	110	86	85	1	153
71	4	0	0	0	0	1	1	1	1
71	5	2400701	0	22028	1231	149	24	1	977
71	6	1066145	20107	1188	798	130	81	1	987
71	7	404045	13902	6643	467	101	69	1	118
71	8	3058213	27928	15574	977	307	36	1	498
71	9	4564330	33026	56284	5498	97	26	0	117
71	10	2707011	47531	95134	15252	53	47	1	301
71	11	1442656	14726	49192	5302	24	72	2	991
71	12	1361670	37542	25470	2176	96	33	1	155
		17077950	232614	303227	31743	81	73	1	152
72	1	1169335	24591	21109	1174	97	66	1	988
72	2	3087218	22061	24659	1248	171	41	1	97
72	3	715451	29556	19104	1053	56	67	1	983
72	4	1842449	22149	35196	1927	60	15	1	963
72	5	2418680	27494	67667	3116	42	60	1	955
72	6	4724339	44188	109478	4605	49	73	1	948
72	7	1968622	37644	185973	3266	22	17	2	959
72	8	707135	18875	132276	47	158	77	1	97
72	9	1353892	17779	6970	6770	32	41	1	123
72	10	747207	30937	5753	8931	21	42	1	256
72	11	1439473	30465	37899	2787	52	83	1	91
72	12	523124	17136	33094	4316	51	11	1	174
		20696725	321825	779648	57268	59	69	1	150
						59	69	1	110
73	1	910799	22294	23277	1279	55	89	1	43
73	2	1329880	25462	13477	889	136	09	1	30
73	3	442784	20101	13265	917	39	27	1	78
73	4	733336	5819	1870	180	113	38	1	289
73	5	450318	6653	3031	221	226	36	1	111
73	6	2117509	31599	25693	1331	72	86	1	98
73	7	2175099	31599	25693	1331	72	86	1	98
73	8	1644762	29005	223566	5970	16	42	1	88
73	9	3345718	50502	154089	16167	26	77	1	99
73	10	563762	13332	135934	19774	4	75	1	88
73	11	1466593	20128	74172	14153	31	04	2	124
73	12	686050	16630	74581	6508	11	00	1	100
73	1	281395	23314	20970	1631	15	31	1	137
73	2	13312915	262840	764925	69417	24	72	1	142
74	1	931399	28902	68957	2379	10	33	1	77
74	2	0	0	11222	469	0	00	1	050
74	3	143521	8775	3487	91	21	180	1	232
74	4	282917	16245	5409	506	23	77	3	94
74	5	535057	10696	5181	360	26	11	2	21
74	6	2845668	29144	42505	1842	20	53	1	155
74	7	3825414	43303	139518	4263	21	75	2	062
74	8	1659502	23124	151602	17171	51	35	2	250
74	9	1825502	23124	151602	17171	51	35	2	250
74	10	3209147	41645	42830	3740	16	35	1	124
74	11	559490	40722	168821	29395	1	81	1	251
74	12	670430	42862	26064	1595	21	89	1	044
74	1	21639	5581	24652	3404	1	75	1	186
74	2	14673185	291300	689458	56200	31	61	1	143

EXHIBIT 7-13: CLADM Quality Output for Western C-14  
Using Planned Scenario.



2646002	747494	1267875	111157	2.35	83	1.42	1.4
67 1	70436	85872	31902	2.75	3.34	1.24	106
67 2	118909	67713	24220	2.96	1.06	0.94	0.94
67 3	258794	14207	1859	13.48	3.95	0.97	0.97
67 4	8920	0	0	1	1	1	1
67 5	102526	79404	173100	22.52	14.85	1.76	332
67 6	152726	165301	185301	5.86	46	.99	0.46
67 7	362625	111067	13103	1.63	68	2.49	0.73
67 8	368657	59640	41595	4.29	1.14	1.55	1.97
67 9	368657	59640	41595	6.11	1.05	1.73	1.10
67 10	261134	44731	239723	1.93	33	1.77	367
67 11	251134	44731	239723	48.66	33	1.77	367
67 12	170740	46391	15721	1.88	64	0.44	0.45
	36252	9335	23359	2.15	4.97	1.38	222
	2722734	682080	863857	95.976	1.09	1.38	1.54
68 1	35107	40313	7067	5.44	6.24	1.09	150
68 2	64093	89316	15469	4.94	6.35	1.10	152
68 3	38135	40100	4673	6.22	6.54	1.76	142
68 4	0	0	0	1	1	1	1
68 5	484017	87854	122544	2.76	.60	.84	.045
68 6	288569	34920	194521	1.32	16	.89	0.37
68 7	54205	16689	29985	1.3	13	2.23	0.56
68 8	70156	10351	92680	1.11	1.47	1.66	1.92
68 9	328889	82428	16825	3.51	.61	.67	.097
68 10	181104	35895	351877	18	1.80	1.80	374
68 11	15411	34891	34891	57	1.13	1.14	1.14
68 12	18807	5725	1223	9.03	26.78	3.12	587
	1514804	617616	1198131	1.64	.67	1.29	137
	1514804	617616	1198131	.67	1.59	1.37	137
69 1	319866	100520	33527	8.29	2.60	.87	.078
69 2	175282	92520	18716	9.85	3.29	1.05	.099
69 3	41357	90202	3670	6.91	1.51	.87	.61
69 4	14954	28969	1915	58	1.34	1.64	.079
69 5	12432	8227	75548	45.45	1.26	1.14	.069
69 6	93925	63854	102805	6.81	.47	.79	.038
69 7	23672	80718	5091	5.091	2.60	1.83	1.00
69 8	136218	64139	209820	26.081	1.24	.60	.243
69 9	408228	68230	10254	4.254	73	1.76	1.14
69 10	109958	190317	39459	1.05	52	1.96	394
69 11	153577	31018	147509	43	.25	1.17	1.01
69 12	25947	42009	109571	31	50	1.31	1.87
	2951027	776550	1190579	3.18	.83	1.28	1.39
70 1	341892	108630	59660	6.17	1.96	1.08	.075
70 2	113286	63938	45618	2.945	1.34	6.67	.97
70 3	313286	63938	45618	6.67	1.34	2.945	.97
70 4	714829	84693	134070	4.84	6.63	.91	.047
70 5	0	0	16185	15.08	0.00	1.20	0.050
70 6	498686	36709	15129	10.49	.77	1.08	0.93
70 7	828803	72997	87918	4.899	.64	.77	.040
70 8	268053	27651	225481	2.22	2.13	2.76	2.56
70 9	128160	51865	39466	5.183	1.09	1.09	1.44
70 10	67431	99156	51712	6.697	1.86	.97	1.52
70 11	41665	32283	134356	60	47	1.95	405
70 12	0	0	17027	0.00	17.01	1.93	0.368
	3339810	615705	870452	619	37.18	4.22	805
				72557	4.58	1.23	1.03

71	1	29	69436	7253	451
71	2	23	64139	7692	149
71	3	0	127	5879	274
71	4	0	0	667	571
71	5	0	0	1	1
71	6	442474	99277	16445	64
71	7	442474	92277	16445	64
71	8	243955	81183	16445	64
71	9	82072	42843	13072	67
71	10	103275	75873	17175	81
71	11	459655	36676	17175	81
71	12	235967	109843	32647	101
71	13	131211	183921	57998	174
71	14	181969	26971	20317	233
71	15	2084734	589471	41884	683
72	1	116683	58206	18283	112
72	2	57586	93277	12497	139
72	3	134560	58473	35953	242
72	4	241145	63804	3721	174
72	5	674607	65905	96177	368
72	6	386459	72848	184573	601
72	7	373263	72848	184573	601
72	8	78234	59969	14461	83
72	9	242176	70183	34853	119
72	10	242176	70183	34853	119
72	11	24036	57286	5342	226
72	12	2963101	773784	471115	1827
73	1	48352	71625	22535	122
73	2	121977	76977	15662	1948
73	3	69132	58917	15269	6399
73	4	4183	30842	3511	456
73	5	50306	58468	6796	191
73	6	208996	60227	1876	743
73	7	251536	53129	6133	843
73	8	652462	81476	16722	944
73	9	30002	37115	22	52
73	10	80933	52524	27777	109
73	11	34184	57531	84732	111
73	12	66747	72994	35117	166
73	13	1618680	714985	86652	186
74	1	267058	53800	66727	110
74	2	0	11705	1468	251
74	3	63132	10496	7556	000
74	4	4695	18660	5265	1675
74	5	114059	6772	1519	183
74	6	365051	56147	7885	236
74	7	522145	86610	154016	1089
74	8	203917	5252	19208	488
74	9	516474	37964	4750	186
74	10	998670	148250	30268	199
74	11	333523	54668	3168	248
74	12	33523	24690	3168	248
74	13	16297	27567	3927	81
74	14	3298643	572509	75791	118
75	1	2081	503	2081	503
75	2	1256	149	1256	149
75	3	2638	299	2638	299
75	4	5076	598	5076	598
75	5	9152	1147	9152	1147
75	6	14628	1846	14628	1846
75	7	23404	3010	23404	3010
75	8	37446	4824	37446	4824
75	9	57912	7519	57912	7519
75	10	88256	11428	88256	11428
75	11	132384	17392	132384	17392
75	12	201568	26542	201568	26542
75	13	302352	39813	302352	39813
75	14	453536	59719	453536	59719
75	15	680304	89578	680304	89578
75	16	1020464	134366	1020464	134366
75	17	1530696	201549	1530696	201549
75	18	2296032	302320	2296032	302320
75	19	3444048	453480	3444048	453480
75	20	5166072	680120	5166072	680120
75	21	7748800	1020192	7748800	1020192
75	22	11523200	1530288	11523200	1530288
75	23	17284800	2295376	17284800	2295376
75	24	25927040	3443064	25927040	3443064
75	25	38880000	5164544	38880000	5164544
75	26	58521600	7746016	58521600	7746016
75	27	87842400	11527040	87842400	11527040
75	28	131763200	17288064	131763200	17288064
75	29	197635200	25929024	197635200	25929024
75	30	296457600	38880000	296457600	38880000
75	31	444686400	58521600	444686400	58521600
75	32	670028800	87842400	670028800	87842400
75	33	1005043200	131763200	1005043200	131763200
75	34	1507564800	197635200	1507564800	197635200
75	35	2261350400	296457600	2261350400	296457600
75	36	3442022400	444686400	3442022400	444686400
75	37	5162694400	670028800	5162694400	670028800
75	38	7743366400	1005043200	7743366400	1005043200
75	39	11544000000	1507564800	11544000000	1507564800
75	40	17284800000	2261350400	17284800000	2261350400
75	41	25925600000	3442022400	25925600000	3442022400
75	42	38886400000	5162694400	38886400000	5162694400
75	43	58527200000	7743366400	58527200000	7743366400
75	44	87848000000	11544000000	87848000000	11544000000
75	45	131768000000	17284800000	131768000000	17284800000
75	46	197638000000	25925600000	197638000000	25925600000
75	47	296448000000	38886400000	296448000000	38886400000
75	48	444658000000	58527200000	444658000000	58527200000
75	49	670068000000	87848000000	670068000000	87848000000
75	50	1005072000000	131768000000	1005072000000	131768000000
75	51	1507593600000	197638000000	1507593600000	197638000000
75	52	2261318400000	296448000000	2261318400000	296448000000
75	53	3442043200000	444658000000	3442043200000	444658000000
75	54	5162768000000	670068000000	5162768000000	670068000000
75	55	7743492800000	1005072000000	7743492800000	1005072000000
75	56	11544240000000	1507593600000	11544240000000	1507593600000
75	57	17284448000000	2261318400000	17284448000000	2261318400000
75	58	25924656000000	3442043200000	25924656000000	3442043200000
75	59	38884864000000	5162768000000	38884864000000	5162768000000
75	60	58525072000000	7743492800000	58525072000000	7743492800000
75	61	87845280000000	11544240000000	87845280000000	11544240000000
75	62	131764864000000	17284448000000	131764864000000	17284448000000
75	63	197626944000000	25924656000000	197626944000000	25924656000000
75	64	296429024000000	38884864000000	296429024000000	38884864000000
75	65	444631104000000	58525072000000	444631104000000	58525072000000
75	66	670033184000000	87845280000000	670033184000000	87845280000000
75	67	1005037120000000	131764864000000	1005037120000000	131764864000000
75	68	1507557920000000	197626944000000	1507557920000000	197626944000000
75	69	2261278720000000	296429024000000	2261278720000000	296429024000000
75	70	3442003520000000	444631104000000	3442003520000000	444631104000000
75	71	5162728320000000	670033184000000	5162728320000000	670033184000000
75	72	7743453120000000	1005037120000000	7743453120000000	1005037120000000
75	73	11544739200000000	1507557920000000	11544739200000000	1507557920000000
75	74	17284947200000000	2261278720000000	17284947200000000	2261278720000000
75	75	25925155200000000	3442003520000000	25925155200000000	3442003520000000
75	76	38885363200000000	5162728320000000	38885363200000000	5162728320000000
75	77	58525571200000000	7743453120000000	58525571200000000	7743453120000000
75	78	87845779200000000	11544739200000000	87845779200000000	11544739200000000
75	79	131767872000000000	17284947200000000	131767872000000000	17284947200000000
75	80	197629952000000000	25925155200000000	197629952000000000	25925155200000000
75	81	296432032000000000	38885363200000000	296432032000000000	38885363200000000
75	82	444634112000000000	58525571200000000	444634112000000000	58525571200000000
75	83	670036192000000000	87845779200000000	670036192000000000	87845779200000000
75	84	1005065760000000000	131767872000000000	1005065760000000000	131767872000000000
75	85	1507586560000000000	197629952000000000	1507586560000000000	197629952000000000
75	86	2261307360000000000	296432032000000000	2261307360000000000	296432032000000000
75	87	3442032160000000000	444634112000000000	3442032160000000000	444634112000000000
75	88	5162756960000000000	670036192000000000	5162756960000000000	670036192000000000
75	89	7743481760000000000	1005065760000000000	7743481760000000000	1005065760000000000
75	90	11544925600000000000	1507586560000000000	11544925600000000000	1507586560000000000
75	91	17285133600000000000	2261307360000000000	17285133600000000000	2261307360000000000
75	92	25925341600000000000	3442032160000000000	25925341600000000000	3442032160000000000
75	93	38885549600000000000	5162756960000000000	38885549600000000000	5162756960000000000
75	94	58525757600000000000	7743481760000000000	58525757600000000000	7743481760000000000
75	95	87845965600000000000	11544925600000000000	87845965600000000000	11544925600000000000
75	96	131769736000000000000	17285133600000000000	131769736000000000000	17285133600000000000
75	97	197631816000000000000	25925341600000000000	197631816000000000000	25925341600000000000
75	98	296433896000000000000	38885549600000000000	296433896000000000000	38885549600000000000
75	99	444635976000000000000	58525757600000000000	444635976000000000000	58525757600000000000
75	100	670038056000000000000	878459656000000000000	670038056000000000000	878459656000000000000

Exhibit 7.14: Computer Program for the Discharge Model



000132

DO 60 I=1,12

\*READ HISTORICAL DATA

000134

READ(1,1030)IYRH,IMOH,RAINH,RFH,DSETH

\*READ FUTURE DATA

I

\*READ FUTURE DATA

000151

READ(2,1030)IYRF,IMOF,RAINRF,RFF,DSETF

000167

1030 FORMAT(1X,I2,X,I2,80X,3(2X,F9.0))

000167

IF(IYRH.EQ.IYRF.AND.IMOH.EQ.IMOF)25,9020

000200

25 CONTINUE

000200

IF(IYRH.NE.IYRDISH)GO TO 9030

000202

XNGWLH=RAINH-DISH(I)-DSETH-SWETH(I)

000206

IF(XNGWLH)30,30,40

000210

30 CONTINUE

000210

XNGWLF=XNGWLH\*(1+XIFI)

000214

GO TO 50

000214

40 CONTINUE

000214

XNGWLF=XNGWLH/(1+XIFI)

000217

50 CONTINUE

000217

DISF=RAINH-XNGWLF-DSETF-SWETF(I)+DISFNS

000224

IF(DISF)52,54,54

000226

52 CONTINUE

000226

DISFNS=DISF

000227

DISF=0.

000230

GO TO 56

000231

54 DISFNS=0.

000232

56 CONTINUE

000232

YRAINH=YRAINH+RAINH

000234

YDISH=YDISH+DISH(I)

000236

YRRFH=YRRFH+RFH

I 000236

YRRFH=YRRFH+RFH

000240

YRSWETH=YRSWETH+SWETH(I)

000242

YRDSETH=YRDSETH+DSETH

000244

YRXNGH=YRXNGH+XNGWLH

000246

YRXNGF=YRXNGF+XNGWLF

000250

YRRFF=YRRFF+RFF

000252

YRDSETF=YRDSETF+DSETF

000254

YRSWETF=YRSWETF+SWETF(I)

000256

YRDISF=YRDISF+DISF

000260

WRITE(4,2000)IYRH,IMOH,RAINH,DISH(I),RFH,SWETH(I),

\* DSETH,XNGWLH,XNGWLF,RFF,DSETF,SWETF(I),DISF

000315

2000 FORMAT(X,I2,X,I2,11(2X,F9.0))

000315

60 CONTINUE

000317

WRITE(4,2010)YRAINH,YDISH,YRRFH,YRSWETH,YRDSETH,YRXNGH,

\* YRXNGF,YRRFF,YRDSETF,YRSWETF,YRDISF

000351

2010 FORMAT(6X,11(2X,F9.0)/)

000351

YRAINH=YDISH=YRRFH=YRSWETH=YRDSETH=YRXNGH=YRXNGF=0.

000360

YRRFF=YRDSETF=YRSWETF=YRDISF=0.

000364

READ(1,1050)

000367

READ(2,1050)

000373

1050 FORMAT(X,/)GO TO 10

000373

GO TO 10

I 000373

GO TO 10

\*ERROR MESSAGES

000374

9010 CONTINUE

000374

WRITE(4,9011)

000400

9011 FORMAT(\* STRUCTURE ID DO NOT MATCH\*/

\* \*CHECK ID ON ALL INPUT DATA\*)

000400

STOP1

000402

9020 CONTINUE

000402

WRITE(4,9021)

000406

9021 FORMAT(\* YEARS AND/OR MONTH DO NOT MATCH ON INPUT DATA\*)



```

* * CHECK DATA FILES(LAND AND SCENARIO)*
000406      STOP2
000410      9030  CONTINUE
000410      WRITE(4,9031)
000414      9031  FORMAT(* HISTORICAL DISCHARGE NOT IN SEQUENCE.*/
* * WITH INPUT FILES. CHECK YEAR SEQUENCE OF HISTORICAL*/
* * DISCHARGE.*)
000414      STOP3
000416      9999  STOP
000420      END

```

## CROSS REFERENCE MAP-DISCHAR

```

PROGRAM LENGTH INCLUDING I/O BUFFERS
013052

```

## STATEMENT FUNCTION REFERENCES

#	LOCATION	GEN TAG	SYM TAG	REFERENCES
	LOCATION	GEN TAG	SYM TAG	REFERENCES

## STATEMENT NUMBER REFERENCES

	LOCATION	GEN TAG	SYM TAG	REFERENCES
	000101	L00037	5	000077
	000107	L00042	10	000373
	000130	L00051	20	NONE
	000200	L00070	25	000177
	000210	L00074	30	000207
	000214	L00076	40	000207
	000217	L00077	50	000213
	000226	L00101	52	NONE
	000231	L00104	54	000225
	000232	L00105	56	000230
	000441	C00017	1000	000004 000012
	000504	C00062	1004	000030 000046 000107
	000502	C00060	1020	000101
	000511	C00067	1030	000133 000151
	000525	C00103	1050	000363 000367
	000457	C00035	1060	000024
	000445	C00023	1070	000020
	000516	C00074	2000	000257
	000522	C00100	2010	000317
	000374	L00140	9010	000100 000131
	000527	C00105	9011	000374
	000402	L00145	9020	000177
	000402	L00145	9020	000177
	000543	C00121	9021	000402
	000410	L00152	9030	000201
	000560	C00136	9031	000410
	000416	L00157	9999	000127

## BLOCK NAMES AND LENGTHS

## VARIABLE REFERENCES

	LOCATION	GEN TAG	SYM TAG	REFERENCES
	000704	V00032	DISF	000224 000226 000256 000300
	000656	V00004	DISFNS	000003 000222 000227 000300
	000612	A00001	DISH	NONE
	000701	V00027	DSETF	000164 000221 000252 000300
	000674	V00022	DSETH	000146 000204 000242 000300
	000663	V00011	I	000040 000043 000056 000300
				000133 000202 000217 000300

EXHIBIT 7.12: CLADM Quality Output for Western C-14 Using  
1973-74 Land Uses

	000666	V00014	IDISHT	000274	000310	000315	
	000662	V00010	IDUM	000112	000130		
	000676	V00024	IMOF	000035	000053		
	000671	V00017	IMOH	000156	000173		
				000140	000172	000264	
	000664	V00012	ISMFT	000051	000073		
I	000664	V00012	ISMFT	000051	000073		
	000661	V00007	ISWHT	000033	000070		
	000657	V00005	ITITLEL	000007	000064	000130	
	000660	V00006	ITITLES	000015	000064		
	000667	V00015	IYRDISH	000114	000200		
	000675	V00023	IYRF	000154	000167		
	000670	V00016	IYRH	000136	000167	000200	000264
	000677	V00025	RAINP	000160			
	000672	V00020	RAINH	000142	000203	000220	000264
	000700	V00026	RFF	000162	000250	000304	
	000673	V00021	RFH	000144	000236	000272	
	000642	A00003	SWETF	NONE			
	000626	A00002	SWETH	NONE			
	000665	V00013	XIFI	000104	000211	000214	
	000703	V00031	XNGWLF	000213	000216	000220	000264
	000702	V00030	XNGWLH	000206	000212	000215	000264
	000706	V00034	YDISH	000235	000324	000356	
	000705	V00033	YRAINH	000232	000322	000357	
II	000705	V00033	YRAINH	000232	000322	000357	
	000717	V00045	YRDISF	000255	000346	000360	
	000715	V00043	YRDSETF	000251	000342	000362	
	000711	V00037	YRDSETH	000241	000332	000353	
	000714	V00042	YRRFF	000247	000340	000363	
	000707	V00035	YRRFH	000236	000326	000355	
	000716	V00044	YRSWETF	000254	000344	000361	
	000710	V00036	YRSWETH	000240	000330	000354	
	000713	V00041	YRXNGF	000245	000336	000351	
	000712	V00040	YRXNGH	000243	000334	000352	

## START OF CONSTANTS

000422

## START OF TEMPORARIES

000602

## START OF INDIRECTS

000607

## UNUSED COMPILER SPACE

011200

```

000003      SUBROUTINE CHANGE(ARRAY)
000003      DIMENSION ARRAY(12)
000003      DO 10 I=1,12
000005         ARRAY(I)=(ARRAY(I)*(74850.))/12.
000010      CONTINUE
000012      RETURN
000012      END

```

CROSS REFERENCE MAP-CHANGE

IROSS REFERENCE MAP-CHANGE

SUBPROGRAM LENGTH

000025

STATEMENT FUNCTION REFERENCES

LOCATION	GEN TAG	SYM TAG	REFERENCES
STATEMENT NUMBER	REFERENCES		

LOCATION	GEN TAG	SYM TAG	REFERENCES
BLOCK NAMES AND LENGTHS			

BLOCK NAMES AND LENGTHS

VARIABLE REFERENCES

LOCATION	GEN TAG	SYM TAG	REFERENCES
000024	V00002	I	000004

START OF CONSTANTS

000014

START OF TEMPORARIES

000017

START OF INDIRECTS

000023

UNUSED COMPILER SPACE

013400

H13400

AJYQJLH. 17.46.42. 77/02/16.

\*\*\*\*\*  
\*\*\*\*\*

THIS IS D I S P O S E D OUTPUT.

IT WILL NOT HAVE A CARD DECK.

PLEASE PUT OUT FOR USER 9364003

\*\*\*\*\*  
\*\*\*\*\*

H

Exhibit 7.15: Computer Program for the Quality Computations

RPMQUA T=00004 IS ON CR00002 USING 00023 BLKS R=0197

```
0001 RPM,T10,CM50000, MCGRAW-FBY
0002 ACCOUNT,
0003 CBR,,QUALITY.
0004 R,QUALITY.
0005 RUN,S,,QUALITY,LOOK,QUALITE.
0006 RP,QUALITY,QUALITE.
0007 DISPOSE,LOOK=PR/EI=9364003.
0008 #D
0009          PROGRAM QUALITY(SCENAR,TAPE1=SCENAR,SCENARU,TAPE3=SCENARU,
0010          * LAND,TAPE2=LAND,
0011          * DISCHAR,TAPE4=DISCHAR,CARD2,TAPE5=CARD2,ONPS,TAPE10=ONPS
0012          * ,TLTC,TAPE11=TLTC,RLSSRLU,TAPE13=RLSSRLU,OUTPUT)
0013          DIMENSION ONPSCS(12),ONPSCB(12),ONPSCN(12),ONPSCP(12)
0014
0015 *READ INPUT CARDS
0016
0017          CALL READIT(ONPSCS)
0018          CALL READIT(ONPSCB)
0019          CALL READIT(ONPSCN)
0020          CALL READIT(ONPSCP)
0021
0022          READ(5,8001)REFFSS,REFFBD,REFFN,REFFP
0023 8001  FORMAT(10X,4(F10.2))
0024
0025 *SKIP HEADER ON INPUT FILES
0026
0027          CALL SKHEAD
0028
0029 *PRINT HEADER ON OUTPUT FILES
0030
0031          CALL HEADER
0032 10          CONTINUE
0033
0034          DO 20 I=1,12
0035
0036 *READ FUTURE DISCHARGE FROM FILE
0037
0038          READ(4,8000)IDATE1,DISF
0039 8000  FORMAT(X,R5,10(11X),2X,F9.0)
0040
0041          IF(EOF,4)9999,25
0042 25          CONTINUE
0043
0044 *READ SUMMARY DATA NONURBAN
0045
0046          READ(1,8010)IDATE2,RLSS,RLBBD,PLN,RLP,SRGN
0047 8010  FORMAT(X,R5,3X,2(11X),4(2X,F9.0),2(11X),2X,F9.0)
0048
0049 *READ DATA LAND
0050
0051          READ(2,8010)IDATE4,RLSS,RLBBD,RLLN,RLLP,SRLOW
0052
0053 *READ SUMMARY DATA URBAN
0054          READ(3,8010)IDATE3,RLSS,RLBBD,RLUN,RLUP,SRUGH
0055 *CHECK MONTH AND YEAR ON THE THREE INPUT FILES
0056          IF(IDATE1.NE.IDATE2.OR.IDATE2.NE.IDATE3
0057          * .OR.IDATE3.NE.IDATE4) GO TO 9000
0058
0059 *START CALCULATIONS FOR EACH MONTH
0060
```

```

0193      STOP
0194      END
0195      SUBROUTINE HEADER
0196      WRITE(10,8000)
0197      8000  FORMAT(12X,*0NPSLS*,6X,*0NPSLB*,6X,*0NPSLN*,6X,*0NPSLP*,
0198      * 5X,*0NPSCSY*,5X,*0NPSCBY*,5X,*0NPSCNY*,5X,*0NPSCPY*
0199      * ,6X,*0NPSON*)
0200      WRITE(11,8010)
0201      8010  FORMAT(14X,*TLSS*,7X,*TLBOD*,9X,*TLN*,9X,*TLP*,8X,
0202      * *TCSS*,7X,*TCBOD*,9X,*TCN*,9X,*TCP*)
0203      WRITE(13,8030)
0204      8030  FORMAT(12X,*RLSS/SR*,2X,*RLBOD/SR*,4X,*RLN/SR*,4X,*RLP/SR*,
0205      * 2X,*RLUSS/SR*,1X,*RLUBOD/SR*,3X,*RLUN/SR*,3X,*RLUP/SR*,
0206      * ,2X,*RLSS/SR*,1X,*RLBOD/SR*,3X,*RLN*,3X,*RLLP*)
0207      RETURN
0208      END
0209      SUBROUTINE READIT(ARRAY)
0210      DIMENSION ARRAY(12)
0211      READ(5,8000) ARRAY
0212      8000  FORMAT(10X,7(F10.3)/10X,5(F10.3))
0213      RETURN
0214      END
0215      SUBROUTINE SKIPIT
0216      READ(4,8010) IDUM
0217      READ(2,8010) IDUM
0218      READ(1,8010) IDUM
0219      READ(3,8010) IDUM
0220      8010  FORMAT(A10)
0221      RETURN
0222      END
0223      SUBROUTINE SKHEAD
0224      READ(1,8000)
0225      READ(2,8000)
0226      READ(3,8000)
0227      8000  FORMAT(/////////)
0228      READ(4,8010)
0229      8010  FORMAT(/)
0230      RETURN
0231      END
0232      $E

```

```

0127  ONPSCBY=SUMSLB/TTTTSQN
0128  ONPSCNY=SUMSLN/YYYYSQN
0129  ONPSCPY=SUMSLP/YYYYSQN
0130
0131  WRITE(10,8040)IDATE1,SUMSLS,SUMSLB,SUMSLN,SUMSLP,
0132  * ONPSCSY,ONPSCBY,ONPSCNY,ONPSCPY,SUMSQN
0133  *READ YEARLY FUTURE DISCHARGE
0134  READ(4,8000)IDUM,DISCHYR
0135
0136  ZZDIS=DISCHYR*2.71778
0137  YRTCSS=SUMTLSS/ZZDIS
0138  YRTCBOD=SUMTLBO/ZZDIS
0139  YRTCN=SUMTLN/ZZDIS
0140  YRTCP=SUMTLP/ZZDIS
0141
0142  WRITE(11,8040)IDATE1,SUMTLSS,SUMTLBO,SUMTLN,SUMTLP,
0143  * YRTCSS,YRTCBOD,YRTCN,YRTCP
0144  READ(1,8010)IDUM,RLSS,RLBOD,RLN,RLP,SRQN
0145  READ(3,8010)IDUM,RLUSS,RLUBOD,RLUN,RLUP,SRUQN
0146  READ(2,8010)IDUM,RLLSS,RLLBOD,RLLN,RLLP,SRLQN
0147
0148  AAASRQN=SRQN*2.71778
0149
0150  XRLSS=RLSS/AAASRQN
0151  XRLBOD=RLBOD/AAASRQN
0152  XRLN=RLN/AAASRQN
0153  XRLP=RLP/AAASRQN
0154
0155  AAASRQN=SRUQN*2.71778
0156
0157  XRLUSS=RLUSS/AAASRQN
0158  XRLUBOD=RLUBOD/AAASRQN
0159  XRLUN=RLUN/AAASRQN
0160  XRLUP=RLUP/AAASRQN
0161
0162  AAASRQN=SRLQN*2.71778
0163
0164  XRLSS=RLLSS/AAASRQN
0165  XRLBOD=RLLBOD/AAASRQN
0166  XRLN=RLLN/AAASRQN
0167  XRLP=RLLP/AAASRQN
0168
0169  WRITE(13,8030)IDATE1,XRLSS,XRLBOD,XRLN,XRLP,
0170  * XRLUSS,XRLUBOD,XRLUN,XRLUP,XRLSS,XRLBOD,XRLN,XRLP
0171
0172  WRITE(10,8060)
0173  WRITE(11,8060)
0174  WRITE(13,8060)
0175  8060  FORMAT(/)
0176  *SKIP BETWEEN YEARLY DATA ON INPUT FILES
0177
0178  CALL SKIPIT
0179
0180  *ZERO DATA
0181
0182  SUMSQN=SUMSLS=SUMSLB=SUMSLN=SUMSLP=0.
0183  SUMTLSS=SUMTLBO=SUMTLN=SUMTLP=0.
0184
0185  GO TO 10
0186
0187  *ERROR MESSAGES
0188  9000  CONTINUE
0189  PRINT 9001
0190  9001  FORMAT(* DATES ON INPUT FILES DO NOT MATCH*)
0191  CALL ABORT
0192  9999  CONTINUE

```



```

0061 ONPSQN=DISF-SRQN
0062 IF<ONPSQN.LT.0.> ONPSQN=0.0
0063 XXXSQN=ONPSQN*2.71778
0064 SUMSQN=SUMSQN+ONPSQN
0065
0066 ONPSLS=ONPSCS<I>*XXXSQN
0067 SUMSLS=SUMSLS+ONPSLS
0068 ONPSLB=ONPSCB<I>*XXXSQN
0069 SUMSLB=SUMSLB+ONPSLB
0070 ONPSLN=ONPSCN<I>*XXXSQN
0071 SUMSLN=SUMSLN+ONPSLN
0072 ONPSLP=ONPSCP<I>*XXXSQN
0073 SUMSLP=SUMSLP+ONPSLP
0074
0075 JLSS=ONPSLS+RLSS-REFFSS*RLUSS
0076 SUMTLSS=SUMTLSS+TLSS
0077 TLBOD=ONPSLB+RLBOD-REFBOD*RLUBOD
0078 SUMTLBO=SUMTLBO+TLBOD
0079 TLN=ONPSLN+RLN-REFFN*RLUN
0080 SUMTLN=SUMTLN+TLN
0081 TLP=ONPSLP+RLP-REFFP*RLUP
0082 SUMTLP=SUMTLP+TLP
0083
0084 XXXCON=DISF*2.71778
0085 TCSS=TLSS/XXXCON
0086 TCBOD=TLBOD/XXXCON
0087 TCN=TLN/XXXCON
0088 TCP=TLP/XXXCON
0089
0090 AAASRN=SRQN*2.71778
0091
0092 XRLSS=RLSS/AAASRN
0093 XRLBOD=RLBOD/AAASRN
0094 XRLN=RLN/AAASRN
0095 XRLP=RLP/AAASRN
0096
0097 AAASRN=SRQN*2.71778
0098
0099 XRLUSS=RLUSS/AAASRN
0100 XRLUBOD=RLUBOD/AAASRN
0101 XRLUN=RLUN/AAASRN
0102 XRLUP=RLUP/AAASRN
0103
0104 AAASRN=SRLQN*2.71778
0105
0106 XRLSS=RLLSS/AAASRN
0107 XRLBOD=RLLBOD/AAASRN
0108 XRLN=RLLN/AAASRN
0109 XRLP=RLLP/AAASRN
0110
0111 WRITE<10,8020>IDATE1,ONPSLS,ONPSLB,ONPSLN,ONPSLP
0112 * ,ONPSQN
0113 8020 FORMAT<X,R5,4<X,F11.0>,4<X,F11.0>
0114 WRITE<11,8040>IDATE1,TLSS,TLBOD,TLN,TLP,TCSS,TCBOD,TCN,T
0115 8040 FORMAT<X,R5,4<X,F11.0>,3<X,F11.2>,X,F11.3,X,F11.0>
0116 8030 FORMAT<X,R5,3<X,F9.2>,X,F9.3,3<X,F9.2>,X,F9.3
0117 * ,3<X,F9.2>,X,F9.3>
0118 WRITE<13,8030>IDATE1,XRLSS,XRLBOD,XRLN,XRLP,XRLUSS,XRLUB
0119 * XRLUN,XRLUP,XRLSS,XRLBOD,XRLN,XRLP
0120 20 CONTINUE
0121
0122 *CALCULATE YEARLY DATA
0123
0124 IDATE1=5R
0125 YYSQ=SUMSQN*2.71778
0126 ONPSCSY=SUMSLS/YYSQ

```

Exhibit 7.16: Computer Program for the Summary Output

```

*****
*****
*****
PROGRAM SUMM(OUTPUT, QUAL, TAPE1=QUAL, OUT, TAPE4=OUT
*, QUALSUM, TAPE2=QUALSUM)
000003 COMMON/TOT/ TRF, ITSUSP, ITBOD, ITN, ITP04
000003 COMMON/TOT/ TRF, ITSUSP, ITBOD, ITN, ITP04
000003 COMMON/CONSTA/AREA, RFCOEFF, AREAN, CN, CONST
000003 COMMON/ARRY/ TRAIN(25, 12), YRRAIN(25)
000003 DATA AREA, RFCOEFF, AREAN, CN, CONST/5*0./
000003 DATA(TRAIN(I), I=1, 300)/300*0./
000003 DATA(YRRAIN( I), I=1, 25)/25*0./
000003 DIMENSION IHOLD(132)
000003 DATA IOLDMO/0/
000003 DATA TRF, ITSUSP, ITBOD, ITN, ITP04/1*0., 4*0/
000003 CALL GETCOEF
000004 10 CONTINUE
000004 CALL BLANKIT(IHOLD)
000006 READ(1, 1000) IHOLD
000014 1000 FORMAT(132R1)
000014 IF(EOF, 1)9999, 11
000017 11 CONTINUE
000017 IF(IHOLD(2).EQ.1R*.AND.IHOLD(3).EQ.1R*)GO TO 20
000030 15 CONTINUE

000030 GO TO 10
000031 20 CONTINUE

000031 CALL BLANKIT(IHOLD)
000033 READ(1, 1000) IHOLD
000041 IF(EOF, 1)9999, 25
000041 25 IF(EOF, 1)9999, 25
000044 CONTINUE
000044 IF(IHOLD(2).EQ.1R .AND.IHOLD(6).EQ.1R1)30, 20
000055 30 CONTINUE
000055 ENCODE(2, 1030, IMD)(IHOLD(J), J=11, 12)
000071 1030 FORMAT(2R1)
000071 DECODE(2, 1040, IMD)MONTH
000101 1040 FORMAT(I2)
000101 ENCODE(5, 2000, JYRMDY)(IHOLD(J), J=8, 12)
000115 2010 DECODE(5, 2010, JYRMDY)IYRMDY
000125 2000 FORMAT(R5)
000125 2000 FORMAT(5R1)
000125 IF(IOLDMO.EQ.0) IOLDMO=MONTH
000127 IF(MONTH.NE.IOLDMO
* )CALL PRINTIT(MONTH, IOLDMO
* , IOLDYMD)
000133 ENCODE(5, 1060, IRUNOFF)(IHOLD(J), J=26, 30)
000147 1060 FORMAT(5R1)
000147 DECODE(5, 1062, IRUNOFF)RUNOFF
000157 1062 FORMAT(F5.2)
000157 TRF=TRF+RUNOFF
000161 ENCODE(6, 1064, ISUSP)(IHOLD(J), J=32, 37)
000175 1064 FORMAT(6R1)
000175 1064 FORMAT(6R1)

```

```

000175      DECODE(6,1066,ISUSP)INSUSP
000205      1066      FORMAT(I6)
000205      ITSUSP=ITSUSP+INSUSP
000207      ENCODE(5,1060,IBOD)(IHOLD(J),J=45,49)
000222      DECODE(5,1072,IBOD)INBOD
000232      ITBDD=ITBOD+INBOD
000234      1072      FORMAT(I5)
000234      ENCODE(5,1060,IN)(IHOLD(J),J=51,55)

000247      DECODE(5,1072,IN)N
000257      ITN=ITN+N
000261      ENCODE(5,1060,IP04)(IHOLD(J),J=56,60)
000274      DECODE(5,1072,IP04)NP04
000304      ITP04=ITP04+NP04

000306      CALL BLANKIT(IHOLD)
000307      IOLDYMD=IYRMDY
000311      READ(1,1000) IHOLD
000316      IF(EOF,1)9999,35
000321      35      CONTINUE
000321      IF(IHOLD(6).EQ.1R ) GO TO 38
000323      GO TO 30
000324      38      CONTINUE

000324      IF(IHOLD(2).EQ.1RP.AND.IHOLD(3).EQ.
* 1RA) 40,45
000335      40      CONTINUE
000335      40      CONTINUE

000335      CALL SKIPIT(IHOLD)
000337      GO TO 30
000340      45      CONTINUE

000340      MONTH=1
000341      CALL PRINTIT(MONTH,IOLDMO,IOLDYMD)
000344      9999      STOP
000346      END

SUMM

PROGRAM LENGTH INCLUDING I/O BUFFERS
010771

UNUSED COMPILER SPACE
010300

SUBROUTINE SKIPIT(IHOLD)
000003      DIMENSION IHOLD(132)
000003      10      CONTINUE

000003      1000      FORMAT(132R1)
000003      CALL BLANKIT(IHOLD)
000004      READ(1,1000) IHOLD
000014      IF(EOF,1)20,15
000020      15      CONTINUE
000020      IF(IHOLD(12).GE.1R0.AND.IHOLD(12).LE.1R9)RETURN
000033      GO TO 10

```

```
000034 20 RETURN
000035 END
```

```
SKIPIT
```

```
SUBPROGRAM LENGTH
000055
```

```
UNUSED COMPILER SPACE
013300
```

```
000003 SUBROUTINE BLANKIT(IHOLD)
000003 DIMENSION IHOLD(132)
000003 DIMENSION IHOLD(132)
000003 DO 10 I=1,132
000005 IHOLD(I)=10R
000007 10 CONTINUE
000011 RETURN
000011 END
```

```
BLANKIT
```

```
SUBPROGRAM LENGTH
000022
```

```
UNUSED COMPILER SPACE
013400
```

```
000006 SUBROUTINE PRINTIT(MONTH, IOLDMO, IOLDYMD)
000006 COMMON/TOT/ TRF,ITSUSP,ITBOD,ITN,ITP04
000006 COMMON/CONSTA/AREA,RFCOEFF,AREAN,CN,CONST
000006 COMMON/ARRAY/ TRAIN(25,12),YRRAIN(25)
000006 DATA IXYEAR,JOLDMO/1,1/
000006 DATA IZERO,ZERO/0,0/
000006 YRRF=YRRF+TRF
000010 IYRSUSP=IYRSUSP+ITSUSP
000011 IYRBOD=IYRBOD+ITBOD
000013 IYRN=IYRN+ITN
000014 IYRP04=IYRP04+ITP04
000016 XRAINF=TRAIN(IXYEAR, IOLDMO)
000022 RAINAF=ACFT(XRAINF)
000024 RFAF=ACFT(TRF)
000026 DSET=TRAIN(IXYEAR, IOLDMO)-(TRF /CONST)
000036 DSETAF=ACFT(DSET)
000036 DSETAF=ACFT(DSET)
000041 YRDSET=YRDSET+DSET
000043 YRDSAF=YRDSAF+DSETAF
000045 YRAINAF=YRAINAF+RAINAF
000047 YRFAF=YRFAF+RFAF
000051 IF(JOLDMO.LT.IOLDMO)12,16
000057 12 CONTINUE
000057 LCOUNT=IOLDMO-JOLDMO
000061 DO 14 IXI=1,LCOUNT
000062 ENCODE(10,1040,IYM)IOLDYMD,IXI
```

```

000073      RAINAF2=0.
000074      RAINAF2=ACFT(TRAIN(IXYEAR,IXI))
000102      YRAINAF=YRAINAF+RAINAF2
000103      WRITE(2,1020)IYM,TRAIN(IXYEAR,IXI),ZERO,IZERO,IZERO
          * , IZERO, IZERO, ZERO, RAINAF2, ZERO, ZERO

000140      14      CONTINUE
000145      16      CONTINUE
          WRITE(2,1020)IOLDYMD,TRAIN(IXYEAR,IOLDMO),TRF,ITSUSP,ITBOD
          * , ITN, ITP04, DSET, RAINAF, RFAF, DSETAF
000203      1020   FORMAT(X,R5,3X,2(2X,F9.2),4(2X,I9),2X,F9.2,3(2X,F9.0))
000203      TRF=ITSUSP=ITBOD=ITN=ITP04=DSET=RAINAF=RFAF=DSETAF=0
000203      TRF=ITSUSP=ITBOD=ITN=ITP04=DSET=RAINAF=RFAF=DSETAF=0
000215      05      CONTINUE
000215      IF(IOLDMO.GT.MONTH)GO TO 20
000222      IF(MONTH.EQ.IOLDMO+1) GO TO 10
000224      IOLDMO=IOLDMO+1
000225      ENCODE(10,1040,IOLDYMD)IOLDYMD,IOLDMO
000236      1040   FORMAT(A8,I2)
000236      RAINAF2=0.
000237      RAINAF2=ACFT(TRAIN(IXYEAR,IOLDMO))
000251      YRAINAF=YRAINAF+RAINAF2

000252      C
000253      WRITE(2,1020)IOLDYMD,TRAIN(IXYEAR,IOLDMO),TRF,
          * ITSUSP,ITBOD,ITN,ITP04,DSET,RAINAF2,RFAF,DSETAF
          GO TO 05
000311      10      CONTINUE
000314      JOLDMO=MONTH
000314      IOLDMO=MONTH
000315      RETURN
000316      20      CONTINUE
000316      IF(IOLDMO.EQ.12) GO TO 25
000320      IOLDMO=IOLDMO+1
000321      ENCODE(10,1040,IOLDYMD)IOLDYMD,IOLDMO

000333      WRITE(2,1020)IOLDYMD,TRAIN(IXYEAR,IOLDMO),TRF,
          * ITSUSP,ITBOD,ITN,ITP04,DSET,RAINAF,RFAF,DSETAF
          * ITSUSP,ITBOD,ITN,ITP04,DSET,RAINAF,RFAF,DSETAF
          GO TO 20
000373      25      CONTINUE
000376      WRITE(2,1010)YRRAIN(IXYEAR),YRRF,IYRSUSP,IYRBOD,IYRN,IYR
          * ,YRDSET,YRAINAF,YRFAF,YRDSAF
000376      FORMAT(1X,* * ,3X,2(2X,F9.2),4(2X,I9),2X,F9.2,3(2X,F9
000426      1010   IXYEAR=IXYEAR+1
000426      JOLDMO=1
000430      IOLDMO=MONTH
000431      YRRF=IYRSUSP=IYRBOD=IYRN=IYRP04=0
000433      YRDSET=YRDSAF=YRAINAF=YRFAF=0.
000440      RETURN
000444      END
000445

```

PRINTIT

SUBPROGRAM LENGTH

000532

UNUSED COMPILER SPACE

011400

```

SUBROUTINE GETCOEF
COMMON/CONSTA/AREA,RFCOEFF,AREAN,CN,CONST
DIMENSION ITITLE1(10),ITITLE2(10),ITITLE3(10)
DIMENSION IHOLD(132)
CONTINUE
10 READ(4,1000) I
   FORMAT(1X,R1)
000010 IF(I.EQ.1R*) 20,10
000015 20 CONTINUE
100015 20 CONTINUE
000015 READ(4,1020)ITITLE1,ITITLE2,ITITLE3,NONURB
000031 1020 * FORMAT(////,10A10/10A10/10A10/////58X,I1
   * ///////////////)
000031 CALL SUMRAIN
000032 READ(4,1024) AREA
000040 1024 FORMAT(/////25X,F9.2)
000040 35 CONTINUE
000040 READ(4,1026) IHOLD
000046 1026 FORMAT(132R1)
000046 IF(IHOLD(50).NE.1RF.AND.IHOLD(51).NE.1RF) GO TO 35
000060 ENCODE(7,1027,COE)<IHOLD(I),I=75,81)
000074 1027 FORMAT(7R1)
000074 DECODE(7,1028,COE) RFCOEFF
000104 1028 FORMAT(F7.5)
000104 IF(NONURB.EQ.0)GO TO 50
000105 30 CONTINUE
000105 READ(4,1030) KEY
000113 1030 FORMAT(25X,R5)
000113 IF(KEY.EQ.5RAREAN)40,30
000120 40 CONTINUE
000120 READ(4,1050)AREAN,CN
000130 1050 FORMAT(23X,F7.1,3X,F5.2)
000130 1050 FORMAT(23X,F7.1,3X,F5.2)
000130 GO TO 55
000131 50 CONTINUE
000131 AREAN=CN=0.
000133 55 CONTINUE
000133 READ(4,1055)KEY
000141 1055 FORMAT(1X,R9)
000141 IF(KEY.NE.9RTREATMENT) GO TO 55
000143 READ(4,1057) KEYTITL
000151 1057 FORMAT(103X,R7)
000151 WRITE(2,1058) KEYTITL
000157 1058 FORMAT(1X,R7)
000157 WRITE(2,1060)ITITLE1,ITITLE2,ITITLE3
000171 1060 FORMAT(3(10A10,/))
000171 WRITE(2,1070)
000175 1070 FORMAT(1X,*NONURB*,10X,*AREA*,3X,*RUNOFF COEFF*
   * ,4X,*AREAN*,8X,*CN*)
000175 WRITE(2,1080)NONURB,AREA,RFCOEFF,AREAN,CN
000213 1080 FORMAT(6X,I1,5X,F9.2,5X,F7.5,5X,F7.1,5X,F5.2)
000213 CONST=((RFCOEFF*AREA)+(CN*AREAN))/(AREA+AREAN)
000221 WRITE(2,1090)CONST
000226 1090 FORMAT(1X,*CONSTANT= *,F8.5)
000226 WRITE(2,2000)
000226 WRITE(2,2000)
000232 2000 FORMAT(1X,*MONTH*,6X,*RAIN(IN)*,1X,*RUNOFF(IN)*,
   * 7X,*SUSP*,8X,*BOD*,10X,*N*,8X,*P04*,7X,
   * *DSET*,3X,*RAIN(AF)*,1X,*RUNOFF(AF)*,
   * 3X,*DSET(AF)*)

```

```
000232      RETURN
000233      END
```

```
GETCOEF
```

```
SUBPROGRAM LENGTH
000653
```

```
UNUSED COMPILER SPACE
012100
```

```
000003      FUNCTION ACFT(XXX)
000003      COMMON/CONST/AREA,RFCOEFF,AREAN,CN,CONST
000007      ACFT=(XXX*(AREA+AREAN))/12.
000007      RETURN
000007      END
```

```
ACFT
```

```
SUBPROGRAM LENGTH
000022
```

```
UNUSED COMPILER SPACE
013400
```

```
000002      SUBROUTINE SUMRAIN
000002      COMMON/ARRY/TRAIN(25,12),YRRAIN(25)
000003      XMORAIN=0.
000003      READ(4,8000)IOLDYR,IOLDMD,RAIN
000015      8000  FORMAT(X,I4,X,I2,104X,F4.2)
          *READ RAINFALL DATA AND SUM FOR EACH MONTH
000015      ISTARYR=IOLDYR
000017      10  CONTINUE
000017      10  CONTINUE
000017      XMORAIN=XMORAIN+RAIN
000021      READ(4,8000)IYR,IMD,RAIN
          *SKIP IF HEADER DATA IS ENCOUNTERED .I.E. YEAR=0000
000033      IF(IYR.EQ.0000) GO TO 40
          *CHECK TO SEE IF MONTH HAS CHANGED
000034      15  CONTINUE
000034      IF(IOLDMD.NE.IMD) 20,10
000041      20  CONTINUE
          *ENTER RRAIN FOR MONTH IN PROPER ARRAY LOCATION
000041      I=IOLDYR-ISTARYR+1
000044      TRAIN(I,IOLDMD)=XMORAIN
000050      YRTEMP=YRTEMP+XMORAIN
000052      XMORAIN=0.
```



```

000052          IOLDM0=IM0
                *CHECK TO SEE IF YEAR HAS CHANGED

000053          IF(IOLDYR.NE.IYR) 30,10
000060          30      CONTINUE
000060          YRRAIN(I)=YRTEMP
000062          YRTEMP=0
000063          IOLDYR=IYR
000064          GO TO 10

                *SKIP HEADER AND CHECK IF RAINFALL DATA IS FINISHED
                *SKIP HEADER AND CHECK IF RAINFALL DATA IS FINISHED

000065          40      CONTINUE
000065          READ(4,8010) IYR,IM0,RAIN
000077          8010   FORMAT(///X,I4,X,I2,104X,F4.2)

                *IF YEAR IS EQUAL TO 0000 ON SECOND READ RAINFALL
                *DATA HAS ENDED

000077          IF(IYR.NE.0000) GO TO 15
000100          TRAIN(I,IOLDM0)=XMORAIN
000105          YRRAIN(I)=YRTEMP+XMORAIN
000107          9999   RETURN
000110          END

```

SUMRAIN

SUBPROGRAM LENGTH  
000141

UNUSED COMPILER SPACE  
013000  
113000

AJYQHWI. 23.20.10. 77/02/18.

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THIS IS D I S P O S E D OUTPUT.

IT WILL NOT HAVE A CARD DECK.

PLEASE PUT OUT FOR USER 9364003

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