

OPERATIONAL ANALYSIS OF A FLOOD IN THE LOWER
KISSIMMEE RIVER BASIN

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Central and Southern Florida Flood Control District

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1. INTRODUCTION

1.1 General Background

The Central and Southern Florida Flood Control District is responsible for the management and operation of a water resource system which extends over eighteen counties of the State of Florida and covers approximately 16,000 square miles in area. One of the major natural drainage areas within the District boundaries is the Kissimmee River - Lake Okeechobee - Everglades system, which includes a range of land use from the sprawl of cities to the wilderness of the Everglades. Inevitably, varieties of competing interests concerned with water and water-related problems tend to exert pressure on the management of the District water resource system.

Initial emphasis on Project works was flood control. To ensure it the Corps of Engineers in consultation with the Flood Control District improved channels and built control structures where necessary to serve flood control objectives. Some of the recent construction in the lower Kissimmee River Basin has already been subjected to the tests of nature under high flow conditions. In the early part of October 1969 a flood event in the lower Kissimmee River Basin occurred which caused considerable damage to Project facilities; i.e., the rip-rap channel protection downstream of several of the gated spillways. Consequently, analyses of the flood were made to find out the probable causes of damage and make recommendations to prevent such occurrences in the future. However, before going into the details of analysis, it is desirable to briefly describe the physical system itself.

1.2 Physical System

The Kissimmee River Basin (Figure 1) of the Kissimmee River - Lake Okeechobee - Everglades system is located in central Florida and includes most of Osceola and Okeechobee and parts of Orange, Polk, and Highlands Counties. It is bounded on the north by the lakes of the Orlando area, on the west by the Peace River watershed, on the south by Lake Okeechobee and the Lake Istokpoga - Indian Prairie area, and on the east by the Upper St. Johns River Basin.

The entire Kissimmee River Basin is approximately 3,000 square miles in area and it may be broadly divided into two parts: the upper basin and the lower basin. The upper basin consists of the lakes portion of the drainage area north of and including Lake Kissimmee, and totals approximately 1,600 square miles in area. The lower basin consists of the drainage area of the Kissimmee River itself and the Lake Istokpoga drainage, for a total of approximately 1,400 square miles. The study area, the lower Kissimmee River Basin, is described below in some detail.

The lower Kissimmee River Basin, excluding the Lake Istokpoga area, between the outlet of Lake Kissimmee and Lake Okeechobee, has a drainage area of 758 square miles. The easterly divide separating that basin from the Upper St. Johns River Basin is low and poorly defined with ground elevations up to 75 ft. msl. For the most part, the westerly divide is a well-defined ridge with elevations ranging up to 130 feet. The main natural channel of the river meanders extremely. The straight line distance between Lake Kissimmee and Lake Okeechobee is about 52 miles, but the actual river distance is about 90 miles, with a total fall of about 35 feet. Maximum flows are experienced in September and October, while

lowest flows occur during the spring. Lands in the lower basin are generally grassy prairies with scattered pinewoods and palmetto growths. There are some large citrus areas, tracts of improved pasture and small acreages of truck crops scattered through the basin.

1.2.1 Canals: The total length of Canal 38 is about 58.3 miles, out of which approximately 8.6 miles are between S-65E and S-65D, 9 miles are between S-65D and S-65C, 7.4 miles are between S-65C and S-65B, and the remainder is between S-65B, S-65A and S-65 and downstream of S-65E. Canal 38 has, in general, a bottom width between 90 feet and 425 feet, bottom elevations between -13.5 ft. and 18.0 ft. msl., and five control structures with navigation locks. A description of the control structures is given below.

1.2.2 Control Structures: There are five gated spillway structures: 65A, 65B, 65C, 65D and 65E on Canal 38. The details of these structures are available in the Design Memoranda but some pertinent information about them is given below.

	<u>S-65A</u>	<u>S-65B</u>	<u>S-65C</u>	<u>S-65D</u>	<u>S-65E</u>
Control Gates	Vert-Lift	Vert-Lift	Vert-Lift	Vert-Lift	Vert-Lift
No. of Gates	3	3	4	4	6
Net Width of a Gate	27'x13.7'	27'x13.7'	27x13.7'	27'x13.7'	27'x13.7'
Crest Elev. (msl.)	34.5'	26.3'	20.8'	13.1'	9.7'
Apron Elev. (msl.)	28.6'	19.4'	13.4'	5.3'	-1.6'
Discharge	11,000cfs	14,000cfs	18,000cfs	21,300cfs	24,000cfs
HWE(msl.)	46.3'	40.0'	34.0'	28.0'	22.0'
TWE(msl.)	42.9'	35.7'	30.1'	23.4'	19.3'

Each of the foregoing structures is associated with a lock for navigational purposes. The lock size is 30'x90' with 6 ft. normal depth of water over the sill.

1.2.3 Transient Situations: The transient physical situations that existed in the lower Kissimmee River Basin during the occurrence of the event were as follows: first, the dredge by-pass channel closures at the structures were not built to the tie-back levee elevation; second, the embankments were not covered with vegetation and were, therefore, totally exposed to the hazards of erosion; third, the channels above S-65C were not dredged to final design cross-section.

1.3 Normal Climatology

The normal climate over the basin is of the tropical type. Of the 50-55 inch average yearly rainfall over the basin, approximately 70 percent occurs in the five-month period of June through October. The other seven months account for the remaining 30 percent of the average yearly rainfall. The region is also subject to tropical storms and hurricanes which generally occur during the rainy season period of June through October. These hurricanes bring intense rainfall which often aggravates a flood situation already serious from heavy seasonal rainfall. Highest flows are generally experienced in September and October, while lowest flows occur during spring. Pertinent information concerning rainfall stations in the lower Kissimmee River Basin and neighboring areas is presented in Table 1.

1.4 Normal Operation

The gates of the control structures are operated by a lock-tender who resides at the site. The gates are usually operated in such a way that the headwater stage stays within two-tenths of a foot from its optimum value. This is done manually by the operator.

For flood control regulation the gate operation is obtained from an appropriate structure rating curve provided by the Office of the Corps of Engineers at Jacksonville, Florida. Insofar as possible all the gates are opened gradually and uniformly so that all the gates have the same opening. The gates which can be opened automatically are not allowed to exceed about two feet before all gates are opened.

When all gates are discharging, the difference in gate opening between the manually operated and automatic gates is not allowed to exceed one foot. The prescribed operation limits for the structures in question are presented in the section entitled "Analysis of the Event."

Also, when Structures 65A, 65B, 65C, 65D and 65E are discharging at their full capacity, a normal recommended operating practice is that Structure 65 be completely closed; that is, discharge through Structure 65 is zero.

2. THE EVENT

2.1 General Description

Tropical Storm Jenny first appeared as a threat to the mainland of Florida on October 1, 1969 as it appeared in the Gulf of Mexico approximately 30 miles west of Naples. It entered the mainland in the vicinity of Fort Myers on the afternoon of October 2, 1969, and proceeded north-northeastward over the Kissimmee and St. Johns basins at approximately 15 miles per hour, leaving the mainland in the vicinity of Titusville at approximately 10:00AM on October 3, 1969. Winds averaged 25 miles per hour with gusts of 40 to 50 miles per hour.

The heaviest rainfall during the October 1-3, 1969 occurrence was concentrated in the lower Kissimmee River Basin between Lakes Kissimmee and Okeechobee. Within this area of heavy rainfall the maximum concentration was in an approximate 200 square mile area centered almost exactly on the River and extending from S-65A to S-65D. The accumulated rainfall for this event, as measured by FCD raingages numbered 35, 38 and 43, at Structures 65B, 65C and 65D, were 9.33, 9.66 and 8.82 inches, respectively. Isohyetal maps for the periods of September 6 through 17, 1969; September 18 through 30, 1969; October 1 through 3, 1969; October 1, 2 and 3, 1969 are presented in the appendix. Rainfall values used in developing these isohyetals (see appendix) were those available at stations listed in Table 1. It is estimated that in this area the rainfall occurrence was of about a 1 in 15 years frequency.

2.2 Structure Operation

The structure operations were greatly handicapped due to a combination of the transient situations and the effects of unusual rainfall occurrence on the transient situations. However, in order to maintain the design stages and discharges at each of the five structures in the lower Kissimmee River during the flood period, the gates were accordingly opened. This operation resulted in sufficiently high stages behind some of the structures to cause concern. The concern was that the plugs could go off because the fill materials on the plugs were already severely eroded from heavy rainfall and the river was rising. Therefore, it was necessary to increase the discharge through these structures and place additional fill on the by-pass channel closures at the structures.

An increase in discharge through the structures created a further concern that high flows could severely damage the banks. Consequently, at Structure 65C, gates in the middle were opened higher than the gates on the sides. To lessen the critical conditions at the by-pass channel closures at the structures, a minimum discharge of 4,500 cfs was maintained at S-65 because of an abnormal condition that occurred in the Upper Kissimmee River Basin about a week before this event. The Kissimmee River discharge at S-65E rapidly reduced from October 7-8, 1969. This reduction enabled discharge at S-65 to be increased to 7,000 cfs. A listing of hourly gate operations performed at the problem Structures 65B, 65C, 65D and 65E during the period October 1 (8:00AM) through October 15 (1:00PM), 1969 is presented in the appendix.

2.3 Results

An antecedent condition of saturated ground caused the basin to produce relatively heavy runoff from Tropical Storm Jenny. This heavy runoff occurred primarily in the area south of Lake Cypress beginning with the Kissimmee-Hatchineha-Cypress Lake complex regulated by S-65 at the outlet of Lake Kissimmee. This complex rose 1.5 feet between October 1 and October 8, 1969 when stages in the Kissimmee River had reduced sufficiently to permit increased discharge rates at S-65. Lake Kissimmee peaked on October 8, 1969 at 54.15 feet while the maximum stages in this lake in 1953 and 1960 were 56.64 feet and 55.84 feet respectively.

Rather extensive flooding of pasture occurred in the area of the heaviest rainfall due to an inability of existing drainage ways to accommodate this type of rainfall occurrence. Some flooding was experienced in the flood plain of the Kissimmee River. Nevertheless, the present channelization was sufficient to materially reduce the length of flooding over that experienced under pre-Project conditions.

Damages were considerable to the channel rip-rap downstream of those control structures between S-65B and S-65E. Within the S-65B and S-65E reach the maximum damage was experienced at S-65D. A pattern of the damage that occurred at S-65D is presented in the appendix in the form of a river bed contour map. This contour map was prepared from the data collected from soundings taken shortly after the high flows of October 1969. In order to understand the extent of damage very broadly, a few design elevations are also shown (in red) on this map. These led to an analysis of the event which is presented in the next Section.

3. ANALYSIS OF THE EVENT

3.1 Objectives

The damages caused to the channel rip-rap, particularly at Structure 65D, created some concern to the Flood Control District. Consequently, the District undertook an analysis of the event with the following objectives:

1. Within the limits of available data, could reasonable assumptions be made to show if the District clearly violated the operational limits on the structures in question?
2. If the answer to objective one is yes, what should have been the proper way to operate the structures?
3. If the answer to objective one is no, could other reasons for rip-rap movement be determined in order that measures could be taken to prevent damages in the future?

3.2 Data Collection and Preparation

The data available were channel cross-sections (S-65B to S-65C, design; others, as built) along the reach from S-65B to S-65E; tail-and-headwater elevations and gate operations for the period 8:00AM October 1, 1969 through 1:00PM October 15, 1969; and Corps of Engineers (Jacksonville District, Florida) discharge rating curves received by the Flood Control District at West Palm Beach, Florida, on October 20, 1969.

The channel cross-sections data contained some negative elevations (mean sea level elevation = 0 was used as reference) and the computer program which existed at the time of analysis for the processing of cross-section data could not utilize negative elevations. Therefore, a constant of twelve feet was added to make every elevation a positive number greater than zero. An over bank capacity of the design channel cross-sections was arbitrarily limited to an extension (1:100 slope) of the channel section beyond its top elevation. The data available on tailwater elevations, TWE, at S-65E and on headwater elevations, HWE, at S-65B, S-65C, S-65D and S-65E were assumed to be satisfactory. The gate operations data were linearly interpolated at one hour intervals. The discharge rating curves for the structures received from the Corps of Engineers, Jacksonville District, Florida, were also assumed to be satisfactory. It was found from the stage records that, at times, reverse water slope and a high drop or rise of water surface elevation values at the control points along the reaches (which are fairly long) occurred with the one-hour interval basis. This was assumed to be due

to a combination of surges in the tailwater and errors in datum. Therefore, a datum correction of 0.1, 0.5 and 0.4 foot was applied to headwater stages (HWE) at S-65D, S-65C and S-65B, respectively. It was also decided to establish tailwater elevations at S-65D, S-65C, and S-65B. The computation of TWE is discussed below.

3.3 Tailwater Computation

The tailwater computation was based essentially upon the principles of gradually varied flow which utilized an equation of the form

$$\frac{dy}{dx} = PC \left[\frac{S_0 - SE}{1 - \alpha \frac{Q^2 T}{gA^3}} \right] \quad (1)$$

where y = depth of water,

S_0 = slope along the channel bed,

SE = energy gradient,

α = velocity head coefficient,

Q = discharge,

T = top width,

g = acceleration due to gravity,

A = cross-sectional area of the channel,

$PC = -1$, if the computation proceeds upstream, and

= 1, if computation proceeds downstream.

The three reaches (S-65B to S-65C, S-65C to S-65D, and S-65D to S-65E) were divided into several sub-reaches and use of Equation 1 necessarily required that bed elevations at various points along each of the reaches be known. To eliminate doubts as to the values of bed elevations and thereby in the computed S_0 values, it was decided to work directly in terms of water surface elevations (WSE) rather than the depth

of water. Further, the term $\alpha \frac{Q^2 T}{gA^3}$ in Equation 1 was assumed to be negligible. Thus, Equation 1 could be re-written as

$$\frac{d(WSE)}{dx} = PC(-SE) \quad (2)$$

where WSE = water surface elevation.

Energy gradient, SE, was determined as

$$SE = \frac{(RN)^2 Q^2}{2.22(Con)^2} \quad (3)$$

where RN = Manning's roughness coefficient, and

$$Con = \frac{A^{5/3}}{P^{2/3}} = \text{section factor in which } p = \text{wetted perimeter.}$$

The section factor for each of the sections along the reach was estimated with the help of a generalized computer program developed for estimating geometric elements of natural channel sections. The program utilized available section data and yielded a functional relationship between the section factor and WSE at each of the sections along the reach. The functional relationship between Con and WSE was based upon Legendre Polynomial approximation. A six-order polynomial, in general, produced a best fit between Con and WSE at each of the sections along the reach.

Using available discharge rating curves, functional relationships for estimating discharge through each of the structures were developed. An equation, in its general form, representing the relationship, is as follows:

$$Q_n = a(GO)^b(EH)^c, \quad 0 \leq GO \leq Y, \quad EH > 0 \quad (4)$$

where n = structure number,

G_0 = effective gate opening,

EH = effective head, i.e., difference in head across the structure,

Y = depth of water at the weir crest or maximum limit on gate opening, and

a, b, c = constants.

The value of Q that should reflect into the change of WSE within a reach at any time could be estimated very well by an equation

$$Q_{NET} = Q_D - (Q_U + Q_L) + WL \quad (5)$$

where Q_{NET} = net discharge in the reach,

Q_D = discharge through downstream structure,

Q_U = discharge through upstream structure,

Q_L = local inflow into the reach, and

WL = water loss from the reach.

Due to the unavailability of time distribution of rainfall within each reach and reliable tailwater elevations (TWE), it is difficult to obtain reliable estimates of Q_L and WL with time. However, if WL is assumed to be negligible, Q_L may be approximated for wet or flood periods by an equation, given below:

$$Q_L = Q_D - Q_U \quad (6)$$

It should be noted that Equation 6 is based essentially upon individual "feel" that during flood or wet periods, for Q_{NET} in Equation 5 to be zero, the downstream structure may be operated in a manner to carry

QU and surface and sub-surface discharges in the channel from the flood plain of the reach in question (i.e., flood water or local inflow) to a downstream reservoir (Lake Okeechobee in our case).

The values of QL obtained by Equation 6 were distributed along the reach as

$$\frac{QL \times DIS}{DIST}$$

where DIS and DIST are the lengths of the sub-reach and the whole reach, respectively.

A constant Manning's roughness value of 0.029 was initially assumed to exist throughout the reach between S-65B and S-65E. The solution to Equation 2 was then obtained by an iterative procedure which used an equation based upon a numerical integration technique. The equation is

$$WSE_{i+1} = WSE_i + \frac{WSE_i + WSE_{i+1}}{2} dx \quad (7)$$

where WSE = water surface elevation,

$$\dot{WSE} = d(WSE)/dx$$

dx = horizontal distance between i^{th} and $(i+1)^{\text{th}}$ position
along the channel bed.

The TWE values computed at one hour intervals were fitted to the highest water mark (HWS) recorded during the flood period in each reach. The HWS values for reaches S-65E to S-65D, S-65D to S-65C, and S-65C to S-65B were 23.8, 32.2 and 39.85 feet, respectively. The fitting criterion was:

$$ABS(HWS_i - CTWE_i) \leq 0.1$$

where ABS = absolute value

$i = 1, 2, 3$ = reach number

CTWE = computed TWE.

In order to be able to do the fitting, the Manning's roughness values of the reach S-65D to S-65C and S-65C to S-65B were changed to 0.034 and 0.036, respectively. The fitting criterion was not met in the reach S-65C to S-65B and the ABS(HWS3-CTWE3) was ≤ 0.21 instead of 0.1. The hourly computed TWE values together with recorded HWE values for Structures 65B, 65C, 65D and 65E are presented in the appendix. Also, the computed fall difference between TWE value of the upstream structure and the HWE value of the downstream structure, is presented in the appendix.

3.4 Discharge Computation

Equation 4 is logarithmically transformed as

$$\ln(Q_N) = \ln a + b \ln(GO) + c \ln(EH) \quad (8)$$

in which \ln represents the natural logarithm. Using the data from the discharge rating curves, a multiple regression and correlation technique was employed to determine the constants, a , b , and c in Equation 8. The discharge equations thus developed for Structures 65E, 65D, 65C and 65B are presented in Table 2 together with their pertinent statistics. The synthesized values of TWE at S-65B, S-65C and S-65D and recorded values of TWE at S-65E together with recorded HWE at S-65B, S-65C, S-65D and S-65E were used to compute EH values for determining discharges through the respective structures. The hourly discharge through the structures, as computed by the equations presented in Table 2, are enclosed herewith in the appendix.

3.5 Storage Computation

The total storage (WATER) for any of the reaches at any time is computed by multiplying the appropriate area by the WSE values. The computation of area involved use of Simpson's rule, which did the integration along the section at 20 foot intervals. The computer outputs, consisting of QD-QU, DSTORE, QLAT and SUM for each of the three reaches at one-hour intervals, are enclosed herewith. The column QD-QU represents the average QL of two consecutive hours, DSTORE is the change in the water storage of the reach between two consecutive hours, QLAT represents the sum of QD-QU and DSTORE, and SUM is the cumulative sum of QLAT. All the units are in acre feet (AF).

3.6 Prescribed Operational Limits vs. Operations Performed

The limits within which operations should have been performed at the structures in question are as presented below:

Prescribed Operational Limits

Structure Number	Structure Discharge QLIMIT**	Maximum Headwater, HWM**	Maximum Difference in Head(EHL)* across the Structure
S-65B	QLIMIT \leq 587(TW-19.8')	\leq 44.9'	\leq 9.4'
S-65C	QLIMIT \leq 1020(TW-13.9')	\leq 38.1'	\leq 9.0'
S-65D	QLIMIT \leq 1127(TW-5.4')	\leq 32.5'	\leq 8.0'
S-65E	QLIMIT \leq 1453(TW+1.6')	\leq 24.2'	\leq 10.5'

* EHL is equal to the difference between maximum headwater (HWM) and minimum tailwater (TW).

** Elevations include appropriate datum corrections.

The basis used in developing the above limits are given in the appendix.

The results of operations performed, such as discharge through the structures (Q), headwater elevations (HWE) and difference in head across the structure (EH) were checked at one-hour intervals for the entire period (8:00AM October 1, 1969 through 1:00PM October 15, 1969) to find out the violations, if any, of the prescribed operational limits. The detected violations of the prescribed operational limits are given below. The design discharge through S-65B, S-65C, S-65D and S-65E is 14,000, 18,000, 21,300, and 24,000 cfs, respectively.

<u>(1) Structure Number</u>	<u>(2) Violation date and time</u>	<u>(3) Q>QLIMIT by (cfs)</u>	<u>(4) Col. 3 as % of design discharge</u>	<u>(5) HWE>HWM by (ft)</u>	<u>(6) EH>EHL by (ft)</u>
S-65B	Oct. 2, 10PM	297	2.12		
	Oct. 3, 2AM	72	0.51		
	9AM	320	2.29		
	10AM	551	3.94		
	11AM	53	0.38		
	8PM	34	0.24		
	9PM	58	0.41		
	11PM	4	0.03		
	12AM	30	0.21		
	Oct. 4, 1AM	3	0.03		
	6AM	622	4.44		
	7AM	47	0.34		
	8AM	119	0.85		
	11AM	11	0.08		
	12PM	47	0.34		
	1PM	55	0.39		
	10PM	50	0.36		
	Oct. 5, 8AM	10	0.07		
	9AM	37	0.26		
	10AM	56	0.40		
	11AM	44	0.31		
	12PM	33	0.24		

S-65C None

(1) Structure Number	(2) Violation date and time	(3) Q>QLIMIT by (cfs)	(4) Col. 3 as % of design discharge	(5) HWE>HWM by (ft)	(6) EH>EHL by (ft)
S-65D	Oct. 4, 8AM	78	0.37		
	9AM	236	1.11		
	10AM	380	1.78		
	11AM	514	2.41		
	12PM	672	3.15		
	1PM	804	3.77		
	2PM			0.29	
	3PM				0.05
S-65E	None				

The magnitude of the violations in discharge rates through S-65B and S-65D, expressed as percent of design discharge in column 4 above, is for all practical purposes within the limits of calculation error. This is also true for the violations in difference in head across Structure S-65D. Therefore, further efforts were made to evaluate the damages with an intention of pointing out the possible causes for such damages and, if possible, to make recommendations for prevention of damages in the future.

3.7 Damage Evaluation

The damage to the rip-rap downstream of S-65D was severe in comparison with that at the other structures (S-65B, S-65C and S-65E). Therefore, attempted evaluation of damages was limited only to S-65D. The damage pattern at S-65D presented in appendix 7.9 clearly indicates that rip-rap materials were transported from near the end of the apron and were accumulated at approximately 100+ feet distance from the end of the apron. A circle formed by the red dots on the left hand corner is simply to point out an approximate region where not only the cut-off wall was very much exposed but also the wing-wall was severely damaged. Another thing found by sending down a scuba diver was that the eroded surface had also caved in underneath the apron. Such damages are of major concern to the Flood Control District because of the effect of loss of rip-rap materials on the safety and integrity of the structures. Therefore, further efforts were made to investigate, qualitatively and quantitatively, into the causes of such damages.

3.7.1 Qualitative: The rip-rap displacement which occurred downstream of S-65D was apparently caused by an unusual high flow during the period of October 1 through October 15, 1969. The factors commonly expected to affect movement of rip-rap materials are gradation of stone sizes, depth of flow over stone, unit weight of stone and shape of individual stones. An underlying assumption here is that placement of the rip-rap materials was done and inspected under ideal conditions.

Inevitably, a better understanding is needed of the flow phenomena, specifically energy dissipation, which occur at these structures and onto the bed and bank protection below them at high discharges. Critically, but qualitatively speaking, the movement of rip-rap must also be

a function of the interactions among the factors affecting it. An ideal rip-rap composition, sizewise, would be a gradation which allows the large and small particles to interlock as much as possible. The resulting rock matrix would be more resistant than even one consisting of large uniform size stone. On the other hand, if a poor gradation were used, such as a few large boulders mixed with a majority of small crushed rock, an equivalent resistance would be for a uniform blanket of stone of smaller size. An example of this is given by Izbas and Khaldre (17) "fill material consisting of rocks of 1-2 ton size and occasional boulders up to 5 tons mixed with crushed rock and stone of various sizes --- this mass was equivalent to a uniform fill of stone 100-200kg size (equivalent velocity resistance)."

It is likely that the rip-rap held to its design expectations and an interlocking effect of gradation resisted until the velocities in the vicinity of the rip-rap reached or even far exceeded those the largest stone could resist individually. Then, the largest stones were finally displaced and rolled away at a rapid transport rate for some distance. The smaller stone immediately was transported along with a considerable depth of underlying sand. An alternative case would be that of a velocity segregated removal of rip-rap materials starting with relatively small rock, say 25-50 lbs. As the velocity or intensity of flow increased, the size of the rip-rap stone transported increased. Finally, the largest stones were left on various portions of the bed relatively unprotected and were moved at their expected critical velocities. These thoughts led to further search into the literature so that

some theoretical approaches could be utilized for quantitatively estimating the flow phenomena occurring downstream from S-65D.

3.7.2 Quantitative:

3.7.2.1 ~ Energy Dissipation.

An intensive review of the literature was undertaken concerning energy dissipation and the velocity of water needed to move the rip-rap materials. A listing of the references is enclosed herewith. Based upon the literature review a conceptual definition of the energy dissipation problem was made (Figure 2). The submerged jet and submerged hydraulic jump concepts are used when the water efflux through the gate is sub-critical and super-critical, respectively. The flow is sub-critical when the water efflux through the gate has a Froude number (F_1) less than unity and the flow is super-critical when the water efflux through the gate has a Froude number greater than unity.

Figure 2 illustrates the case of a jet with uniform velocity (assumed) U_1 , and depth, GOAV (average gate opening), issuing through a vertical lift gate situated over an ogee weir at a height, H , above the apron, where difference in head (Headwater elevation, HWE - Tailwater elevation, TWE) across the weir is the driving force and Y_T is the tailwater depth over the downstream apron. As water passes the gate, the jet curves towards the solid boundary due to the reduction of pressure below the jet, which is called the Coanda effect, and re-attaches to the bed at a certain section enclosing a region of separated flow. The pressure inside the eddying region (EL) will be less than

the hydrostatic pressure. Downstream of the re-attachment line, there will be an impingement zone where the pressure will be higher than the hydrostatic pressure. Due to the steep favorable pressure gradients existing in the impingement zone, the flow is accelerated and the high velocity filaments will be in the neighborhood of the bed. At the end of the impingement zone, the acceleration ceases and the high velocity stream undergoes turbulent walljet. This flow beyond the impingement region is designated herein as the "re-attached wall jet." The wall jet is defined as a jet of fluid impinging tangentially or at an angle on a boundary surrounded by stationary or moving fluid. The deflected jet impinges on the bed in the region surrounding the re-attachment line. In this region the pressures in excess of the hydrostatic pressure are built up over the bed. According to Rajaratnam and Subramanya (25) the position of the re-attachment line coincides fairly well with the position of the maximum pressure. The position would occur approximately at $(9.5 \times GOAV)$ feet downstream from the position of the jet. The velocity distribution at any point, x , downstream from the gate is assumed as shown in Figure 2a.

Figure 2b illustrates the case of a super-critical stream discharging from a slot, $GOAV$ (average gate opening) situated in the same way as shown in Figure 2a. If a normal hydraulic jump is to be formed at the efflux section where the depth is $GOAV$ and the Froude number is $F1$, the tailwater depth, YT , should be equal to the sub-critical sequent depth, $Y2$, given by the momentum equation. If YT is less than $Y2$, the jump is swept

downstream and is called a repelled jump. If Y_T is greater than Y_2 , the jump gets submerged or drowned as shown in Figure 2b and is called a submerged hydraulic jump, a drowned jump, or simply a submerged jump.

At the inlet section, there is a backing up and the depth is Y_3 . From this section forward, there is a continuous drop in water surface to a section of minimum depth of Y_5 , beyond which it increases continuously to the tailwater depth, Y_T . An intermediate drop in water surface is distinct for smaller submergences and levels off slowly for higher submergences; becoming almost level for the case of the submerged jet when the submergence factor is infinity.

3.7.2.1.1 - Mathematical Development

The submergence factor S for the submerged jump of supercritical depth $G O A V$ and Froude number F_1 is defined as

$$S = \frac{Y_T - Y_2}{Y_2} \quad (9)$$

If $S = 0$ normal jump would occur, $S \rightarrow \infty$ meaning the tailwater is too high as compared with Y_2 , and $S < 0$ meaning the tailwater is too low as compared with Y_2 and the jump would be swept downstream. The Froude number, F_1 , is determined as

$$F_1 = \sqrt{\frac{U_1}{G X G O A V}} \quad (10)$$

where G is acceleration due to gravity. If $F_1 = 1$, Equation 10 for $S=65D$ becomes

$$\frac{U_1}{\sqrt{G \cdot GOAV}} = 1$$

$$GOAV = \frac{(U_1)^2}{32.2} = \frac{(162 \times GOAV \times EH^{0.5})^2}{L^2 \times (GOAV)^2 \times 32.2} \quad (11)$$

where L = average net width of the gate = 27 feet for S-65D.

Simplifying Equation 11 yields $GOAV = 1.118(EH)$. (12)

Figure 3 is a graphical representation of Equation 12. The regions above and below the line representing Equation 12 will be the regions of occurrences of the submerged jet ($F_1 < 1.0$) and submerged hydraulic jump ($F_1 > 1.0$), respectively. The subcritical sequent depth, Y_2 , is determined from an equation based upon the momentum principle. The equation is

$$Y_2 = 1/2 (\sqrt{1 + 8(F_1)^2} - 1) GOAV \quad (13)$$

or

$$\frac{Y_2}{GOAV} = 1/2 (\sqrt{1 + 8(F_1)^2} - 1) \quad (14)$$

The tailwater depth, YT , is obtained as

$$YT = TWE - APE \quad (15)$$

where TWE is the tailwater elevation and APE is the apron elevation.

(a) Backed-up depth (Y_3): Define an inlet depth factor, ψ , as the ratio of backed-up depth Y_3 to the supercritical depth $GOAV$. Thus

$$\psi = \frac{Y_3}{GOAV} \quad (16)$$

Using the principles of continuity and momentum, ψ , can be shown to be a function of only F_1 and S .

Applying the momentum equation to the efflux section and

the end of the jump,

$$\frac{\gamma(Y_3)}{2} - \frac{\gamma(Y_T)}{2} = \frac{qY}{G} \left(\frac{q}{Y_T} - \frac{q}{GOAV} \right) \quad (17)$$

in which γ is the specific weight of water, q is the discharge per unit total net width of the gates. Mathematically, q is expressed as

$$q = \frac{Q}{N_1} \sum_{i=1}^{N_1} B_i \quad (18)$$

in which Q is the total discharge through the structure, N_1 is the total number of gates and B_i is the net width of the i^{th} gate. The total discharge through the structure is obtained as

$$Q = \sum_{i=1}^N a(GO_i)^b (HWE - TWE)^c \quad (19)$$

in which (GO_i) is the opening of the i^{th} gate and a , b , and c are constants. Substituting Equations 9 and 14 into Equation 17, using the equation of continuity, and simplifying results

$$\Psi = \left[\frac{(1+S)^2}{4} \left(\sqrt{1+8(F1)^2} - 1 \right)^2 - 2(F1)^2 + \frac{4(F1)^2}{(1+S)(\sqrt{1+8(F1)^2} - 1)} \right]^{0.5} = \Psi(F1, S) \quad (20)$$

Then the backed-up depth Y_3 is obtained from Equation 16 as

$$Y_3 = \Psi \times GOAV \quad (21)$$

(b) Minimum depth (Y_5): Figure 4 is a plot of $Y_5/GOAV$ against $F1$. The data was obtained from Figure 10 of Rao

and Rajaratnam (30). From Figure 4 data presented in Table 3 was obtained. This was necessary because the relationship given by Rao and Rajaratnam (30) could not be applied to the range of F_1 and S values occurring at Structure 650 during the period of investigation. Using the data in Table 3 an equation was developed by a multiple regression and correlation technique to determine $Y_5/GOAV$ as a function of F_1 and S . The equation is

$$Y_5/GOAV = -0.6297 - 0.9498F_1 + 1.3171S + 0.3754(F_1)^2 - 1.6S^2 + 2.2906(F_1)S \quad (22)$$

which has a coefficient of multiple determination, $R^2 = 0.997$ with a standard deviation, $\delta = 0.075$.

Then Y_5 is determined as

$$Y_5 = (Y_5/GOAV) GOAV \quad (23)$$

(c) Length of the Submerged Jump: (SJL) is determined by an equation due to Rao and Rajaratnam (30). The equation is

$$SJL = (4.9S + 6.1) Y_2 \quad (24)$$

(d) Energy Loss in the Submerged Jump: From Figure 2b, energy (E_1) at the efflux section could be written as

$$E_1 = Y_3 + \frac{U_1^2}{2G} \quad (25)$$

where $U_1 = q/GOAV$

The energy (E_4) at the end of jump is written as

$$E_4 = Y_T + \frac{(U_4)^2}{2G} \quad (26)$$

In which U_4 is the mean velocity at the end of the jump. Equation 26 can be expressed in terms of sequent depth, Y_2 , submergence factor, S , and discharge, q , per unit of total net width of the gate as

$$E_4 = (1 + S)Y_2 + \frac{1}{2G} \left(\frac{q}{(1+S) Y_2} \right)^2 \quad (27)$$

The energy loss (E) in the submerged jump is then given by

$$E = E_1 - E_4 \quad (28)$$

(e) Length of Eddy Region: The length of eddy region (EL) has been presented in Figure 4 of Rajaratnam and Subramanya (25) as a dimensionless plot against the nozzle size. The data was extracted from this figure and is presented in Table 4. Using this data an equation was developed as

$$\frac{EL}{H} = 3.7 (H/G0AV)^{-0.302} \quad (29)$$

which has a R^2 value of 0.93 and a standard deviation, σ , of 0.095.

Then EL is obtained as

$$EL = (EL/H)H \quad (30)$$

The height above the apron, H , is determined as

$$H = CREL - APE \quad (31)$$

where $CREL$ is the crest elevation.

(f) Velocity Decay: An excellent discussion about velocity decay of wall jets with downstream distance is available in (25). Therefore, only the equations used in determining

velocity at any downstream point are presented here. The data presented in Table 2 of Rajaratnam and Subramanya (25) were used in the development of the following equations. In the classical wall jet the minimum distance (X_1) beyond which the velocity profiles are similar is

$$X_1 = (13.0 + 2.83 \frac{H}{GOAV}) GOAV \quad (32)$$

In this region maximum velocity at any downstream point from the gate is determined by an equation developed by applying Legendre polynomial approximation. The equation is a fifth order polynomial and is

$$\begin{aligned} \frac{U_m}{U_1} = & 0.99155 + 0.00598 \frac{X_1}{GOAV} - 0.00192 \left(\frac{X_1}{GOAV} \right)^2 + \\ & 0.000077 \left[\frac{X_1}{GOAV} \right]^3 - 0.00000127 \left[\frac{X_1}{GOAV} \right]^4 + 0.0000000076 \\ & \left[\frac{X_1}{GOAV} \right]^5 \end{aligned} \quad (33)$$

where U_m is the maximum velocity at a downstream distance of X_1 from the gate.

In the region of re-attachment the emerging stream is not a wall jet but a curved plan turbulent free jet. The distance from the gate, X_2 , beyond which the decay of velocity would follow the same curve as that of classical wall jet is based upon the ratio of $H/GOAV$.

For $\frac{H}{GOAV} \leq 1.0$

$$\frac{X_2}{GOAV} = 25.28 \left(\frac{H}{GOAV} \right)^{0.4277} \quad (34)$$

For $\frac{H}{GOAV} > 1.0$

$$\frac{X_2}{GOAV} = 20.0 + \frac{50}{7} \frac{H}{GOAV} \quad (35)$$

The maximum velocity at any point between the region of X1 and X2 is determined as follows

For $\frac{H}{GOAV} \leq 1.4$

$$\begin{aligned} \frac{U_m}{U_1} = 1.0663 - 0.04484 \frac{X}{GOAV} + 0.00263 \left(\frac{X}{GOAV} \right)^2 - \\ 0.00000778 \left(\frac{X}{GOAV} \right)^3 + 0.00000097 \left(\frac{X}{GOAV} \right)^4 - 0.0000000038 \\ \left(\frac{X}{GOAV} \right)^5 \end{aligned} \quad (36)$$

where X is any point in the region X1 and X2.

$$\begin{aligned} \frac{U_m}{U_1} = 1.0754 - 0.0354 \left(\frac{X}{GOAV} \right) - 0.001103 \left(\frac{X}{GOAV} \right)^2 + \\ 0.000204 \left(\frac{X}{GOAV} \right)^3 - 0.00000711 \left(\frac{X}{GOAV} \right)^4 + 0.0000000767 \\ \left(\frac{X}{GOAV} \right)^5 \end{aligned} \quad (37)$$

Height from the bottom of the bed, YX, at which the U_m at any downstream point is determined, is as follows

For $\frac{H}{GOAV} > 1.4$

$$\frac{\delta l}{GOAV} = 2.2558 - 0.3784 \frac{X_3}{GOAV} + 0.00205 \left(\frac{X_3}{GOAV} \right)^2 \quad (38)$$

in which X_3 is any downstream point from the gate and δl is the height from the bottom of the bed at which the velocity equals $\frac{U_m}{2}$.

For $\frac{H}{GOAV} \leq 1.4$

$$\frac{\delta_1}{GOAV} = 3.3195 - 0.048 \frac{X_3}{GOAV} + 0.00188 \left(\frac{X_3}{GOAV} \right)^2 \quad (39)$$

$$\text{Then } \delta_1 = \left[\frac{\delta_1}{GOAV} \right] GOAV \quad (40)$$

$$\text{and } YX = 0.2\delta \quad (41)$$

3.7.2.1.2 - Computation of Velocity for Moving Rip-Rap Materials

A considerable body of work is available which could help in computing or inferring the velocity of water needed for moving rip-rap materials. One of the commonly used relations is the formula of Izbas (17). The formula is

$$V_{cr} = 0.86 \sqrt{\frac{2G(W_s - W)}{W}} ds \quad (42)$$

where V_{cr} = the maximum velocity a given size and characteristic stone can endure and still remain in place, in ft/sec,

G = acceleration due to gravity, in ft/sec/sec,

W_s = unit weight of the stone, in lbs/ft³,

W = unit weight of water, in lbs/ft³,

ds = diameter of the stone, in ft.

If $W_s = 160$ lbs/ft³, $w = 62.4$ lbs/ft³, $G = 32.2$ ft/sec.² and

$ds = 1.5$ ft, then $V_{cr} = 10.6$ ft/sec (from Equation 42).

Mean velocity for 'first displacement' of bed material is determined with an equation developed by Neill (22). The equation is

$$\frac{(WMC)^2}{G(SG-1)DG} = 2.5 \left(\frac{d}{DG} \right)^{0.2} \quad (43)$$

where WMC = competent mean velocity for 'first displacement' of bed material,

SG = specific gravity,

DG = effective diameter of bed grains, and

d = depth of flow.

The velocity that would roll the first rock was found from the nomogram of Equation 43 to be 12.7 ft/sec to 13.2 ft/sec depending upon the values used for specific gravity, size of rip-rap materials and the depth of flow. An effective specific gravity of the rip-rap materials was found to be 2.0 to 2.4. Similarly, effective size of the rip-rap materials was found to be 14 to 12 inches. An average value for the depth of flow used in the computation was tailwater depth, YT, of 16 to 17 ft. Neill (22) has discussed the limitations of Equation 43.

3.8 Results and Discussion

The computed TWE at S-65D, S-65C and S-65B are consistent with the computed QL values, that is, increases and decreases in QL values reflect increases and decreases in computed fall (COMP DH = difference in computed TWE values of upstream structure and observed HWE values of downstream structure) values for the reach. The observed fall (OBS DH = difference in observed TWE values of upstream structure and observed HWE values of downstream structure) values do not show such a consistency with the QL values. This may be because of the discharges through Structures 65D, 65C and 65B are computed by using the computed TWE values.

A simultaneous occurrence of negative values in QD - QU and DSTORE columns seem to contradict the fact that additions of water into the reach should reflect an increase in WSE values if the WL values are negligible. However, such occurrences are only four (October 4 on the 14th hour, and October 12 on the 17th, 18th, and 19th hours). Also, it seems that estimation of QL by Equation 6 may not be too far from reality particularly during wet or flood periods in controlled systems like the lower Kissimmee River Basin.

Investigations concerning energy dissipation and velocity for moving rip-rap materials were limited to S-65D only. Almost all the mathematical relationships presented concerning energy dissipation and velocity for moving rip-rap materials are based upon model studies. Thus a main assumption involved herein is that information obtained from the model could be applied to S-65D without introducing much error

in the results. One of the major questionable aspects may be the variation in surface roughness characteristics of the prototype and the model. However, Rouse (32) indicates that effects of surface roughness on the behavior of the submerged jump or jet is not well understood and information available pertains only to smooth surfaces. The computation was done at one hour intervals. Whenever the jump occurred the Froude number, F_1 , was never greater than 1.3 indicating a minimum jump condition. The energy loss in the jump was in the neighborhood of 10%. The length of the jump varied between 83 to 87 feet indicating that if the jump occurred immediately past the gate, then the sub-critical sequent depth, Y_2 , was occurring on the level portion of the rip-rap. The results may appear a little too much biased against using the submerged jump as the energy dissipator, but the literature (10) seems to support the fact that a submerged jump may be a poor energy dissipator as compared with a free jump. Also, Elevatorski (13) indicates a fear with the submerged jump that a high velocity might travel along the bed, without much retardation, to considerable distances, thereby causing scour.

Using the plane turbulent jet concept, velocities at 78 and 97 ft. distances from the gate were computed. The 78 foot distance from the gate means 6 1/2 inches past the end sill on the level rip-rap section, and 97 feet from the gate means 6 1/2 inches before the end of the level rip-rap section.

The point at 78 ft. distance was assumed to represent the channel condition of the apron and the point at 97 ft. distance was assumed to represent the channel condition of the rip-rap section. The maximum

velocities that occurred at the point 97 feet from the gate during the flood period (October 3 through October 7, 1969) were in the order of 13 to 15.8 feet per second with 15+ feet per second, which is greater than the upper limit (13.2 ft/sec) of velocity needed to roll the rocks, occurring during 6:00AM through 5:00PM on October 4, 1969. The maximum velocities occurring at the point 78 feet from the gate were greater by 0.3 to 0.4 ft/sec than those occurring at 97 feet.

The heights from the bed at which the above referred maximum velocities occurred at 97 feet distance varied between 4 to 7.3 feet. These heights were always less by 0.1 foot as compared with those at 78 ft. distance. Therefore, it appears that at distances, X_1 , greater than 97 ft. the maximum velocity would occur still closer to the bed if there were no change in the channel configuration. If the area of the channel increased due to channel expansion, then depth of flow would be smaller which would further push the maximum velocity closer to the bed. However, the magnitude of the maximum velocity would tend to decrease with increasing downstream distance. Also, there may be some effect of increasing bed slope and changing roughness. It would be difficult to guess the effect on the magnitude of the maximum velocities and the heights from the bed at which they would occur.

4. SUMMARY AND CONCLUSIONS

An unusual rainfall event (9.33, 9.66 and 8.82 inches at Structures 65B, 65C, 65D, respectively) which resulted in a severe flood during the first week of October 1969, caused considerable damage to the rip-rap channel sections downstream of the control structures, particularly at S-65D, in Canal 38. To analyze the situation data were collected, assumptions were made and mathematical relationships were developed.

Due to the inability of the computer program to handle negative elevations, a constant of twelve feet was added to each elevation in the cross-sections data (S-65B to S-65C, design; and S-65C to S-65D and S-65D to S-65E, as built). Using a sixth order Legendre polynomial approximation, functional relationships were developed between section factor and water surface elevation for each of the cross-sections. A datum correction of 0.1, 0.5 and 0.4 foot was applied at Structures 65D, 65C and 65B, respectively. The recorded TWE at S-65E and the recorded HWE at S-65E, S-65D, S-65C and S-65B were assumed satisfactory. Assuming the structure discharge rating curves provided by the Corps of Engineers at Jacksonville, Florida, to be satisfactory, equations were developed to compute discharge through each of the structures as a function of gate operation and difference in head across the structures.

The TWE values were computed at S-65D, S-65C, and S-65B at one hour intervals for the period 8:00AM October 1, 1969 through 1:00PM October 15, 1969 by employing the mathematical relationships based upon the principles of gradually varied flow. The Manning's roughness values of 0.029, 0.034 and 0.036 were used for reaches S-65E to S-65D, S-65

to S-65C and S-65C to S-65B, respectively. The computed TWE values were fitted to the highest water mark (HWS) values of 23.8, 32.2, and 39.85 feet for reaches S-65E to S-65D, S-65D to S-65C, and S-65C to S-65B, respectively.

A comparison of the operations performed with the prescribed operational limits led to further investigation of energy dissipation phenomena and the velocity required for moving rip-rap materials at S-65D only. Two phenomena of energy dissipation, submerged hydraulic jump and submerged jet, were investigated. A submerged jump occurred if the Froude number, F_1 , of water efflux through the gate was greater than unity. It was assumed that a submerged jet would occur if F_1 was less than unity. Appropriate mathematical relationships were developed to compute the velocity of water at distances of 78 and 97 feet downstream of the gate. The 78 ft. distance downstream means 6 1/2 inches past the end sill on the level rip-rap section and the 97 ft. distance downstream means 6 1/2 inches before the end of the level rip-rap section. The 78 and 97 ft. distances were assumed to represent the channel conditions of the apron and rip-rap, respectively. The works of Rajaratnam and Subramanya (25) and Rao and Rajaratnam (30) were assumed to be applicable without introducing much error in this investigation.

The computation of velocity for moving the rip-rap materials was based upon a combination of such factors as size and weight or specific gravity of the rip-rap materials and depth of flow of water on the bed.

A very high correlation coefficient, R^2 , value and a very low standard error of estimate associated with each of the discharge equations indicate that they approximate the structure discharge rating curves very

well. The computed TWE values in reaches S-65E to S-65D and S-65D to S-65C are within 0.1 foot of the observed high water marks whereas in the reach S-65C to S-65B the TWE values are within 0.21 foot of the observed high water mark. The computed TWE values at S-65D, S-65C and S-65B are consistent with the computed QL values; that is, increases or decreases in QL values reflect increases and decreases in computed fall (COMP DH) values for the reach.

The magnitude of violation in discharges through S-65B and S-65D, expressed as a percent of design discharge, is for all practical purposes within the limits of calculation error. This is also true for the violations in difference in head across S-65D.

Whenever the jump occurred the Froude number, F_1 , was never greater than 1.3 indicating a minimum jump condition. The energy loss in the jump was computed to be in the neighborhood of 10 percent. The length of the jump varied between 83 and 87 feet indicating that if the jump occurred immediately past the gate, the sub-critical sequent depth, Y_2 , was occurring on the level portion of the rip-rap.

The maximum velocities that occurred at the point 97 feet downstream from the gate during the flood period (October 3 through October 7, 1969) were in the order of 13 to 15.8 feet per second with 15+ feet per second occurring during the period 6:00AM through 5:00PM on October 4, 1969. The maximum velocities occurring at the point 78 feet from the gate were greater by 0.3 to 0.4 feet per second than those occurring at 97 feet. The heights from the bed at which the above maximum velocities occurred at 97 feet distance varied between 4 to 7.3 feet. These heights were always less by 0.1 foot as compared with those at 78 feet distance.

Depending upon the method or equation used, the rip-rap materials at S-65D would start rolling with water velocities between 10.6 to 13.2 feet per second.

Based upon the above findings the following conclusions can be drawn:

1. Within the limits of the data used and assumptions made, it is clear that for all practical purposes the Flood Control District did not violate the prescribed operational limits on any of the structures (S-65B, S-65C, S-65D or S-65E) in question.
2. Water velocities greater than that required to displace the rip-rap materials at S-65D apparently occurred for several days.

In order to prevent such damages in the future, some recommendations for further investigations are made in the next section.

5. RECOMMENDATIONS

Based upon the results of this analysis, it is recommended that further investigations be made, as follows:

1. Investigation of energy dissipation phenomena such as submerged hydraulic jump and submerged jet for spillway structures having low head, high discharge, and high tailwater conditions for submerged flow.
2. Review of the structure discharge rating curves. It may be likely that the structures are discharging at rates in excess of those values indicated by the rating curves under a given set of conditions.
3. Investigation of the life of rip-rap materials as affected by time and flow conditions.
4. Alternative ways of laying the rip-rap blankets.
5. Effects of channel transitions (expansion and contractions) and channel surface roughness created by rip-rap materials on flow phenomena.

These investigations can best be undertaken by means of conducting an appropriate series of model studies.

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APPENDICES

Explanatory notes for Appendices

7.1 through 7.6

x^i = Rainfall stations where $i = 1, 2, \dots, 21, 22$, with 17 and 18 missing. A listing of these rainfall stations are as below:

i	Station Name	i	Station Name
1	Structure 65	11	Structure 65D
2	Yeehaw Jct.-7W	12	Okeechobee Field Station
3	Structure 65A	13	Structure 65E
4	Lake Arbuckle	14	Brighton
5	Avon Park Bombing Range	15	Hurricane Gate H.G.S.#6
6	Structure 65B	16	Rocking K Ranch
7	Fort Pierce-3W	19	Lake Placid-2SW
8	Structure 65C	20	Cornwell-4NW
9	Structure 68	21	Fort Drum-5NW
10	Highland Park Estates	22	Avon Park

x^1 = Structure 65

x^3 = Structure 65A

x^6 = Structure 65B

x^8 = Structure 65C

x^{11} = Structure 65D

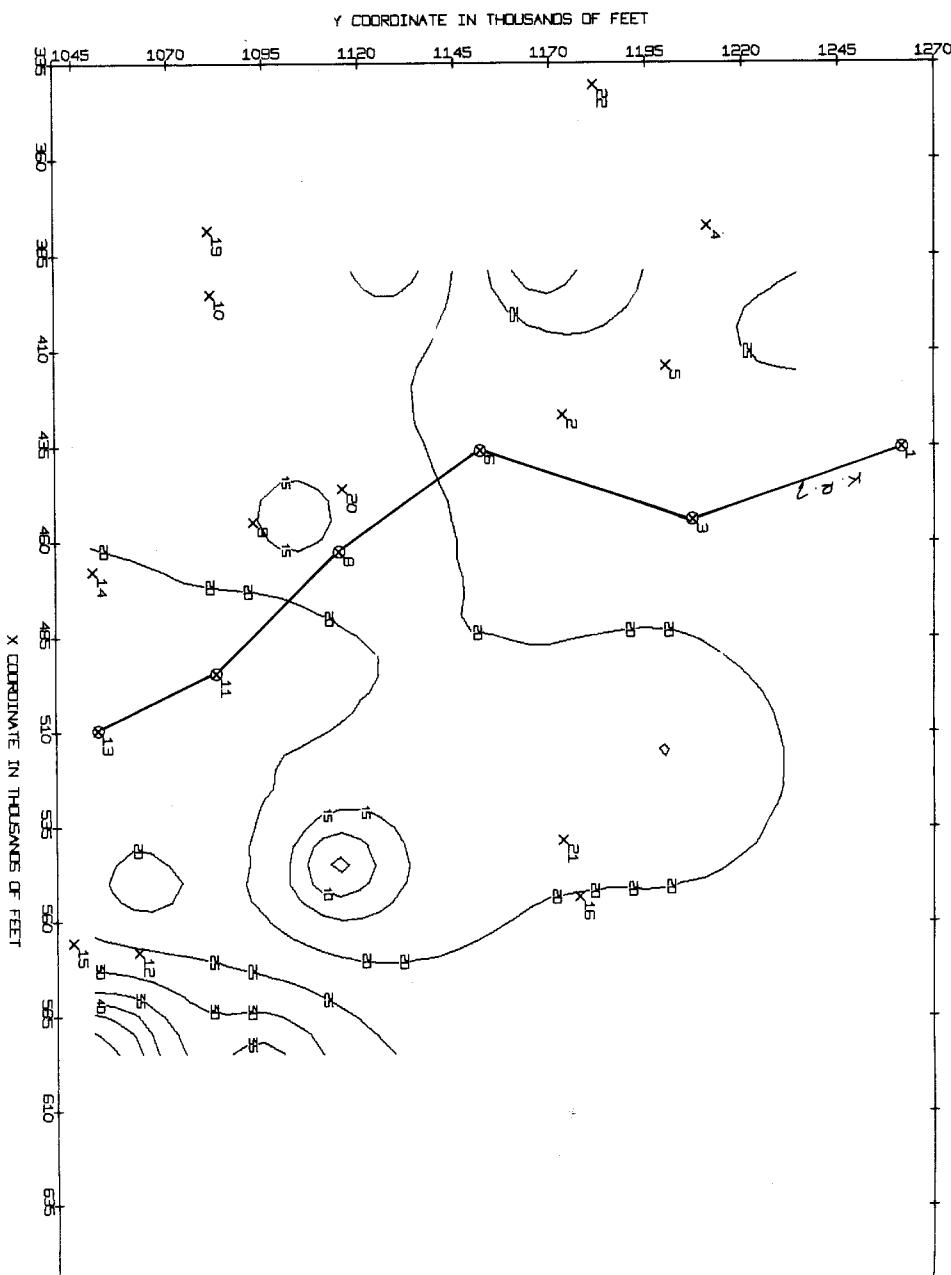
x^{13} = Structure 65E

Contour annotations are to be divided by 10 and they are in inches.

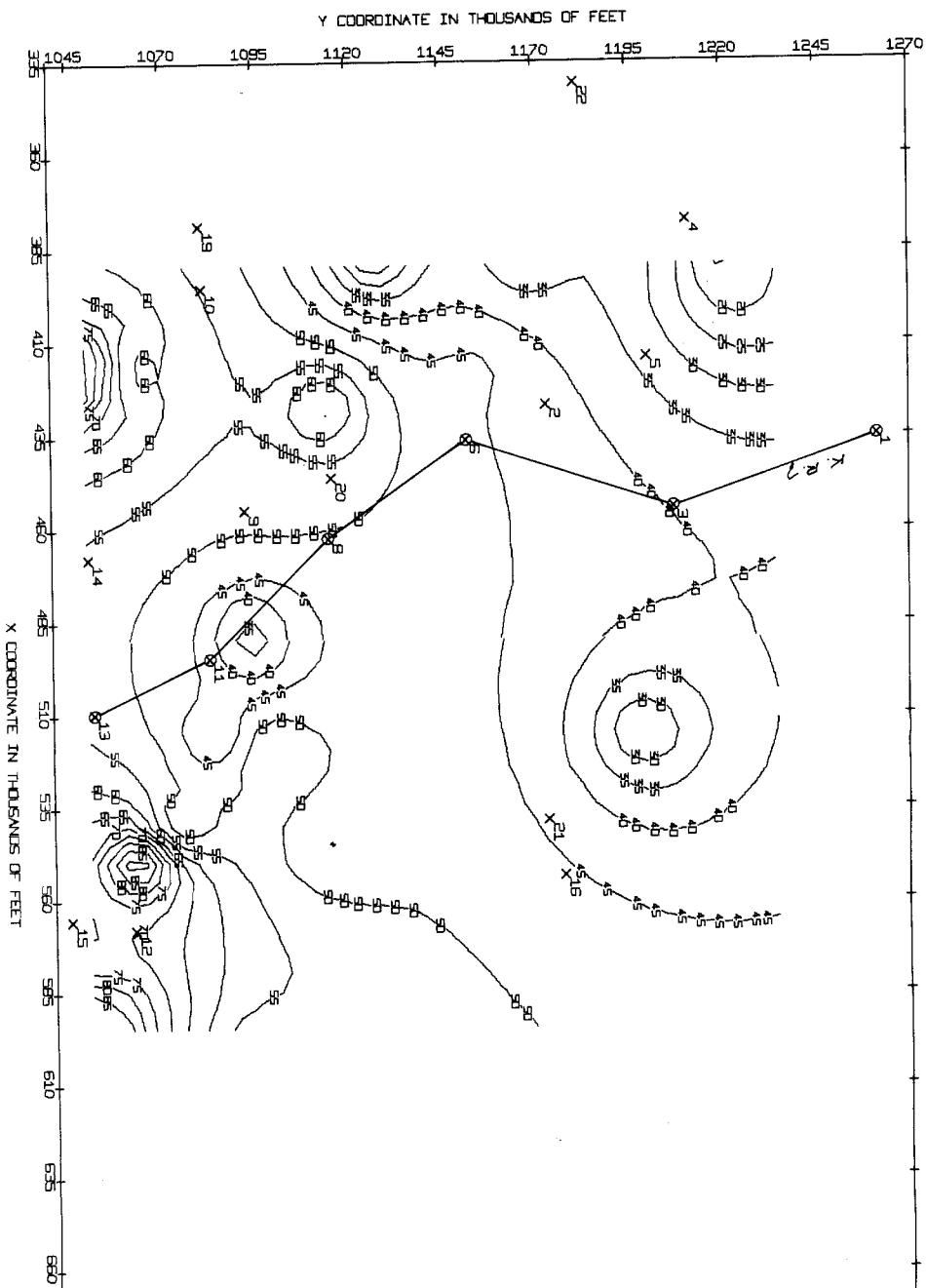
Contour interval is 0.5 inch.

Contours not annotated are either equal to the first neighboring annotated contour or are greater than or less than the first neighboring contour by the contour interval.

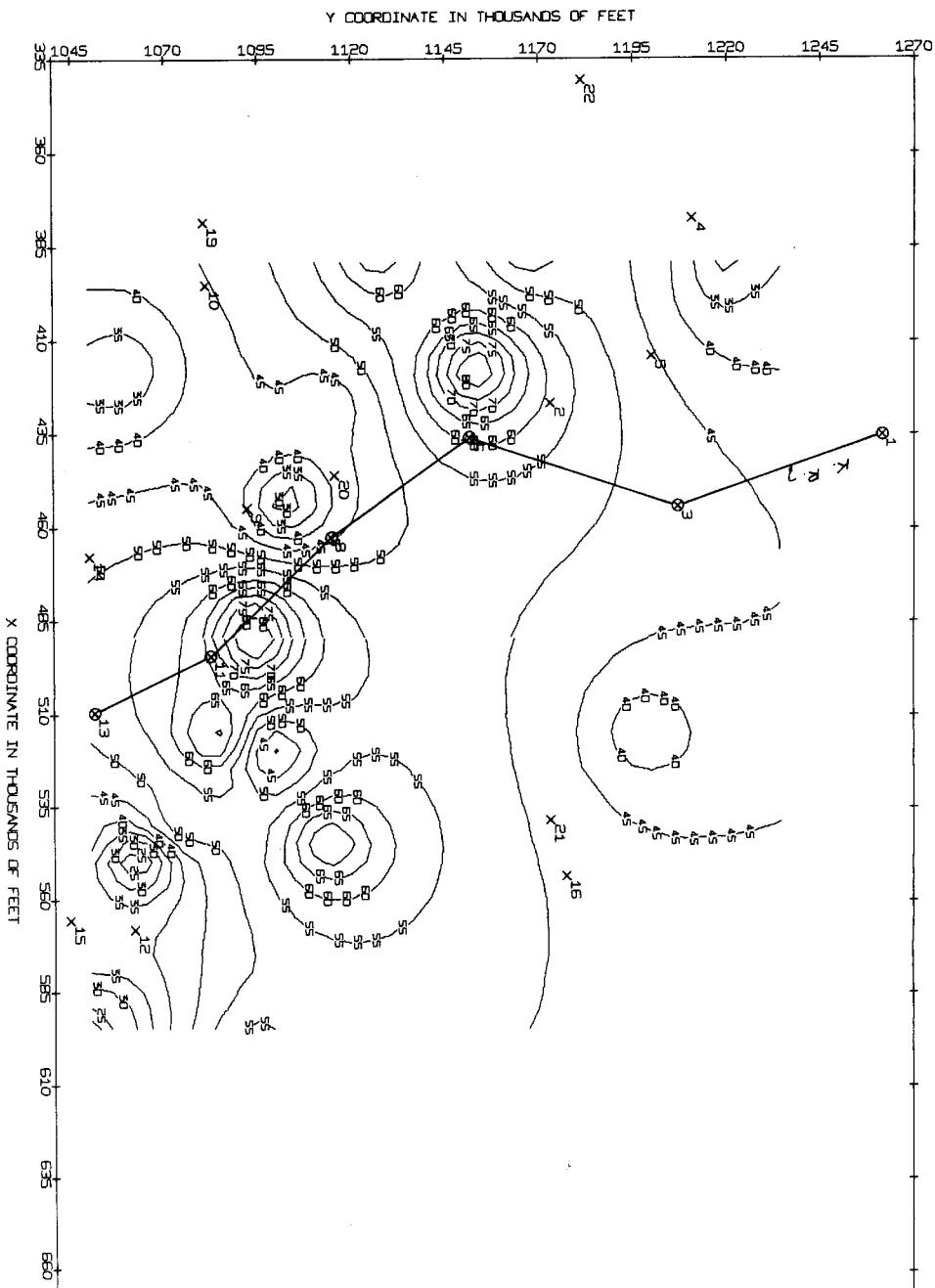
K.R. = Kissimmee River



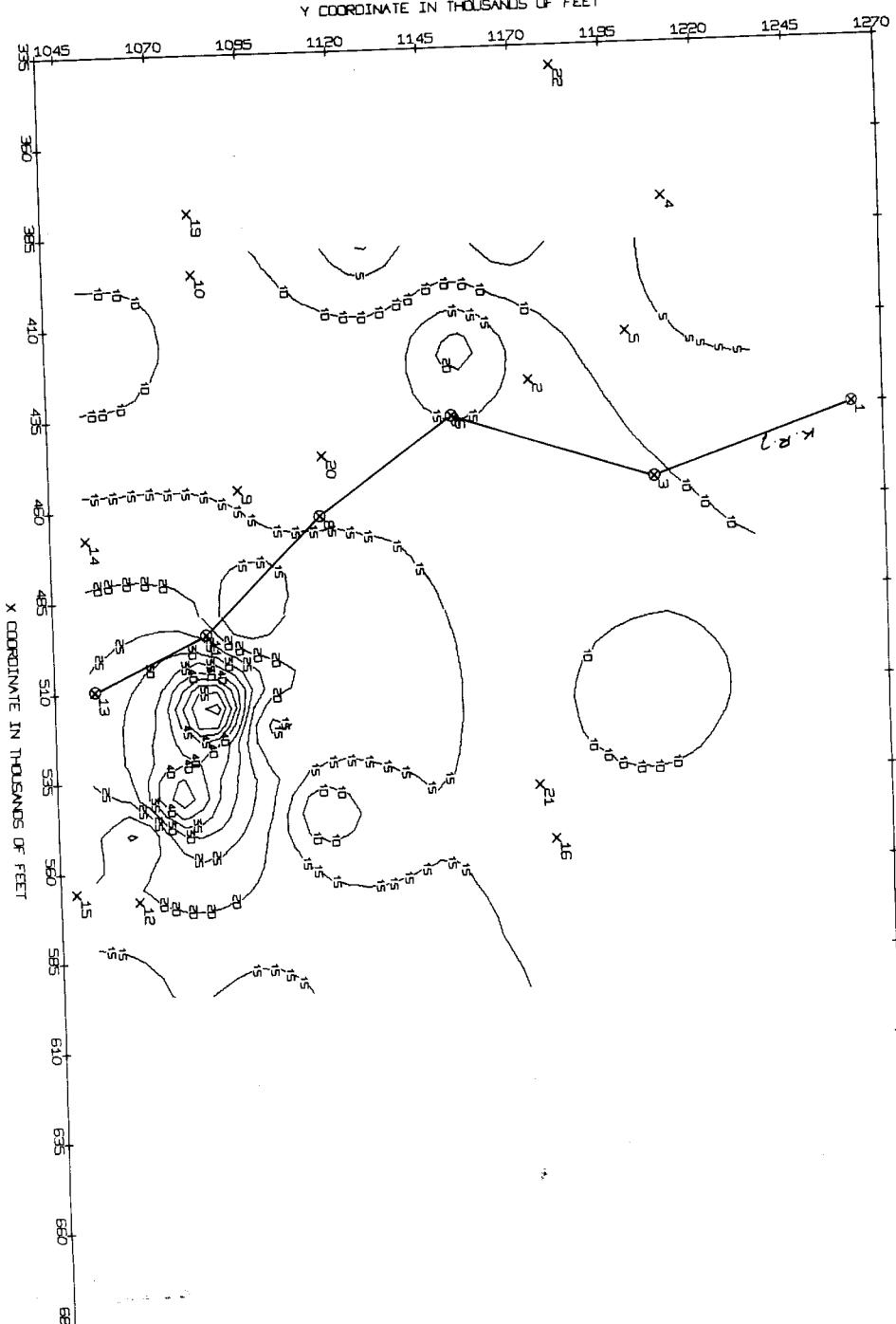
7.1 ISOHYETAL GRAPH FOR SEPT 6 THRU SEPT 17 - 1969 CUMULATED RAINFALL
PG. 48



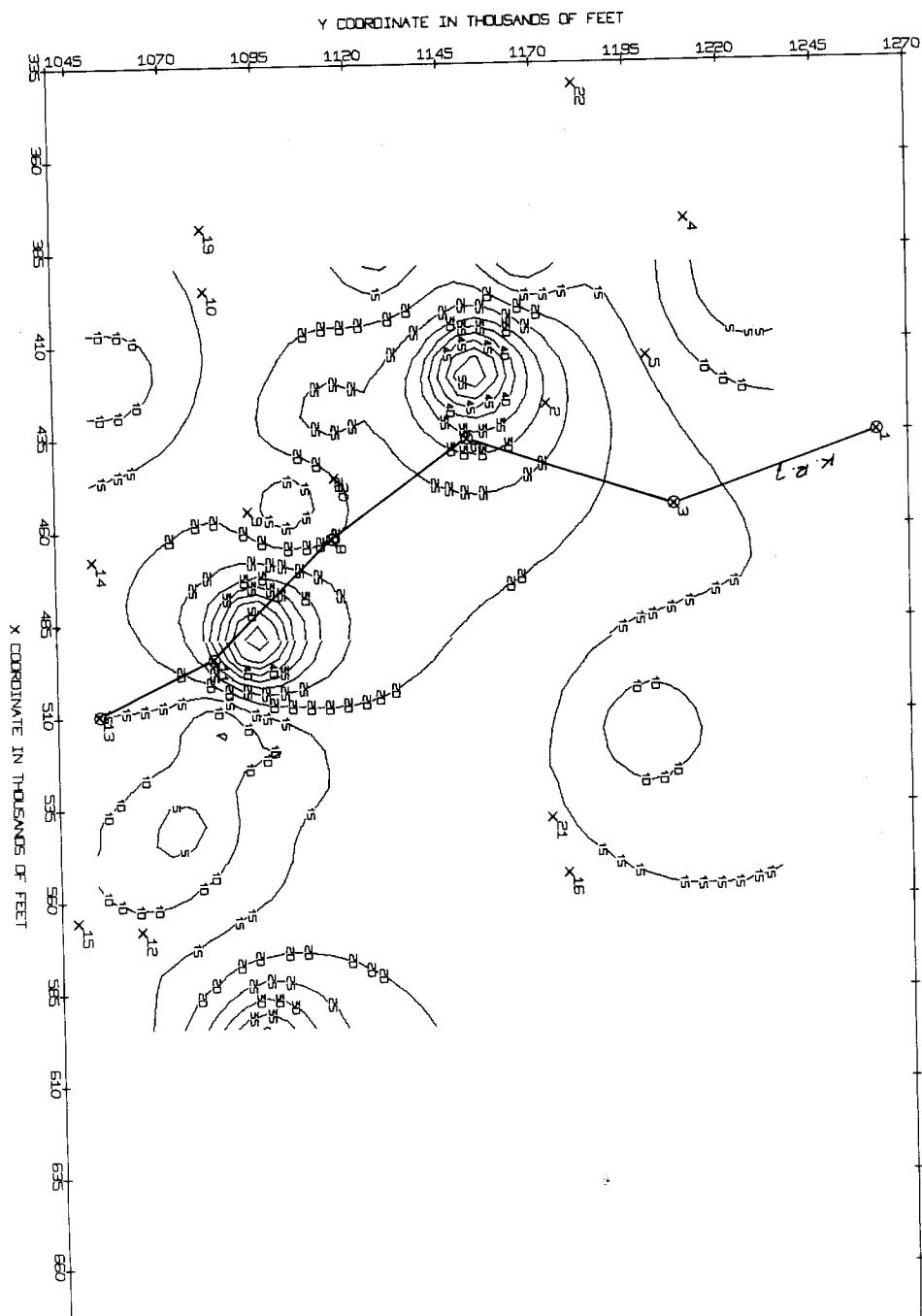
7.2 ISOHYETAL GRAPH FOR SEPT 18 THRU SEPT 30 - 1969 CUMULATED RAINFALL



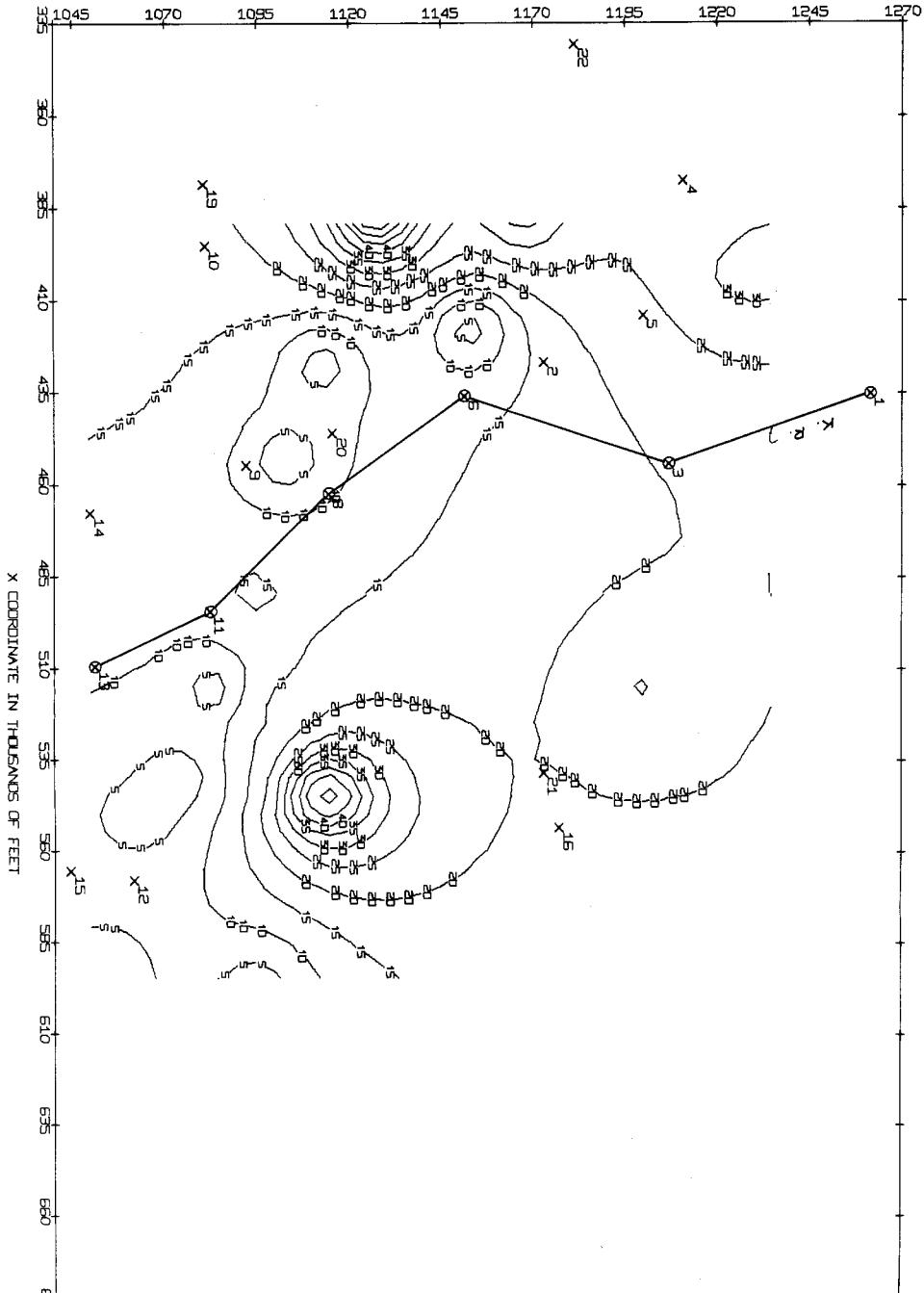
7.3 ISOHYETAL GRAPH FOR OCT 1 THRU OCT 3 - 1969 CUMULATED RAINFALL



7.4 ISOHYETAL GRAPH FOR OCT 1, 1969 - DAILY RAINFALL
Pg. 51



Y COORDINATE IN THOUSANDS OF FEET



7.7 Data Used in Developing Isohyetal Maps

Rainfall Station	Cumulative Rainfall (in.) Sept. 6-17, 1969	Cumulative Rainfall (in.) Sept. 18-30, 1969	Cumulative Rainfall (in.) October 1-3, 1969	Rainfall (in.) Oct. 1, 1969	Rainfall (in.) Oct. 2, 1969	Rainfall (in.) Oct. 3, 1969
Structure 65	3.95	5.08	5.83	1.19	4.64	0.00
Structure 65A	0.00	4.32	8.00	0.20	1.70	6.10
Lake Arbuckle	1.61	10.40	1.32	0.92	0.40	0.00
Ft. Pierce	4.25	6.91	1.40	0.10	1.30	0.00
Brighton	1.13	2.23	6.79	0.00	1.02	5.77
Okeechobee Field Sta.	2.86	2.08	3.93	0.00	0.15	3.78
Highlands Park Estates	1.50	10.98	3.39	0.61	0.72	2.06
Structure 65E	3.44	3.11	4.33	0.17	0.63	3.53
Indian Lake Forestry Tower	5.44	9.37	2.16	1.03	1.13	0.00
Avon Park Bombing Range	2.23	3.71	5.83	5.33	0.00	0.00
Yee-Haw Junction	2.63	3.69	7.75	7.75	0.00	0.00
Structure 65B	2.13	2.84	9.45	0.55	7.15	1.65
Structure 65D	2.15	4.64	8.95	2.35	6.55	0.05
Structure 68	1.97	6.83	4.16	1.20	2.80	0.06
Avon Park	1.91	5.80	3.12	0.57	0.85	1.70
Cornewell	1.00	5.08	2.42	1.42	1.00	0.00
Fort Drum	1.44	2.46	3.57	0.51	0.49	2.57
Lake Placid	1.98	3.97	2.92	0.36	0.69	1.37
HGS-6	2.18	1.15	2.58	0.00	2.52	2.52

7.8 Hourly gate operations at S-65B, S-65C, S-65D and S-65E
for the period October 1 (8:00AM) through October 15,
(1:00PM), 1969.

Explanatory notes pertaining to the listings.

S-65E refers to the specific structure name.

Gate No. refers to the number of gates = 1, 2, 3, 4, 5, 6

S-65E has 6 gates; S-65D and S-65C have 4 gates and S-65B
has 3 gates.

Time = 1, 2, 3,..., 340, 341, 342 hours.

1st hour corresponds to 8:00AM of October 1, 1969, and 342nd
hour corresponds to 1:00PM of October 15, 1969.

Data listing is of gate operations in feet.

S-65B

Time	Gate 1	Gate 2	Gate 3			
1	3.25	3.25	3.25	0.00	0.00	0.00
2	3.25	3.25	3.25	0.00	0.00	0.00
3	3.25	3.25	3.25	0.00	0.00	0.00
4	3.25	3.25	3.25	0.00	0.00	0.00
5	3.25	3.25	3.25	0.00	0.00	0.00
6	3.25	3.25	3.25	0.00	0.00	0.00
7	3.25	3.25	3.25	0.00	0.00	0.00
8	3.25	3.25	3.25	0.00	0.00	0.00
9	3.25	3.25	3.25	0.00	0.00	0.00
10	3.50	3.50	3.50	0.00	0.00	0.00
11	3.75	4.00	4.00	0.00	0.00	0.00
12	3.75	4.00	4.00	0.00	0.00	0.00
13	3.75	4.00	4.00	0.00	0.00	0.00
14	4.00	4.50	4.00	0.00	0.00	0.00
15	4.00	4.50	4.00	0.00	0.00	0.00
16	4.00	4.50	4.00	0.00	0.00	0.00
17	4.00	4.50	4.00	0.00	0.00	0.00
18	4.00	4.50	4.00	0.00	0.00	0.00
19	4.00	4.50	4.00	0.00	0.00	0.00
20	4.00	4.50	4.00	0.00	0.00	0.00
21	4.00	4.50	4.00	0.00	0.00	0.00
22	4.00	4.50	4.00	0.00	0.00	0.00
23	4.00	4.50	4.00	0.00	0.00	0.00
24	4.50	5.00	4.50	0.00	0.00	0.00
25	4.50	5.00	4.50	0.00	0.00	0.00
26	4.50	5.00	4.50	0.00	0.00	0.00
27	4.50	5.00	4.50	0.00	0.00	0.00
28	4.50	5.00	4.50	0.00	0.00	0.00
29	4.50	5.00	4.50	0.00	0.00	0.00
30	4.50	5.00	4.50	0.00	0.00	0.00
31	4.50	5.00	4.50	0.00	0.00	0.00
32	4.50	5.00	4.50	0.00	0.00	0.30
33	4.50	5.00	4.50	0.00	0.00	0.00
34	5.00	5.00	5.00	0.00	0.00	0.00
35	6.00	6.00	6.00	0.00	0.00	0.00
36	6.00	6.00	6.00	0.00	0.00	0.00
37	8.00	8.00	8.00	0.00	0.00	0.00
38	9.50	9.50	9.50	0.00	0.00	0.00
39	11.00	11.00	11.00	0.00	0.00	0.00
40	12.00	12.00	12.00	0.00	0.00	0.00
41	12.00	12.00	12.00	0.00	0.00	0.00
42	12.00	12.00	12.00	0.00	0.00	0.00
43	12.00	12.00	12.00	0.00	0.00	0.00
44	13.00	13.00	13.00	0.00	0.00	0.00
45	13.00	13.00	13.00	0.00	0.00	0.00
46	13.00	13.00	13.00	0.00	0.00	0.00

S-65B(Contd)	Gate 1	Gate 2	Gate 3		
47	13.00	13.00	13.00	0.00	0.00
48	13.00	13.00	13.00	0.00	0.00
49	13.00	13.00	13.00	0.00	0.00
50	13.00	13.00	13.00	0.00	0.00
51	12.00	12.00	12.00	0.00	0.00
52	12.00	12.00	12.00	0.00	0.00
53	12.00	12.00	12.00	0.00	0.00
54	12.00	12.00	12.00	0.00	0.00
55	12.00	12.00	12.00	0.00	0.00
56	12.00	12.00	12.00	0.00	0.00
57	12.00	12.00	12.00	0.00	0.00
58	12.00	12.00	12.00	0.00	0.00
59	12.00	12.00	12.00	0.00	0.00
60	12.00	12.00	12.00	0.00	0.00
61	12.00	12.00	12.00	0.00	0.00
62	12.00	12.00	12.00	0.00	0.00
63	12.00	12.00	12.00	0.00	0.00
64	12.00	12.00	12.00	0.00	0.00
65	12.00	12.00	12.00	0.00	0.00
66	12.00	12.00	12.00	0.00	0.00
67	12.00	12.00	12.00	0.00	0.00
68	12.00	12.00	12.00	0.00	0.00
69	12.00	12.00	12.00	0.00	0.00
70	12.00	12.00	12.00	0.00	0.00
71	12.00	12.00	12.00	0.00	0.00
72	12.00	12.00	12.00	0.00	0.00
73	12.00	12.00	12.00	0.00	0.00
74	12.00	12.00	12.00	0.00	0.00
75	12.00	12.00	12.00	0.00	0.00
76	12.00	12.00	12.00	0.00	0.00
77	12.00	12.00	12.00	0.00	0.00
78	12.00	12.00	12.00	0.00	0.00
79	12.00	12.00	12.00	0.00	0.00
80	12.00	12.00	12.00	0.00	0.00
81	12.00	12.00	12.00	0.00	0.00
82	12.00	12.00	12.00	0.00	0.00
83	12.00	12.00	12.00	0.00	0.00
84	12.00	12.00	12.00	0.00	0.00
85	12.00	12.00	12.00	0.00	0.00
86	12.00	12.00	12.00	0.00	0.00
87	12.00	12.00	12.00	0.00	0.00
88	11.50	11.50	11.50	0.00	0.00
89	11.50	11.50	11.50	0.00	0.00
90	11.50	11.50	11.50	0.00	0.00
91	11.50	11.50	11.50	0.00	0.00
92	11.50	11.50	11.50	0.00	0.00
93	11.50	11.50	11.50	0.00	0.00
94	11.50	11.50	11.50	0.00	0.00
95	11.50	11.50	11.50	0.00	0.00
96	11.50	11.50	11.50	0.00	0.00
97	11.50	11.50	11.50	0.00	0.00
98	11.50	11.50	11.50	0.00	0.00
99	11.50	11.50	11.50	0.00	0.00
100	11.50	11.50	11.50	0.00	0.00
101	11.50	11.50	11.50	0.00	0.00
102	11.50	11.50	11.50	0.00	0.00
103	11.50	11.50	11.50	0.00	0.00
104	11.50	11.50	11.50	0.00	0.00
105	11.50	11.50	11.50	0.00	0.00

S-65B (Contd)

	<u>Gate 1</u>	<u>Gate 2</u>	<u>Gate 3</u>			
106	11.50	11.50	11.50	0.00	0.00	0.00
107	11.50	11.50	11.50	0.00	0.00	0.00
108	11.50	11.50	11.50	0.00	0.00	0.00
109	11.50	11.50	11.50	0.00	0.00	0.00
110	11.50	11.50	11.50	0.00	0.00	0.00
111	11.50	11.50	11.50	0.00	0.00	0.00
112	11.50	11.50	11.50	0.00	0.00	0.00
113	11.50	11.50	11.50	0.00	0.00	0.00
114	11.50	11.50	11.50	0.00	0.00	0.00
115	11.50	11.50	11.50	0.00	0.00	0.00
116	11.50	11.50	11.50	0.00	0.00	0.00
117	11.50	11.50	11.50	0.00	0.00	0.00
118	11.50	11.50	11.50	0.00	0.00	0.00
119	11.50	11.50	11.50	0.00	0.00	0.00
120	11.50	11.50	11.50	0.00	0.00	0.00
121	11.50	11.50	11.50	0.00	0.00	0.00
122	11.50	11.50	11.50	0.00	0.00	0.00
123	11.50	11.50	11.50	0.00	0.00	0.00
124	11.50	11.50	11.50	0.00	0.00	0.00
125	10.50	10.50	10.50	0.00	0.00	0.00
126	10.50	10.50	10.50	0.00	0.00	0.00
127	10.50	10.50	10.50	0.00	0.00	0.00
128	10.50	10.50	10.50	0.00	0.00	0.00
129	10.50	10.50	10.50	0.00	0.00	0.00
130	10.50	10.50	10.50	0.00	0.00	0.00
131	10.50	10.50	10.50	0.00	0.00	0.00
132	10.50	10.50	10.50	0.00	0.00	0.00
133	9.50	9.50	9.50	0.00	0.00	0.00
134	9.50	9.50	9.50	0.00	0.00	0.00
135	9.50	9.50	9.50	0.00	0.00	0.00
136	9.50	9.50	9.50	0.00	0.00	0.00
137	9.50	9.50	9.50	0.00	0.00	0.00
138	9.50	9.50	9.50	0.00	0.00	0.00
139	9.50	9.50	9.50	0.00	0.00	0.00
140	9.50	9.50	9.50	0.00	0.00	0.00
141	9.50	9.50	9.50	0.00	0.00	0.00
142	9.50	9.50	9.50	0.00	0.00	0.00
143	9.50	9.50	9.50	0.00	0.00	0.00
144	9.50	9.50	9.50	0.00	0.00	0.00
145	8.50	8.50	8.50	0.00	0.00	0.00
146	8.00	8.00	8.00	0.00	0.00	0.00
147	8.00	8.00	8.00	0.00	0.00	0.00
148	8.00	8.00	8.00	0.00	0.00	0.00
149	8.00	8.00	8.00	0.00	0.00	0.00
150	8.00	8.00	8.00	0.00	0.00	0.00
151	8.00	8.00	8.00	0.00	0.00	0.00
152	8.00	8.00	8.00	0.00	0.00	0.00
153	7.50	7.50	7.50	0.00	0.00	0.00
154	7.50	7.50	7.50	0.00	0.00	0.00
155	7.50	7.50	7.50	0.00	0.00	0.00
156	7.50	7.50	7.50	0.00	0.00	0.00
157	7.50	7.50	7.50	0.00	0.00	0.00
158	7.00	7.00	7.00	0.00	0.00	0.00
159	7.00	7.00	7.00	0.00	0.00	0.00
160	7.00	7.00	7.00	0.00	0.00	0.00
161	7.00	7.00	7.00	0.00	0.00	0.00
162	7.00	7.00	7.00	0.00	0.00	0.00
163	7.00	7.00	7.00	0.00	0.00	0.00
164	7.00	7.00	7.00	0.00	0.00	0.00

<u>S-65B(Contd)</u>	<u>Gate 1</u>	<u>Gate 3</u>	<u>Gate 3</u>			
165	7.00	7.00	7.00	0.00	0.00	0.00
166	7.00	7.00	7.00	0.00	0.00	0.00
167	7.00	7.00	7.00	0.00	0.00	0.00
168	7.00	7.00	7.00	0.00	0.00	0.00
169	6.50	7.00	6.50	0.00	0.00	0.00
170	6.50	7.00	6.50	0.00	0.00	0.00
171	6.50	7.00	6.50	0.00	0.00	0.00
172	6.50	7.00	6.50	0.00	0.00	0.00
173	6.50	7.00	6.50	0.00	0.00	0.00
174	6.00	6.50	6.00	0.00	0.00	0.00
175	6.00	6.50	6.00	0.00	0.00	0.00
176	6.00	6.50	6.00	0.00	0.00	0.00
177	6.00	6.50	6.00	0.00	0.00	0.00
178	6.00	6.50	6.00	0.00	0.00	0.00
179	6.00	6.50	6.00	0.00	0.00	0.00
180	6.00	6.50	6.00	0.00	0.00	0.00
181	6.00	6.50	6.00	0.00	0.00	0.00
182	6.50	7.50	6.50	0.00	0.00	0.00
183	6.50	7.50	6.50	0.00	0.00	0.00
184	6.50	7.50	6.50	0.00	0.00	0.00
185	6.50	7.50	6.50	0.00	0.00	0.00
186	6.50	7.50	6.50	0.00	0.00	0.00
187	6.50	7.50	6.50	0.00	0.00	0.00
188	6.50	7.50	6.50	0.00	0.00	0.00
189	6.50	7.50	6.50	0.00	0.00	0.00
190	6.50	7.50	6.50	0.00	0.00	0.00
191	6.50	7.50	6.50	0.00	0.00	0.00
192	6.00	7.00	6.50	0.00	0.00	0.00
193	6.00	7.00	6.50	0.00	0.00	0.00
194	6.00	7.00	6.50	0.00	0.00	0.00
195	6.00	7.00	6.50	0.00	0.00	0.00
196	6.00	7.00	6.50	0.00	0.00	0.00
197	6.00	7.00	6.50	0.00	0.00	0.00
198	7.00	7.00	7.00	0.00	0.00	0.00
199	7.00	7.00	7.00	0.00	0.00	0.00
200	7.00	7.00	7.00	0.00	0.00	0.00
201	7.00	7.00	7.00	0.00	0.00	0.00
202	6.50	7.00	7.00	0.00	0.00	0.00
203	6.50	7.00	7.00	0.00	0.00	0.00
204	6.50	7.00	7.00	0.00	0.00	0.00
205	6.50	7.00	7.00	0.00	0.00	0.00
206	6.50	7.00	7.00	0.00	0.00	0.00
207	6.50	7.00	7.00	0.00	0.00	0.00
208	6.50	7.00	7.00	0.00	0.00	0.00
209	6.50	7.00	7.00	0.00	0.00	0.00
210	6.50	7.00	7.00	0.00	0.00	0.00
211	6.50	7.00	7.00	0.00	0.00	0.00
212	6.50	7.00	7.00	0.00	0.00	0.00
213	6.50	7.00	7.00	0.00	0.00	0.00
214	6.50	7.00	7.00	0.00	0.00	0.00
215	6.50	7.00	7.00	0.00	0.00	0.00
216	6.50	7.00	7.00	0.00	0.00	0.00
217	6.50	7.00	7.00	0.00	0.00	0.00
218	6.50	7.00	7.00	0.00	0.00	0.00
219	6.50	7.00	7.00	0.00	0.00	0.00
220	6.50	7.00	7.00	0.00	0.00	0.00
221	6.50	7.00	7.00	0.00	0.00	0.00
222	6.50	7.00	7.00	0.00	0.00	0.00
223	6.50	7.00	7.00	0.00	0.00	0.00

S-65B(Contd)

	Gate 1	Gate 2	Gate 3			
224	6.50	7.00	7.00	6.00	0.00	0.00
225	6.50	7.00	6.50	0.00	0.00	0.00
226	6.50	7.00	6.50	0.00	0.00	0.00
227	6.50	7.00	6.50	0.00	0.00	0.00
228	6.50	7.00	6.50	0.00	0.00	0.00
229	6.50	7.00	6.50	0.00	0.00	0.00
230	6.50	7.00	6.50	0.00	0.00	0.00
231	6.50	7.00	6.50	0.00	0.00	0.00
232	6.50	7.00	6.50	0.00	0.00	0.00
233	6.50	7.00	6.50	0.00	0.00	0.00
234	6.50	7.00	6.50	0.00	0.00	0.00
235	6.50	7.00	6.50	0.00	0.00	0.00
236	6.50	7.00	6.50	0.00	0.00	0.00
237	6.50	7.00	6.50	0.00	0.00	0.00
238	6.00	6.50	6.00	0.00	0.00	0.00
239	6.00	6.50	6.00	0.00	0.00	0.00
240	6.00	6.50	6.00	0.00	0.00	0.00
241	6.00	6.50	6.00	0.00	0.00	0.00
242	6.00	6.50	6.00	0.00	0.00	0.00
243	6.00	6.50	6.00	0.00	0.00	0.00
244	6.00	6.50	6.00	0.00	0.00	0.00
245	6.00	6.50	6.00	0.00	0.00	0.00
246	6.00	6.50	6.00	0.00	0.00	0.00
247	6.00	6.50	6.00	0.00	0.00	0.00
248	6.00	6.50	6.00	0.00	0.00	0.00
249	6.00	6.50	6.00	0.00	0.00	0.00
250	6.00	6.50	6.00	0.00	0.00	0.00
251	6.00	6.50	6.00	0.00	0.00	0.00
252	6.00	6.00	6.00	0.00	0.00	0.00
253	6.00	6.00	6.00	0.00	0.00	0.00
254	6.00	6.00	6.00	0.00	0.00	0.00
255	6.00	6.00	6.00	0.00	0.00	0.00
256	6.00	6.00	6.00	0.00	0.00	0.00
257	6.00	6.00	6.00	0.00	0.00	0.00
258	6.00	6.00	6.00	0.00	0.00	0.00
259	6.00	6.00	6.00	0.00	0.00	0.00
260	6.00	6.00	6.00	0.00	0.00	0.00
261	6.00	6.00	6.00	0.00	0.00	0.00
262	6.00	6.00	6.00	0.00	0.00	0.00
263	6.00	6.00	6.00	0.00	0.00	0.00
264	6.00	6.00	6.00	0.00	0.00	0.00
265	6.00	6.00	6.00	0.00	0.00	0.00
266	6.00	6.00	6.00	0.00	0.00	0.00
267	6.00	6.00	6.00	0.00	0.00	0.00
268	6.00	6.00	6.00	0.00	0.00	0.00
269	6.00	6.00	6.00	0.00	0.00	0.00
270	6.00	6.00	6.00	0.00	0.00	0.00
271	6.00	6.00	6.00	0.00	0.00	0.00
272	6.00	6.00	6.00	0.00	0.00	0.00
273	6.00	6.00	6.00	0.00	0.00	0.00
274	6.00	6.00	6.00	0.00	0.00	0.00
275	6.00	6.00	6.00	0.00	0.00	0.00
276	6.00	6.00	6.00	0.00	0.00	0.00
277	6.00	6.00	6.00	0.00	0.00	0.00
278	6.00	6.00	6.00	0.00	0.00	0.00
279	6.00	6.00	6.00	0.00	0.00	0.00
280	6.00	6.00	6.00	0.00	0.00	0.00
281	6.00	6.00	6.00	0.00	0.00	0.00
282	6.00	6.00	6.00	0.00	0.00	0.00

S-65B(Contd)

	<u>Gate 1</u>	<u>Gate 2</u>	<u>Gate 3</u>			
283	6.00	6.00	6.00	0.00	0.00	0.00
284	6.00	6.00	6.00	0.00	0.00	0.00
285	6.00	6.00	6.00	0.00	0.00	0.00
286	6.00	6.00	6.00	0.00	0.00	0.00
287	6.00	6.00	6.00	0.00	0.00	0.00
288	6.00	6.00	6.00	0.00	0.00	0.00
289	6.00	6.00	6.00	0.00	0.00	0.00
290	6.00	6.00	6.00	0.00	0.00	0.00
291	6.00	6.00	6.00	0.00	0.00	0.00
292	6.00	6.50	6.00	0.00	0.00	0.00
293	6.00	6.50	6.00	0.00	0.00	0.00
294	6.00	6.50	6.00	0.00	0.00	0.00
295	6.00	6.50	6.00	0.00	0.00	0.00
296	6.00	6.50	6.00	0.00	0.00	0.00
297	6.00	6.50	6.00	0.00	0.00	0.00
298	6.00	6.50	6.00	0.00	0.00	0.00
299	6.00	6.50	6.00	0.00	0.00	0.00
300	6.00	6.50	6.00	0.00	0.00	0.00
301	6.00	6.50	6.00	0.00	0.00	0.00
302	6.00	6.50	6.00	0.00	0.00	0.00
303	6.00	6.50	6.00	0.00	0.00	0.00
304	6.00	6.50	6.00	0.00	0.00	0.00
305	6.00	6.50	6.00	0.00	0.00	0.00
306	6.00	6.50	6.00	0.00	0.00	0.00
307	6.00	6.50	6.00	0.00	0.00	0.00
308	6.00	6.50	6.00	0.00	0.00	0.00
309	6.00	6.50	6.00	0.00	0.00	0.00
310	6.00	6.50	6.00	0.00	0.00	0.00
311	6.00	6.50	6.00	0.00	0.00	0.00
312	6.00	6.50	6.00	0.00	0.00	0.00
313	6.00	6.50	6.00	0.00	0.00	0.00
314	6.00	6.50	6.00	0.00	0.00	0.00
315	6.00	6.50	6.00	0.00	0.00	0.00
316	6.00	6.50	6.00	0.00	0.00	0.00
317	6.00	6.50	6.00	0.00	0.00	0.00
318	6.00	6.50	6.00	0.00	0.00	0.00
319	6.00	6.50	6.00	0.00	0.00	0.00
320	6.00	6.50	6.00	0.00	0.00	0.00
321	6.00	6.50	6.00	0.00	0.00	0.00
322	6.00	6.50	6.00	0.00	0.00	0.00
323	6.00	6.50	6.00	0.00	0.00	0.00
324	6.00	6.50	6.00	0.00	0.00	0.00
325	6.00	6.50	6.00	0.00	0.00	0.00
326	6.00	6.50	6.00	0.00	0.00	0.00
327	6.00	6.50	6.00	0.00	0.00	0.00
328	6.00	6.50	6.00	0.00	0.00	0.00
329	6.00	6.50	6.00	0.00	0.00	0.00
330	6.00	6.50	6.00	0.00	0.00	0.00
331	6.00	6.50	6.00	0.00	0.00	0.00
332	6.00	6.50	6.00	0.00	0.00	0.00
333	6.00	6.50	6.00	0.00	0.00	0.00
334	6.00	6.50	6.00	0.00	0.00	0.00
335	6.00	6.00	6.00	0.00	0.00	0.00
336	6.00	6.00	6.00	0.00	0.00	0.00
337	6.00	6.00	6.00	0.00	0.00	0.00
338	6.00	6.00	6.00	0.00	0.00	0.00
339	6.00	6.00	6.00	0.00	0.00	0.00
340	6.00	6.00	6.00	0.00	0.00	0.00
341	6.00	6.00	6.00	0.00	0.00	0.00
342	6.00	6.00	6.00	0.00	0.00	0.00
Time						

Time

S-65C

	<u>Gate 1</u>	<u>Gate 2</u>	<u>Gate 3</u>	<u>Gate 4</u>		
1	3.25	3.00	3.00	3.00	0.00	0.00
2	3.25	3.00	3.00	3.00	0.00	0.00
3	3.25	3.00	3.00	3.00	0.00	0.00
4	3.25	3.00	3.00	3.00	0.00	0.00
5	3.00	3.00	3.00	3.00	0.00	0.00
6	3.00	3.00	3.00	3.00	0.00	0.00
7	3.00	3.00	3.00	3.00	0.00	0.00
8	3.00	3.00	3.00	3.00	0.00	0.00
9	3.00	3.00	3.00	3.00	0.00	0.00
10	3.00	3.00	3.00	3.00	0.00	0.00
11	3.00	3.00	3.00	3.00	0.00	0.00
12	3.00	3.00	3.00	3.00	0.00	0.00
13	3.25	3.25	3.25	3.25	0.00	0.00
14	3.25	3.25	3.25	3.25	0.00	0.00
15	3.50	3.50	3.50	3.50	0.00	0.00
16	3.50	3.50	3.50	3.50	0.00	0.00
17	3.75	3.75	3.75	3.75	0.00	0.00
18	3.75	3.75	3.75	3.75	0.00	0.00
19	3.75	3.75	3.75	3.75	0.00	0.00
20	3.75	3.75	3.75	3.75	0.00	0.00
21	3.75	3.75	3.75	3.75	0.00	0.00
22	3.75	3.75	3.75	3.75	0.00	0.00
23	3.75	3.75	3.75	3.75	0.00	0.00
24	3.75	3.75	3.75	3.75	0.00	0.00
25	4.25	4.25	4.25	4.25	0.00	0.00
26	4.25	4.25	4.25	4.25	0.00	0.00
27	4.25	4.25	4.25	4.25	0.00	0.00
28	4.25	4.25	4.25	4.25	0.00	0.00
29	4.25	4.25	4.25	4.25	0.00	0.00
30	4.25	4.25	4.25	4.25	0.00	0.00
31	4.25	4.25	4.25	4.25	0.00	0.00
32	4.25	4.25	4.25	4.25	0.00	0.00
33	4.25	4.25	4.25	4.25	0.00	0.00
34	4.50	4.50	4.75	4.75	0.00	0.00

<u>S-65C(Contd)</u>	<u>Gate 1</u>	<u>Gate 2</u>	<u>Gate 3</u>	<u>Gate 4</u>	
55	4.50	4.50	4.75	4.75	0.00
56	5.00	5.00	5.25	5.25	0.00
57	5.50	5.50	5.75	6.00	0.00
58	7.00	7.00	7.00	7.00	0.00
59	7.50	7.50	7.50	7.50	0.00
60	9.00	9.00	9.00	9.00	0.00
61	9.00	9.00	9.00	9.00	0.00
62	9.00	9.00	9.00	9.00	0.00
63	9.00	9.00	9.00	9.00	0.00
64	11.00	11.00	11.00	11.00	0.00
65	11.00	11.00	11.00	11.00	0.00
66	11.00	11.00	11.00	11.00	0.00
67	11.00	11.00	11.00	11.00	0.00
68	11.00	11.00	11.00	11.00	0.00
69	11.00	11.00	11.00	11.00	0.00
70	11.00	11.00	11.00	11.00	0.00
71	10.00	10.00	10.00	10.00	0.00
72	10.00	10.00	10.00	10.00	0.00
73	10.00	10.00	10.00	10.00	0.00
74	10.00	10.00	10.00	10.00	0.00
75	10.00	10.00	10.00	10.00	0.00
76	10.00	10.00	10.00	10.00	0.00
77	10.00	10.00	10.00	10.00	0.00
78	10.00	10.00	10.00	10.00	0.00
79	10.00	10.00	10.00	10.00	0.00
80	10.00	10.00	10.00	10.00	0.00
81	10.00	10.00	10.00	10.00	0.00
82	10.00	10.00	10.00	10.00	0.00
83	10.00	10.00	10.00	10.00	0.00
84	10.00	10.00	10.00	10.00	0.00
85	10.00	10.00	10.00	10.00	0.00
86	10.00	10.00	10.00	10.00	0.00
87	10.00	10.00	10.00	10.00	0.00
88	10.00	10.00	10.00	10.00	0.00
89	10.00	10.00	10.00	10.00	0.00
90	10.00	10.00	10.00	10.00	0.00
91	10.00	10.00	10.00	10.00	0.00
92	10.00	10.00	10.00	10.00	0.00
93	10.00	10.00	10.00	10.00	0.00

S-65C (Contd)

	<u>Gate 1</u>	<u>Gate 2</u>	<u>Gate 3</u>	<u>Gate 4</u>	
94	10.00	10.00	10.00	10.00	0.00
95	10.00	10.00	10.00	10.00	0.00
96	10.00	10.00	10.00	10.00	0.00
97	10.00	10.00	10.00	10.00	0.00
98	10.00	10.00	10.00	10.00	0.00
99	10.00	10.00	10.00	10.00	0.00
100	10.00	10.00	10.00	10.00	0.00
101	10.00	10.00	10.00	10.00	0.00
102	10.00	10.00	10.00	10.00	0.00
103	10.00	10.00	10.00	10.00	0.00
104	10.00	10.00	10.00	10.00	0.00
105	10.00	10.00	10.00	10.00	0.00
106	10.00	10.00	10.00	10.00	0.00
107	10.00	10.00	10.00	10.00	0.00
108	10.00	10.00	10.00	10.00	0.00
109	10.00	10.00	10.00	10.00	0.00
110	10.00	10.00	10.00	10.00	0.00
111	10.00	10.00	10.00	10.00	0.00
112	10.00	10.00	10.00	10.00	0.00
113	10.00	10.00	10.00	10.00	0.00
114	10.00	10.00	10.00	10.00	0.00
115	10.00	10.00	10.00	10.00	0.00
116	10.00	10.00	10.00	10.00	0.00
117	10.00	10.00	10.00	10.00	0.00
118	10.00	10.00	10.00	10.00	0.00
119	10.00	10.00	10.00	10.00	0.00
120	10.00	10.00	10.00	10.00	0.00
121	10.00	10.00	10.00	10.00	0.00
122	10.00	10.00	10.00	10.00	0.00
123	10.00	10.00	10.00	10.00	0.00
124	8.00	10.00	10.00	10.00	0.00
125	7.00	10.00	10.00	10.00	0.00
126	6.00	10.00	10.00	10.00	0.00
127	5.00	10.00	10.00	10.00	0.00
128	5.00	10.00	10.00	10.00	0.00
129	5.00	10.00	10.00	10.00	0.00
130	5.00	10.00	10.00	9.00	0.00
131	5.00	10.00	10.00	8.00	0.00
132	5.00	10.00	10.00	8.00	0.00
133	5.00	10.00	10.00	8.00	0.00
134	5.00	10.00	10.00	8.00	0.00
135	5.00	10.00	10.00	8.00	0.00
136	5.00	10.00	10.00	8.00	0.00
137	5.00	10.00	10.00	8.00	0.00
138	5.00	10.00	10.00	8.00	0.00
139	5.00	10.00	10.00	8.00	0.00
140	5.00	10.00	10.00	8.00	0.00
141	5.00	10.00	10.00	8.00	0.00
142	5.00	10.00	10.00	8.00	0.00
143	5.00	10.00	10.00	8.00	0.00
144	5.00	10.00	10.00	8.00	0.00
145	5.00	10.00	10.00	6.00	0.00
146	5.00	10.00	10.00	6.00	0.00
147	5.00	10.00	10.00	5.00	0.00
148	5.00	10.00	10.00	5.00	0.00
149	5.00	10.00	10.00	5.00	0.00
150	5.00	10.00	10.00	5.00	0.00
151	5.00	10.00	10.00	10.00	0.00
152	5.00	9.00	9.00	5.00	0.00

<u>S-65C(Contd)</u>	<u>Gate 1</u>	<u>Gate 2</u>	<u>Gate 3</u>	<u>Gate 4</u>
153	5.00	5.00	5.00	5.00
154	5.00	5.00	5.00	5.00
155	5.00	5.00	5.00	5.00
156	5.00	5.00	5.00	5.00
157	5.00	5.00	5.00	5.00
158	5.00	5.00	5.00	5.00
159	5.00	5.00	5.00	5.00
160	5.00	5.00	5.00	5.00
161	5.00	5.00	5.00	5.00
162	5.00	5.00	5.00	5.00
163	5.00	5.00	5.00	5.00
164	5.00	5.00	5.00	5.00
165	5.00	5.00	5.00	5.00
166	5.00	5.00	5.00	5.00
167	5.00	5.00	5.00	5.00
168	5.00	5.00	5.00	5.00
169	5.00	5.00	5.00	5.00
170	5.00	5.00	5.00	5.00
171	5.00	5.00	5.00	5.00
172	5.00	5.00	5.00	5.00
173	5.00	5.00	5.00	5.00
174	5.00	5.00	5.00	5.00
175	5.00	5.00	5.00	5.00
176	5.00	5.00	5.00	5.00
177	5.00	5.00	5.00	5.00
178	5.00	5.00	5.00	5.00
179	5.00	5.00	5.00	5.00
180	5.00	5.00	5.00	5.00
181	5.00	5.00	5.00	5.00
182	5.00	5.00	5.00	5.00
183	5.00	5.00	5.00	5.00
184	5.00	5.00	5.00	5.00
185	5.00	5.00	5.00	5.00
186	5.00	5.00	5.00	5.00
187	5.00	5.00	5.00	5.00
188	5.00	5.00	5.00	5.00
189	5.00	5.00	5.00	5.00
190	5.00	5.00	5.00	5.00
191	5.00	5.00	5.00	5.00
192	5.00	5.00	5.00	5.00
193	5.00	5.00	5.00	5.00
194	5.00	5.00	5.00	5.00
195	5.00	5.00	5.00	5.00
196	5.00	5.00	5.00	5.00
197	5.00	5.00	5.00	5.00
198	5.50	5.50	5.50	5.50
199	5.50	5.50	5.50	5.50
200	5.50	5.50	5.50	5.50
201	5.50	5.50	5.50	5.50
202	5.50	5.50	5.50	5.50
203	5.50	5.50	5.50	5.50
204	5.50	5.50	5.50	5.50
205	5.50	5.50	5.50	5.50
206	5.50	5.50	5.50	5.50
207	5.50	5.50	5.50	5.50
208	5.00	5.00	5.00	5.00
209	5.00	5.00	5.00	5.00
210	5.00	5.00	5.00	5.00
211	5.00	5.00	5.00	5.00

<u>S-65C (Contd)</u>	<u>Gate 1</u>	<u>Gate 2</u>	<u>Gate 3</u>	<u>Gate 4</u>
212	5.00	5.00	5.00	5.00
213	5.00	5.00	5.00	5.00
214	5.00	5.00	5.00	5.00
215	5.00	5.00	5.00	5.00
216	5.00	5.00	5.00	5.00
217	5.00	5.00	5.00	5.00
218	5.25	5.25	5.25	5.00
219	5.25	5.25	5.25	5.00
220	5.25	5.25	5.25	5.00
221	5.25	5.25	5.25	5.00
222	5.25	5.25	5.25	5.25
223	5.25	5.25	5.25	5.25
224	5.25	5.25	5.25	5.25
225	5.25	5.25	5.25	5.00
226	5.00	5.25	5.00	5.00
227	5.00	5.25	5.00	5.00
228	5.00	5.25	5.00	5.00
229	5.00	5.25	5.00	5.00
230	5.00	5.25	5.00	5.00
231	5.00	5.25	5.00	5.00
232	5.00	5.25	5.00	5.00
233	5.00	5.25	5.00	5.00
234	5.00	5.25	5.00	5.00
235	5.00	5.25	5.00	5.00
236	5.00	5.00	5.00	5.00
237	5.00	5.00	5.00	5.00
238	5.00	5.00	5.00	5.00
239	4.50	4.75	4.75	4.50
240	4.50	4.75	4.75	4.50
241	4.50	4.75	4.75	4.50
242	4.50	4.75	4.75	4.50
243	4.50	4.75	4.75	4.50
244	4.50	4.75	4.75	4.50
245	4.50	4.75	4.75	4.50
246	4.50	4.75	4.75	4.50
247	4.50	4.75	4.75	4.50
248	4.50	4.75	4.75	4.50
249	4.50	4.75	4.75	4.50
250	4.50	4.75	4.75	4.50
251	4.50	4.75	4.75	4.50
252	4.50	4.75	4.75	4.50
253	4.50	4.75	4.75	4.50
254	4.50	4.75	4.75	4.50
255	4.50	4.75	4.75	4.50
256	4.50	4.50	4.50	4.50
257	4.50	4.50	4.50	4.50
258	4.50	4.50	4.50	4.50
259	4.50	4.50	4.50	4.50
260	4.50	4.50	4.50	4.50
261	4.50	4.50	4.50	4.50
262	4.50	4.50	4.50	4.50
263	4.50	4.50	4.50	4.50
264	4.50	4.50	4.50	4.50
265	4.50	4.50	4.50	4.50
266	4.50	4.50	4.50	4.50
267	4.50	4.50	4.50	4.50
268	4.50	4.50	4.50	4.50
269	4.50	4.50	4.50	4.50
270	4.50	4.50	4.50	4.50

S-65C(Contd)	Gate 1	Gate 2	Gate 3	Gate 4		
271	4.50	4.50	4.50	4.50	0.00	0.00
272	4.50	4.50	4.50	4.50	0.00	0.00
273	4.50	4.50	4.50	4.50	0.00	0.00
274	4.50	4.50	4.50	4.50	0.00	0.00
275	4.50	4.50	4.50	4.50	0.00	0.00
276	4.50	4.50	4.50	4.50	0.00	0.00
277	4.50	4.50	4.50	4.50	0.00	0.00
278	4.50	4.50	4.50	4.50	0.00	0.00
279	4.50	4.50	4.50	4.50	0.00	0.00
280	4.50	4.50	4.50	4.50	0.00	0.00
281	4.50	4.50	4.50	4.50	0.00	0.00
282	4.50	4.50	4.50	4.50	0.00	0.00
283	4.50	4.50	4.50	4.50	0.00	0.00
284	4.50	4.50	4.50	4.50	0.00	0.00
285	4.50	4.50	4.50	4.50	0.00	0.00
286	4.50	4.50	4.50	4.50	0.00	0.00
287	4.50	4.50	4.50	4.50	0.00	0.00
288	4.50	4.50	4.50	4.50	0.00	0.00
289	4.25	4.25	4.50	4.50	0.00	0.00
290	4.25	4.25	4.50	4.50	0.00	0.00
291	4.25	4.25	4.50	4.50	0.00	0.00
292	4.25	4.25	4.50	4.50	0.00	0.00
293	4.25	4.25	4.50	4.50	0.00	0.00
294	4.50	4.75	4.50	4.50	0.00	0.00
295	4.50	4.75	4.50	4.50	0.00	0.00
296	4.50	4.75	4.50	4.50	0.00	0.00
297	4.50	4.75	4.50	4.50	0.00	0.00
298	4.50	4.75	4.50	4.50	0.00	0.00
299	4.50	4.75	4.50	4.50	0.00	0.00
300	4.50	4.75	4.50	4.50	0.00	0.00
301	4.50	4.75	4.50	4.50	0.00	0.00
302	4.50	4.75	4.50	4.50	0.00	0.00
303	4.50	4.75	4.50	4.50	0.00	0.00
304	4.50	4.75	4.50	4.50	0.00	0.00
305	4.50	4.75	4.50	4.50	0.00	0.00
306	4.50	4.75	4.50	4.50	0.00	0.00
307	4.50	4.75	4.50	4.50	0.00	0.00
308	4.50	4.75	4.50	4.50	0.00	0.00
309	4.50	4.75	4.50	4.50	0.00	0.00
310	4.50	4.75	4.50	4.50	0.00	0.00
311	4.50	4.75	4.50	4.50	0.00	0.00
312	4.50	4.75	4.50	4.50	0.00	0.00
313	4.25	4.25	4.50	4.50	0.00	0.00
314	4.25	4.25	4.50	4.50	0.00	0.00
315	4.25	4.25	4.50	4.50	0.00	0.00
316	4.25	4.25	4.50	4.50	0.00	0.00
317	4.25	4.25	4.50	4.50	0.00	0.00
318	4.25	4.25	4.50	4.50	0.00	0.00
319	4.25	4.25	4.50	4.50	0.00	0.00
320	4.25	4.25	4.50	4.50	0.00	0.00
321	4.25	4.25	4.50	4.50	0.00	0.00
322	4.25	4.25	4.50	4.50	0.00	0.00
323	4.25	4.25	4.50	4.50	0.00	0.00
324	4.25	4.25	4.50	4.50	0.00	0.00
325	4.25	4.25	4.50	4.50	0.00	0.00
326	4.25	4.25	4.50	4.50	0.00	0.00
327	4.25	4.25	4.50	4.50	0.00	0.00
328	4.25	4.25	4.50	4.50	0.00	0.00
329	4.25	4.25	4.50	4.50	0.00	0.00

<u>S-65C (Contd)</u>	<u>Gate 1</u>	<u>Gate 2</u>	<u>Gate 3</u>	<u>Gate 4</u>	
330	4.25	4.25	4.50	4.50	0.00
331	4.25	4.25	4.50	4.50	0.00
332	4.25	4.25	4.50	4.50	0.00
333	4.25	4.25	4.50	4.50	0.00
334	4.25	4.25	4.50	4.50	0.00
335	4.25	4.25	4.50	4.50	0.00
336	4.25	4.25	4.50	4.50	0.00
337	4.25	4.25	4.50	4.50	0.00
338	4.25	4.25	4.50	4.50	0.00
339	4.25	4.25	4.50	4.50	0.00
340	4.25	4.25	4.50	4.50	0.00
341	4.25	4.25	4.50	4.50	0.00
342	4.25	4.25	4.50	4.50	0.00

Time.

S-65D

Time	Gate	Gate	Gate	Gate		
	1	2	3	4		
1	3.50	3.50	4.25	3.50	0.00	0.00
2	3.50	3.50	4.25	3.50	0.00	0.00
3	3.50	3.50	4.25	3.50	0.00	0.00
4	3.50	3.50	4.25	3.50	0.00	0.00
5	3.50	3.50	4.25	3.50	0.00	0.00
6	3.50	3.50	4.25	3.50	0.00	0.00
7	3.50	3.50	4.25	3.50	0.00	0.00
8	3.50	3.50	4.25	3.50	0.00	0.00
9	3.50	3.50	4.25	3.50	0.00	0.00
10	3.50	4.50	4.25	3.50	0.00	0.00
11	3.50	4.50	4.25	3.50	0.00	0.00
12	3.50	4.50	4.25	3.50	0.00	0.00
13	3.50	5.00	4.50	3.50	0.00	0.00
14	3.50	5.00	4.50	3.50	0.00	0.00
15	4.00	4.50	4.75	4.75	0.00	0.00
16	4.00	4.50	4.75	4.75	0.00	0.00
17	5.00	4.75	4.75	4.75	0.00	0.00
18	5.00	4.75	4.75	4.75	0.00	0.00
19	5.00	4.75	4.75	4.75	0.00	0.00
20	5.00	4.75	4.75	4.75	0.00	0.00
21	5.00	4.75	4.75	4.75	0.00	0.00
22	5.00	4.75	4.75	4.75	0.00	0.00

S-65D (Contd)

Gate 1

Gate 2

Gate 3

Gate 4

23	5.00	4.75	4.75	4.75	0.00	0.00
24	5.00	4.75	4.75	4.75	0.00	0.00
25	5.00	7.00	4.75	4.75	0.00	0.00
26	5.00	7.00	4.75	4.75	0.00	0.00
27	5.00	7.00	4.75	4.75	0.00	0.00
28	5.00	7.00	4.75	4.75	0.00	0.00
29	5.00	7.00	4.75	4.75	0.00	0.00
30	5.00	6.25	4.75	4.75	0.00	0.00
31	5.00	6.25	4.75	4.75	0.00	0.00
32	5.00	6.25	4.75	4.75	0.00	0.00
33	5.00	6.25	4.75	4.75	0.00	0.00
34	6.00	6.25	6.00	4.75	0.00	0.00
35	6.00	6.25	6.00	4.75	0.00	0.00
36	6.75	6.25	6.75	6.25	0.00	0.00
37	8.75	8.75	8.75	8.75	0.00	0.00
38	8.75	8.75	8.75	8.75	0.00	0.00
39	10.75	10.75	10.75	10.75	0.00	0.00
40	10.75	10.75	10.75	10.75	0.00	0.00
41	11.50	11.50	11.50	11.50	0.00	0.00
42	11.50	11.50	11.50	11.50	0.00	0.00
43	11.50	11.50	11.50	11.50	0.00	0.00
44	11.50	11.50	11.50	11.50	0.00	0.00
45	11.50	11.50	11.50	11.50	0.00	0.00
46	11.50	11.50	11.50	11.50	0.00	0.00
47	12.00	12.00	12.00	12.00	0.00	0.00
48	12.00	12.00	12.00	12.00	0.00	0.00
49	12.00	12.00	12.00	12.00	0.00	0.00
50	12.00	12.00	12.00	12.00	0.00	0.00
51	11.00	11.00	11.00	11.00	0.00	0.00
52	11.00	11.00	11.00	11.00	0.00	0.00
53	11.00	11.00	11.00	11.00	0.00	0.00
54	11.00	11.00	11.00	11.00	0.00	0.00
55	11.00	11.00	11.00	11.00	0.00	0.00
56	11.00	11.00	11.00	11.00	0.00	0.00
57	11.00	11.00	11.00	11.00	0.00	0.00
58	11.00	11.00	11.00	11.00	0.00	0.00
59	11.00	11.00	11.00	11.00	0.00	0.00
60	11.00	11.00	11.00	11.00	0.00	0.00
61	11.00	11.00	11.00	11.00	0.00	0.00
62	11.00	11.00	11.00	11.00	0.00	0.00
63	11.00	11.00	11.00	11.00	0.00	0.00
64	11.00	11.00	11.00	11.00	0.00	0.00
65	11.00	11.00	11.00	11.00	0.00	0.00
66	11.00	11.00	11.00	11.00	0.00	0.00
67	11.00	11.00	11.00	11.00	0.00	0.00
68	11.00	11.00	11.00	11.00	0.00	0.00
69	11.00	11.00	11.00	11.00	0.00	0.00
70	11.00	11.00	11.00	11.00	0.00	0.00
71	11.00	11.00	11.00	11.00	0.00	0.00
72	11.00	11.00	11.00	11.00	0.00	0.00
73	11.00	11.00	11.00	11.00	0.00	0.00
74	11.00	11.00	11.00	11.00	0.00	0.00
75	11.00	11.00	11.00	11.00	0.00	0.00
76	11.00	11.00	11.00	11.00	0.00	0.00
77	11.00	11.00	11.00	11.00	0.00	0.00
78	11.00	11.00	11.00	11.00	0.00	0.00
79	10.00	10.00	10.00	10.00	0.00	0.00
80	10.00	10.00	10.00	10.00	0.00	0.00
81	10.00	10.00	10.00	10.00	0.00	0.00

<u>S-65D(Contd)</u>	<u>Gate 1</u>	<u>Gate 2</u>	<u>Gate 3</u>	<u>Gate 4</u>		
82	10.00	10.00	10.00	10.00	0.00	0.00
83	9.50	9.50	9.50	9.50	0.00	0.00
84	9.50	9.50	9.50	9.50	0.00	0.00
85	9.50	9.50	9.50	9.50	0.00	0.00
86	9.50	9.50	9.50	9.50	0.00	0.00
87	9.50	9.50	9.50	9.50	0.00	0.00
88	9.50	9.50	9.50	9.50	0.00	0.00
89	9.50	9.50	9.50	9.50	0.00	0.00
90	9.50	9.50	9.50	9.50	0.00	0.00
91	9.50	9.50	9.50	9.50	0.00	0.00
92	9.50	9.50	9.50	9.50	0.00	0.00
93	9.50	9.50	9.50	9.50	0.00	0.00
94	9.50	9.50	9.50	9.50	0.00	0.00
95	9.50	9.50	9.50	9.50	0.00	0.00
96	9.50	9.50	9.50	9.50	0.00	0.00
97	9.50	9.50	9.50	9.50	0.00	0.00
98	9.50	9.50	9.50	9.50	0.00	0.00
99	9.50	9.50	9.50	9.50	0.00	0.00
100	9.50	9.50	9.50	9.50	0.00	0.00
101	9.50	9.50	9.50	9.50	0.00	0.00
102	9.50	9.50	9.50	9.50	0.00	0.00
103	9.50	9.50	9.50	9.50	0.00	0.00
104	9.50	9.50	9.50	9.50	0.00	0.00
105	9.50	9.50	9.50	9.50	0.00	0.00
106	10.00	10.00	10.00	10.00	0.00	0.00
107	10.00	10.00	10.00	10.00	0.00	0.00
108	10.00	10.00	10.00	10.00	0.00	0.00
109	10.00	10.00	10.00	10.00	0.00	0.00
110	10.00	10.00	10.00	10.00	0.00	0.00
111	10.00	10.00	10.00	10.00	0.00	0.00
112	10.00	10.00	10.00	10.00	0.00	0.00
113	10.00	10.00	10.00	10.00	0.00	0.00
114	10.00	10.00	10.00	10.00	0.00	0.00
115	10.00	10.00	10.00	10.00	0.00	0.00
116	10.00	10.00	10.00	10.00	0.00	0.00
117	10.00	10.00	10.00	10.00	0.00	0.00
118	10.00	10.00	10.00	10.00	0.00	0.00
119	10.00	10.00	10.00	10.00	0.00	0.00
120	10.00	10.00	10.00	10.00	0.00	0.00
121	10.00	10.00	10.00	10.00	0.00	0.00
122	10.00	10.00	10.00	10.00	0.00	0.00
123	10.00	10.00	10.00	10.00	0.00	0.00
124	10.00	10.00	10.00	10.00	0.00	0.00
125	10.00	10.00	10.00	10.00	0.00	0.00
126	10.00	10.00	10.00	10.00	0.00	0.00
127	10.00	10.00	10.00	10.00	0.00	0.00
128	10.00	10.00	10.00	10.00	0.00	0.00
129	10.00	10.00	10.00	10.00	0.00	0.00
130	10.00	10.00	10.00	10.00	0.00	0.00
131	10.00	10.00	10.00	10.00	0.00	0.00
132	10.00	10.00	10.00	10.00	0.00	0.00
133	10.00	10.00	10.00	10.00	0.00	0.00
134	10.00	10.00	10.00	10.00	0.00	0.00
135	10.00	10.00	10.00	10.00	0.00	0.00
136	10.00	10.00	10.00	10.00	0.00	0.00
137	10.00	10.00	10.00	10.00	0.00	0.00
138	10.00	10.00	10.00	10.00	0.00	0.00
139	10.00	10.00	10.00	10.00	0.00	0.00
140	10.00	10.00	10.00	10.00	0.00	0.00

S-65D(Contd)

	<u>Gage 1</u>	<u>Gate 2</u>	<u>Gate 3</u>	<u>Gate 4</u>		
141	10.00	10.00	10.00	10.00	0.00	0.00
142	10.00	10.00	10.00	10.00	0.00	0.00
143	10.00	10.00	10.00	10.00	0.00	0.00
144	10.00	10.00	10.00	10.00	0.00	0.00
145	10.00	10.00	10.00	10.00	0.00	0.00
146	10.00	10.00	10.00	10.00	0.00	0.00
147	10.00	10.00	10.00	10.00	0.00	0.00
148	10.00	10.00	10.00	10.00	0.00	0.00
149	10.00	10.00	10.00	10.00	0.00	0.00
150	10.00	10.00	10.00	10.00	0.00	0.00
151	10.00	10.00	10.00	10.00	0.00	0.00
152	10.00	10.00	10.00	10.00	0.00	0.00
153	9.00	9.00	9.00	9.00	0.00	0.00
154	8.00	8.00	8.00	8.00	0.00	0.00
155	8.00	8.00	8.00	8.00	0.00	0.00
156	8.00	8.00	8.00	8.00	0.00	0.00
157	8.00	8.00	8.00	8.00	0.00	0.00
158	7.00	7.00	7.00	7.00	0.00	0.00
159	7.00	7.00	7.00	7.00	0.00	0.00
160	7.00	7.00	7.00	7.00	0.00	0.00
161	7.00	7.00	7.00	7.00	0.00	0.00
162	7.00	7.00	7.00	7.00	0.00	0.00
163	7.00	7.00	7.00	7.00	0.00	0.00
164	7.00	7.00	7.00	7.00	0.00	0.00
165	7.00	7.00	7.00	7.00	0.00	0.00
166	7.00	7.00	7.00	7.00	0.00	0.00
167	7.00	7.00	7.00	7.00	0.00	0.00
168	6.50	6.50	6.50	6.50	0.00	0.00
169	6.50	6.50	6.50	6.50	0.00	0.00
170	6.50	6.50	6.50	6.50	0.00	0.00
171	6.50	6.50	6.50	6.50	0.00	0.00
172	6.50	6.50	6.50	6.50	0.00	0.00
173	6.50	6.50	6.50	6.50	0.00	0.00
174	6.50	6.50	6.50	6.50	0.00	0.00
175	6.50	6.50	6.50	6.50	0.00	0.00
176	6.50	6.50	6.50	6.50	0.00	0.00
177	6.50	6.50	6.50	6.50	0.00	0.00
178	6.50	6.50	6.50	6.50	0.00	0.00
179	6.50	6.50	6.50	6.50	0.00	0.00
180	6.50	6.50	6.50	6.50	0.00	0.00
181	6.50	6.50	6.50	6.50	0.00	0.00
182	6.50	6.50	6.50	6.50	0.00	0.00
183	6.50	6.50	6.50	6.50	0.00	0.00
184	5.50	6.50	6.50	6.50	0.00	0.00
185	5.50	6.50	6.50	6.50	0.00	0.00
186	5.50	6.50	6.50	6.50	0.00	0.00
187	5.50	6.50	6.50	6.50	0.00	0.00
188	5.50	6.50	6.50	6.50	0.00	0.00
189	5.50	6.50	6.50	6.50	0.00	0.00
190	5.50	6.50	6.50	6.50	0.00	0.00
191	5.50	6.50	6.50	6.50	0.00	0.00
192	5.50	6.50	6.50	6.50	0.00	0.00
193	5.50	6.50	6.50	6.50	0.00	0.00
194	5.50	6.50	6.50	6.50	0.00	0.00
195	5.50	6.50	6.50	6.50	0.00	0.00
196	5.50	6.50	6.50	6.00	0.00	0.00
197	5.50	6.50	6.50	6.00	0.00	0.00
198	5.50	6.50	6.50	6.00	0.00	0.00
199	6.50	6.50	6.50	6.50	0.00	0.00

S-65D (Contd)	Gate 1	Gate 2	Gate 3	Gate 4	
200	6.50	6.50	6.50	6.50	0.00
201	6.50	6.50	6.50	6.50	0.00
202	6.25	6.50	6.50	6.50	0.00
203	6.25	6.50	6.50	6.50	0.00
204	6.25	6.50	6.50	6.50	0.00
205	6.25	6.50	6.50	6.50	0.00
206	6.25	6.50	6.50	6.50	0.00
207	6.25	6.50	6.50	6.50	0.00
208	6.25	6.50	6.50	6.50	0.00
209	5.50	6.50	5.50	5.25	0.00
210	5.50	6.50	5.50	5.25	0.00
211	5.50	6.50	5.50	5.25	0.00
212	5.50	6.50	5.50	5.25	0.00
213	5.50	6.50	5.50	5.25	0.00
214	5.50	6.50	5.50	5.25	0.00
215	5.50	6.50	5.50	5.25	0.00
216	5.50	6.50	5.50	5.25	0.00
217	5.50	6.50	5.50	5.25	0.00
218	5.50	6.50	5.50	5.25	0.00
219	5.50	7.00	7.00	5.25	0.00
220	5.50	7.00	7.00	5.25	0.00
221	5.50	7.00	7.00	5.25	0.00
222	5.50	7.00	7.00	5.25	0.00
223	5.50	7.00	7.00	5.25	0.00
224	5.50	7.00	7.00	5.25	0.00
225	5.50	7.00	7.00	5.25	0.00
226	5.00	7.00	7.00	5.25	0.00
227	5.00	7.00	7.00	5.25	0.00
228	5.00	7.00	7.00	5.25	0.00
229	5.00	7.00	7.00	5.25	0.00
230	5.00	7.00	7.00	5.25	0.00
231	5.00	7.00	7.00	5.25	0.00
232	5.00	7.00	7.00	5.25	0.00
233	5.00	7.00	7.00	5.25	0.00
234	5.00	7.00	7.00	5.25	0.00
235	5.00	7.00	7.00	5.25	0.00
236	5.00	7.00	7.00	5.25	0.00
237	5.00	7.00	7.00	5.25	0.00
238	5.00	7.00	7.00	5.25	0.00
239	5.00	6.50	5.00	5.25	0.00
240	5.00	6.50	5.00	5.25	0.00
241	5.00	6.50	5.00	5.25	0.00
242	5.00	6.50	5.00	5.25	0.00
243	5.00	6.50	5.00	5.25	0.00
244	5.00	6.50	5.00	5.25	0.00
245	5.00	6.50	5.00	5.25	0.00
246	5.00	6.50	5.00	5.25	0.00
247	5.00	6.50	5.00	5.25	0.00
248	5.00	6.50	5.00	5.25	0.00
249	5.00	6.50	5.00	5.25	0.00
250	5.00	6.50	5.00	5.25	0.00
251	5.00	6.50	5.00	5.25	0.00
252	5.00	6.50	5.00	5.25	0.00
253	5.00	6.50	5.00	5.25	0.00
254	5.00	6.50	5.00	5.25	0.00
255	5.00	6.50	5.00	5.25	0.00
256	5.00	6.50	5.00	5.25	0.00
257	5.00	6.50	5.00	5.25	0.00
258	5.00	6.50	5.00	5.25	0.00

S-65D (Contd)	Gate 1	Gate 2	Gate 3	Gate 4		
259	5.00	6.50	5.00	5.25	0.00	0.00
260	5.00	6.50	5.00	5.25	0.00	0.00
261	5.00	6.50	5.00	5.25	0.00	0.00
262	5.00	6.50	5.00	5.25	0.00	0.00
263	5.00	6.50	5.00	5.25	0.00	0.00
264	5.00	6.50	5.00	5.25	0.00	0.00
265	5.00	6.50	5.00	5.25	0.00	0.00
266	5.00	6.50	5.00	5.25	0.00	0.00
267	5.00	6.50	5.00	5.25	0.00	0.00
268	5.00	6.50	5.00	5.25	0.00	0.00
269	5.00	6.50	5.00	5.25	0.00	0.00
270	5.00	6.50	5.00	5.25	0.00	0.00
271	5.00	6.50	5.00	5.25	0.00	0.00
272	5.00	6.50	5.00	5.25	0.00	0.00
273	5.00	6.50	5.00	5.25	0.00	0.00
274	6.77	6.77	6.77	6.77	0.00	0.00
275	6.77	6.77	6.77	6.77	0.00	0.00
276	6.77	6.77	6.77	6.77	0.00	0.00
277	6.77	6.77	6.77	6.77	0.00	0.00
278	6.77	6.77	6.77	6.77	0.00	0.00
279	6.77	6.77	6.77	6.77	0.00	0.00
280	6.77	6.77	6.77	6.77	0.00	0.00
281	6.77	6.77	6.77	6.77	0.00	0.00
282	6.77	6.77	6.77	6.77	0.00	0.00
283	6.77	6.77	6.77	6.77	0.00	0.00
284	6.77	6.77	6.77	6.77	0.00	0.00
285	6.77	6.77	6.77	6.77	0.00	0.00
286	6.77	6.77	6.77	6.77	0.00	0.00
287	6.77	6.77	6.77	6.77	0.00	0.00
288	6.77	6.77	6.77	6.77	0.00	0.00
289	5.00	5.50	5.00	5.25	0.00	0.00
290	5.00	5.50	5.00	5.25	0.00	0.00
291	5.00	5.50	5.00	5.25	0.00	0.00
292	5.00	5.50	5.00	5.25	0.00	0.00
293	5.00	5.50	5.00	5.25	0.00	0.00
294	5.00	5.50	5.00	5.25	0.00	0.00
295	5.00	5.50	5.00	5.25	0.00	0.00
296	5.00	5.50	5.75	5.25	0.00	0.00
297	5.00	5.50	5.75	5.25	0.00	0.00
298	5.00	5.50	5.75	5.25	0.00	0.00
299	5.00	5.50	5.75	5.25	0.00	0.00
300	5.00	5.50	5.75	5.25	0.00	0.00
301	5.00	5.50	5.75	5.25	0.00	0.00
302	5.00	5.50	5.75	5.25	0.00	0.00
303	5.00	5.50	5.75	5.25	0.00	0.00
304	5.00	5.50	5.75	5.25	0.00	0.00
305	5.00	5.50	5.75	5.25	0.00	0.00
306	5.00	5.50	5.75	5.25	0.00	0.00
307	5.00	5.50	5.75	5.25	0.00	0.00
308	5.00	5.50	5.75	5.25	0.00	0.00
309	5.00	5.50	5.75	5.25	0.00	0.00
310	5.00	5.50	5.75	5.25	0.00	0.00
311	5.00	5.50	5.75	5.25	0.00	0.00
312	5.00	5.50	5.75	5.25	0.00	0.00
313	5.00	5.50	5.00	5.25	0.00	0.00
314	5.00	5.50	5.00	5.25	0.00	0.00
315	5.00	5.50	5.00	5.25	0.00	0.00
316	5.00	5.50	5.00	5.25	0.00	0.00
317	5.00	5.50	5.00	5.25	0.00	0.00

<u>S-65D (Contd)</u>	<u>Gate 1</u>	<u>Gate 2</u>	<u>Gate 3</u>	<u>Gate 4</u>		
318	5.00	5.50	5.00	5.25	0.00	0.00
319	5.00	5.50	5.00	5.25	0.00	0.00
320	5.00	5.50	5.00	5.25	0.00	0.00
321	5.00	5.50	5.00	5.25	0.00	0.00
322	5.00	5.50	5.00	5.25	0.00	0.00
323	5.00	5.50	5.00	5.25	0.00	0.00
324	5.00	5.50	5.00	5.25	0.00	0.00
325	5.00	5.50	5.00	5.25	0.00	0.00
326	5.00	5.50	5.00	5.25	0.00	0.00
327	5.00	5.50	5.00	5.25	0.00	0.00
328	5.00	5.50	5.00	5.25	0.00	0.00
329	5.00	5.50	5.00	5.25	0.00	0.00
330	5.00	5.50	5.00	5.25	0.00	0.00
331	5.00	5.50	5.00	5.25	0.00	0.00
332	5.00	5.50	5.00	5.25	0.00	0.00
333	5.00	5.50	5.00	5.25	0.00	0.00
334	5.00	5.50	5.00	5.25	0.00	0.00
335	5.00	5.50	5.00	5.25	0.00	0.00
336	5.00	5.50	5.00	5.25	0.00	0.00
337	5.00	5.50	5.00	5.25	0.00	0.00
338	5.00	5.50	5.00	5.25	0.00	0.00
339	5.00	5.50	5.00	5.25	0.00	0.00
340	5.00	5.50	5.00	5.25	0.00	0.00
341	5.00	5.50	5.00	5.25	0.00	0.00
342	5.00	5.50	5.00	5.25	0.00	0.00

Time

S-65E

Time	Gate <u>1</u>	Gate <u>2</u>	Gate <u>3</u>	Gate <u>4</u>	Gate <u>5</u>	Gate <u>6</u>
1	1.50	3.00	3.00	3.50	2.75	2.75
2	1.50	3.00	3.00	3.50	2.75	2.75
3	1.50	3.00	3.00	3.50	2.75	2.75
4	1.50	3.00	3.00	2.50	2.75	2.75
5	1.50	3.00	3.00	2.50	2.75	2.75
6	1.50	3.00	3.00	2.50	2.75	2.75
7	1.50	3.00	3.00	2.50	2.75	2.75
8	1.50	3.00	3.00	2.50	2.75	2.75
9	1.50	3.00	3.00	2.50	2.75	2.75
10	3.00	3.00	3.00	3.00	2.75	2.75

S-65E(Contd.)	Gate 1	Gate 2	Gate 3	Gate 4	Gate 5	Gate 6
11	3.00	3.00	3.00	3.00	2.75	2.75
12	3.00	3.00	3.00	3.00	2.75	2.75
13	3.00	3.00	3.00	3.00	2.75	2.75
14	3.00	3.00	3.00	3.00	3.50	2.75
15	3.00	3.00	3.00	4.25	3.50	2.75
16	3.00	3.00	3.00	4.25	3.50	2.75
17	3.00	3.00	3.00	4.25	3.50	2.75
18	3.00	3.00	3.00	4.25	3.50	2.75
19	3.00	3.00	3.00	4.25	3.50	2.75
20	3.00	3.00	3.00	4.25	3.50	2.75
21	3.00	3.00	3.00	4.25	3.50	2.75
22	3.00	3.00	3.00	4.25	3.50	2.75
23	3.00	3.00	3.00	4.25	3.50	2.75
24	3.00	3.00	3.00	4.25	3.50	2.75
25	3.00	4.50	4.50	4.25	4.50	2.75
26	3.00	4.50	4.50	4.25	4.50	2.75
27	3.00	4.50	4.50	4.25	4.50	2.75
28	3.00	4.50	4.50	4.25	4.50	3.25
29	3.00	3.00	4.50	4.25	3.50	2.75
30	3.00	3.00	4.50	4.25	3.50	2.75
31	3.00	3.00	4.50	4.25	3.50	2.75
32	3.00	3.00	4.50	4.25	3.50	2.75
33	3.00	3.00	4.50	4.25	3.50	2.75
34	5.00	4.50	4.50	6.00	4.50	3.25
35	6.00	6.00	6.00	6.00	6.00	6.00
36	6.00	8.00	8.00	6.00	6.00	6.00
37	6.00	8.00	8.00	8.00	8.00	8.00
38	6.00	8.00	8.00	8.00	8.00	8.00
39	8.00	10.00	8.00	8.00	8.00	8.00
40	10.00	10.00	10.00	10.00	10.00	10.00
41	10.00	10.00	10.00	10.00	10.00	10.00
42	10.00	10.00	10.00	10.00	10.00	10.00
43	10.00	10.00	10.00	10.00	10.00	10.00
44	10.00	10.00	10.00	10.00	10.00	10.00
45	10.00	10.00	10.00	10.00	10.00	10.00
46	10.00	10.00	10.00	10.00	10.00	10.00
47	10.00	10.00	10.00	10.00	10.00	10.00
48	10.00	10.00	10.00	10.00	10.00	10.00
49	10.00	10.00	10.00	10.00	10.00	10.00
50	10.00	10.00	10.00	10.00	10.00	10.00
51	9.00	9.00	9.00	9.00	9.00	9.00
52	8.00	8.00	8.00	8.00	8.00	8.00
53	8.00	8.00	8.00	8.00	8.00	8.00
54	8.00	8.00	8.00	8.00	8.00	8.00
55	7.00	7.00	7.00	7.00	7.00	7.00
56	7.00	7.00	7.00	7.00	7.00	7.00
57	7.00	7.00	7.00	7.00	7.00	7.00
58	8.00	8.00	8.00	8.00	8.00	8.00
59	9.00	9.00	9.00	9.00	9.00	9.00
60	9.00	9.00	9.00	9.00	9.00	9.00
61	9.00	9.00	9.00	9.00	9.00	9.00
62	9.00	9.00	9.00	9.00	9.00	9.00
63	9.00	9.00	9.00	9.00	9.00	9.00
64	9.00	9.00	9.00	9.00	9.00	9.00
65	9.00	9.00	9.00	9.00	9.00	9.00
66	9.00	9.00	9.00	9.00	9.00	9.00
67	9.00	9.00	9.00	9.00	9.00	9.00
68	9.00	9.00	9.00	9.00	9.00	9.00
69	9.00	9.00	9.00	9.00	9.00	9.00

S-65E(Contd)	Gate 1	Gate 2	Gate 3	Gate 4	Gate 5	Gate 6
70	9.00	9.00	9.00	9.00	9.00	9.00
71	9.00	9.00	9.00	9.00	9.00	9.00
72	9.00	9.00	9.00	9.00	9.00	9.00
73	9.00	9.00	9.00	9.00	9.00	9.00
74	9.00	9.00	9.00	9.00	9.00	9.00
75	9.00	9.00	9.00	9.00	9.00	9.00
76	9.00	9.00	9.00	9.00	9.00	9.00
77	9.00	9.00	9.00	9.00	9.00	9.00
78	9.00	9.00	9.00	9.00	9.00	9.00
79	7.00	7.00	7.00	7.00	7.00	7.00
80	7.00	7.00	7.00	7.00	7.00	7.00
81	7.00	7.00	7.00	7.00	7.00	7.00
82	7.00	7.00	7.00	7.00	7.00	7.00
83	7.00	7.00	7.00	7.00	7.00	7.00
84	7.00	7.00	7.00	7.00	7.00	7.00
85	7.00	7.00	7.00	7.00	7.00	7.00
86	7.00	7.00	7.00	7.00	7.00	7.00
87	7.00	7.00	7.00	7.00	7.00	7.00
88	7.00	7.00	7.00	7.00	7.00	7.00
89	7.00	7.00	7.00	7.00	7.00	7.00
90	7.00	7.00	7.00	7.00	7.00	7.00
91	7.00	7.00	7.00	7.00	7.00	7.00
92	7.00	7.00	7.00	7.00	7.00	7.00
93	7.00	7.00	7.00	7.00	7.00	7.00
94	7.00	7.00	7.00	7.00	7.00	7.00
95	7.50	7.50	7.50	7.50	7.50	7.50
96	7.50	7.50	7.50	7.50	7.50	7.50
97	7.50	7.50	7.50	7.50	7.50	7.50
98	7.50	7.50	7.50	7.50	7.50	7.50
99	7.50	7.50	7.50	7.50	7.50	7.50
100	7.50	7.50	7.50	7.50	7.50	7.50
101	7.50	7.50	7.50	7.50	7.50	7.50
102	7.50	7.50	7.50	7.50	7.50	7.50
103	7.50	7.50	7.50	7.50	7.50	7.50
104	7.50	7.50	7.50	7.50	7.50	7.50
105	7.50	7.50	7.50	7.50	7.50	7.50
106	7.50	7.50	7.50	7.50	7.50	7.50
107	7.50	7.50	7.50	7.50	7.50	7.50
108	7.50	7.50	7.50	7.50	7.50	7.50
109	7.75	7.75	7.75	7.75	7.75	7.75
110	7.75	7.75	7.75	7.75	7.75	7.75
111	7.75	7.75	7.75	7.75	7.75	7.75
112	7.75	7.75	7.75	7.75	7.75	7.75
113	7.75	7.75	7.75	7.75	7.75	7.75
114	7.75	7.75	7.75	7.75	7.75	7.75
115	7.75	7.75	7.75	7.75	7.75	7.75
116	7.75	7.75	7.75	7.75	7.75	7.75
117	7.75	7.75	7.75	7.75	7.75	7.75
118	7.75	7.75	7.75	7.75	7.75	7.75
119	7.75	7.75	7.75	7.75	7.75	7.75
120	7.75	7.75	7.75	7.75	7.75	7.75
121	7.75	7.75	7.75	7.75	7.75	7.75
122	7.75	7.75	7.75	7.75	7.75	7.75
123	7.75	7.75	7.75	7.75	7.75	7.75
124	7.75	7.75	7.75	7.75	7.75	7.75
125	7.75	7.75	7.75	7.75	7.75	7.75
126	7.75	7.75	7.75	7.75	7.75	7.75
127	7.75	7.75	7.75	7.75	7.75	7.75
128	7.75	7.75	7.75	7.75	7.75	7.75

S-65E (Contd)

	Gate 1	Gate 2	Gate 3	Gate 4	Gate 5	Gate 6
129	7.75	7.75	7.75	7.75	7.75	7.75
130	7.75	7.75	7.75	7.75	7.75	7.75
131	7.75	7.75	7.75	7.75	7.75	7.75
132	7.75	7.75	7.75	7.75	7.75	7.75
133	7.75	7.75	7.75	7.75	7.75	7.75
134	7.75	7.75	7.75	7.75	7.75	7.75
135	7.75	7.75	7.75	7.75	7.75	7.75
136	7.75	7.75	7.75	7.75	7.75	7.75
137	7.75	7.75	7.75	7.75	7.75	7.75
138	7.75	7.75	7.75	7.75	7.75	7.75
139	7.75	7.75	7.75	7.75	7.75	7.75
140	7.75	7.75	7.75	7.75	7.75	7.75
141	7.75	7.75	7.75	7.75	7.75	7.75
142	7.75	7.75	7.75	7.75	7.75	7.75
143	7.75	7.75	7.75	7.75	7.75	7.75
144	7.75	7.75	7.75	7.75	7.75	7.75
145	7.75	7.75	7.75	7.75	7.75	7.75
146	7.75	7.75	7.75	7.75	7.75	7.75
147	7.75	7.75	7.75	7.75	7.75	7.75
148	7.75	7.75	7.75	7.75	7.75	7.75
149	7.75	7.75	7.75	7.75	7.75	7.75
150	7.75	7.75	7.75	7.75	7.75	7.75
151	7.75	7.75	7.75	7.75	7.75	7.75
152	7.75	7.75	7.75	7.75	7.75	7.75
153	7.75	7.75	7.75	7.75	7.75	7.75
154	7.75	7.75	7.75	7.75	7.75	7.75
155	7.00	7.00	7.00	7.00	7.00	7.00
156	7.00	7.00	7.00	7.00	7.00	7.00
157	7.00	7.00	7.00	7.00	7.00	7.00
158	6.00	6.00	6.00	6.00	6.00	6.00
159	6.00	6.00	6.00	6.00	6.00	6.00
160	6.00	6.00	6.00	6.00	6.00	6.00
161	6.00	6.00	6.00	6.00	6.00	6.00
162	6.00	6.00	6.00	6.00	6.00	6.00
163	6.00	6.00	6.00	6.00	6.00	6.00
164	6.00	6.00	6.00	6.00	6.00	6.00
165	6.00	6.00	6.00	6.00	6.00	6.00
166	6.00	6.00	6.00	6.00	6.00	6.00
167	6.00	6.00	6.00	6.00	6.00	6.00
168	5.00	5.00	5.00	5.00	5.00	5.00
169	5.00	5.00	5.00	5.00	5.00	5.00
170	5.00	5.00	5.00	5.00	5.00	5.00
171	5.25	5.25	5.25	5.25	5.25	5.25
172	5.25	5.25	5.25	5.25	5.25	5.25
173	5.25	5.25	5.25	5.25	5.25	5.25
174	5.25	5.25	5.25	5.25	5.25	5.25
175	5.25	5.25	5.25	5.25	5.25	5.25
176	5.25	5.25	5.25	5.25	5.25	5.25
177	5.25	5.25	5.25	5.25	5.25	5.25
178	5.25	5.25	5.25	5.25	5.25	5.25
179	5.25	5.25	5.25	5.25	5.25	5.25
180	5.25	5.25	5.25	5.25	5.25	5.25
181	5.25	5.25	5.25	5.25	5.25	5.25
182	5.25	5.25	5.25	5.25	5.25	5.25
183	5.25	5.25	5.25	5.25	5.25	5.25
184	5.25	5.25	5.25	5.25	5.25	5.25
185	5.25	5.25	5.25	5.25	5.25	5.25
186	5.25	5.25	5.25	5.25	5.25	5.25
187	5.25	5.25	5.25	5.25	5.25	5.25

S-65E(Contd)	Gate 1	Gate 2	Gate 3	Gate 4	Gate 5	Gate 6
188	5.25	5.25	5.25	5.25	5.25	5.25
189	5.25	5.25	5.25	5.25	5.25	5.25
190	5.25	5.25	5.25	5.25	5.25	5.25
191	5.25	5.25	5.25	5.25	5.25	5.25
192	5.25	5.25	5.25	5.25	5.25	5.25
193	5.00	5.00	5.00	5.00	5.00	5.00
194	5.00	5.00	5.00	5.00	5.00	5.00
195	5.00	5.00	5.00	5.00	5.00	5.00
196	5.00	5.00	5.00	5.00	5.00	5.00
197	5.00	5.00	5.00	5.00	5.00	5.00
198	5.00	5.00	5.00	5.00	5.00	5.00
199	5.25	5.25	5.25	5.25	5.25	5.25
200	5.25	5.25	5.25	5.25	5.25	5.25
201	5.25	5.25	5.25	5.25	5.25	5.25
202	5.25	5.25	5.25	5.25	5.25	5.25
203	5.00	5.25	5.25	5.25	5.25	5.25
204	5.00	5.25	5.25	5.25	5.25	5.25
205	5.00	5.25	5.25	5.25	5.25	5.25
206	5.00	5.25	5.25	5.25	5.25	5.25
207	5.00	5.25	5.25	5.25	5.25	5.25
208	5.00	5.25	5.25	5.25	5.25	5.25
209	5.00	5.00	5.00	5.00	4.75	4.75
210	5.00	5.00	5.00	5.00	4.75	4.75
211	5.00	5.00	5.00	5.00	4.75	4.75
212	5.00	5.00	5.00	5.00	4.75	4.75
213	5.00	5.00	5.00	5.00	4.75	4.75
214	5.00	5.00	5.00	5.00	4.75	4.75
215	5.00	5.00	5.00	5.00	4.75	4.75
216	5.00	5.00	5.00	5.00	4.75	4.75
217	5.00	5.00	4.50	5.00	4.75	4.75
218	5.00	5.00	4.50	5.00	4.75	4.75
219	5.00	5.00	4.50	5.00	4.75	4.75
220	5.00	5.00	4.50	5.00	4.75	4.75
221	5.00	5.00	4.50	5.00	4.75	4.75
222	5.00	5.00	4.50	5.00	4.75	4.75
223	5.00	5.00	5.00	5.00	5.00	5.00
224	5.00	5.00	5.00	5.00	5.00	5.00
225	5.00	5.00	5.00	5.00	5.00	5.00
226	4.25	5.00	5.00	5.00	5.00	5.00
227	4.25	5.00	5.00	5.00	5.00	5.00
228	4.25	5.00	5.00	5.00	5.00	5.00
229	4.25	5.00	5.00	5.00	5.00	5.00
230	4.25	5.00	5.00	5.00	5.00	5.00
231	4.25	5.00	5.00	5.00	5.00	5.00
232	4.25	5.00	5.00	5.00	5.00	5.00
233	4.25	5.00	5.00	5.00	5.00	5.00
234	4.25	5.00	5.00	5.00	5.00	5.00
235	4.25	5.00	5.00	5.00	5.00	5.00
236	4.25	5.00	5.00	5.00	5.00	5.00
237	4.25	5.00	5.00	5.00	5.00	5.00
238	4.25	5.00	5.00	5.00	5.00	5.00
239	4.25	4.50	4.50	4.50	4.50	4.50
240	4.25	4.50	4.50	4.50	4.50	4.50
241	4.25	4.50	4.50	4.50	4.50	4.50
242	4.25	4.50	4.50	4.50	4.50	4.50
243	4.25	4.50	4.50	4.50	4.50	4.50
244	4.25	4.50	4.50	4.50	4.50	4.50
245	4.25	4.50	4.50	4.50	4.50	4.50
246	4.25	4.50	4.50	4.50	4.50	4.50

S-65E (Contd)	Gate 1	Gate 2	Gate 3	Gate 4	Gate 5	Gate 6
247	4.25	4.50	4.50	4.50	4.50	4.50
248	4.25	4.50	4.50	4.50	4.50	4.50
249	4.25	4.50	4.50	4.50	4.50	4.50
250	4.25	4.50	4.50	4.50	4.50	4.50
251	4.25	4.50	4.50	4.50	4.50	4.50
252	4.25	4.50	4.50	4.50	4.50	4.50
253	4.25	4.50	4.50	4.50	4.50	4.50
254	4.25	4.50	4.50	4.50	4.50	4.50
255	4.25	4.50	4.50	4.50	4.50	4.50
256	4.25	4.50	4.50	4.50	4.50	4.50
257	4.25	4.50	4.50	4.50	4.50	4.50
258	4.25	4.50	4.50	4.50	4.50	4.50
259	4.25	4.50	4.50	4.50	4.50	4.50
260	4.25	4.50	4.50	4.50	4.50	4.50
261	4.25	4.50	4.50	4.50	4.50	4.50
262	4.25	4.50	4.50	4.50	4.50	4.50
263	4.25	4.50	4.50	4.50	4.50	4.50
264	4.25	4.50	4.50	4.50	4.50	4.50
265	4.25	4.50	3.75	4.50	4.50	4.50
266	4.25	4.50	3.75	4.50	4.50	4.50
267	4.25	4.50	3.75	4.50	4.50	4.50
268	4.25	4.50	3.75	4.50	4.50	4.50
269	4.25	4.50	3.75	4.50	4.50	4.50
270	4.25	4.50	3.75	4.50	4.50	4.50
271	4.25	4.50	3.75	4.50	4.50	4.50
272	4.25	4.50	3.75	4.50	4.50	4.50
273	4.25	4.50	3.75	4.50	4.50	4.50
274	4.25	4.50	3.75	4.50	4.50	4.50
275	4.25	4.50	3.75	4.50	4.50	4.50
276	4.25	4.50	3.75	4.50	4.50	3.75
277	4.25	4.50	3.75	4.50	4.50	3.75
278	4.25	4.50	3.75	4.50	4.50	3.75
279	4.25	4.50	3.75	4.50	4.50	3.75
280	4.25	4.50	3.75	4.50	4.50	3.75
281	4.25	4.50	3.75	4.50	4.50	3.75
282	4.25	4.50	3.75	4.50	4.50	3.75
283	4.25	4.50	3.75	4.50	4.50	3.75
284	4.25	4.50	3.75	4.50	4.50	3.75
285	4.25	4.50	3.75	4.50	4.50	3.75
286	4.25	4.50	3.75	4.50	4.50	3.75
287	4.25	4.50	3.75	4.50	4.50	3.75
288	4.25	4.50	3.75	4.50	4.50	3.75
289	4.25	4.25	3.75	4.50	4.50	3.75
290	4.25	4.25	3.75	4.50	4.50	3.75
291	4.25	4.25	3.75	4.50	4.50	3.75
292	4.25	4.25	3.75	4.50	4.50	3.75
293	4.25	4.25	3.75	4.50	4.50	3.75
294	4.25	4.25	3.75	4.50	4.00	3.75
295	4.25	4.25	3.75	4.50	4.00	3.75
296	4.25	4.25	3.75	4.50	4.00	3.75
297	4.25	4.25	3.75	4.50	4.00	3.75
298	4.25	4.25	3.75	4.50	4.50	4.00
299	4.25	4.25	3.75	4.50	4.50	4.00
300	4.25	4.25	3.75	4.50	4.50	4.00
301	4.25	4.25	3.75	4.50	4.50	4.00
302	4.25	4.25	3.75	4.50	4.50	4.00
303	4.25	4.25	3.75	4.50	4.50	4.00
304	4.25	4.25	3.75	4.50	4.50	4.00
305	4.25	4.25	3.75	4.50	4.50	4.00

<u>S-65E (Contd.)</u>	<u>Gate 1</u>	<u>Gate 2</u>	<u>Gate 3</u>	<u>Gate 4</u>	<u>Gate 5</u>	<u>Gate 6</u>
306	4.25	4.25	3.75	4.50	4.50	4.00
307	4.25	4.25	3.75	4.50	4.50	4.00
308	4.25	4.25	3.75	4.50	4.50	4.00
309	4.25	4.25	3.75	4.50	4.50	4.00
310	4.25	4.25	3.75	4.50	4.50	4.00
311	4.25	4.25	3.75	4.50	4.50	4.00
312	4.25	4.25	3.75	4.50	4.50	4.00
313	4.25	4.25	3.75	4.25	4.00	4.00
314	4.25	4.25	3.75	4.25	4.00	4.00
315	4.25	4.25	3.75	4.25	4.00	4.00
316	4.25	4.25	3.75	4.25	4.00	4.00
317	4.25	4.25	3.75	4.25	4.00	4.00
318	4.25	4.25	3.75	4.25	4.00	4.00
319	4.25	4.25	3.75	4.25	4.00	4.00
320	4.25	4.25	3.75	4.25	4.00	4.00
321	4.25	4.25	3.75	4.25	4.00	4.00
322	4.25	4.25	3.75	4.25	4.00	4.00
323	4.25	4.25	3.75	4.25	4.00	4.00
324	4.25	4.25	3.75	4.25	4.00	4.00
325	4.25	4.25	3.75	4.25	4.00	4.00
326	4.25	4.25	3.75	4.25	4.00	4.00
327	4.25	4.25	3.75	4.25	4.00	4.00
328	4.25	4.25	3.75	4.25	4.00	4.00
329	4.25	4.25	3.75	4.25	4.00	4.00
330	4.25	4.25	3.75	4.25	4.00	4.00
331	4.25	4.25	3.75	4.25	4.00	4.00
332	4.25	4.25	3.75	4.25	4.00	4.00
333	4.25	4.25	3.75	4.25	4.00	4.00
334	4.25	4.25	3.75	4.25	4.00	4.00
335	4.25	4.25	3.75	4.25	4.00	4.00
336	4.25	4.25	3.75	4.25	4.00	4.00
337	4.25	4.25	3.75	4.25	4.00	4.00
338	4.25	4.25	3.75	4.25	4.00	4.00
339	4.25	4.25	3.75	4.25	4.00	4.00
340	4.25	4.25	3.75	4.25	4.00	4.00
341	4.25	4.25	3.75	4.25	4.00	4.00
342	4.25	4.25	3.75	4.25	4.00	4.00

Time

7.9 Damage Pattern Downstream of S-650

Explanatory notes pertaining to the figure.

Numbers in red are the design elevation.

Numbers in blue are the soundings taken shortly after
high flows.



7.10 Hourly Stage and Discharge Values for S-65E, S-65D, S-65C
and S-65B.

Explanatory notes pertaining to the listings.

CANAL C-38 ED: Identification of the reach between S-65E and S-65D.

CANAL C-38 DC: Identification of the reach between S-65D and S-65C.

CANAL C-38 CB: Identification of the reach between S-65C and S-65B.

DAY: The calendar day number of the month of October in the year 1969.

TIME: Actual clock time of the day = 1, 2, ..., 23, 24.

1 corresponds to 1:00AM of the day and 24 corresponds to Midnight of the day.

HWEU: Recorded headwater elevation at the upstream structure for the reach, ft.

TWED: Recorded tailwater elevation in the case of S-65E and computed tailwater elevation in case of S-65D, S-65C and S-65B, ft.

HWED: Recorded headwater elevation at the downstream structure for the reach, ft.

COMP TWEU: Computed tailwater elevation at the upstream structure for the reach, ft.

COMP DH: COMP TWEU - HWED, in ft.

OBS TWEU: Recorded tailwater elevation at the upstream structure for the reach, ft.

OBS DH: OBS TWEU - HWED, in ft.

DIFF: COMP TWEU - OBS TWEU, in ft.

QUP: Discharge through the upstream structure for the reach, cfs.

QDN: Discharge through the downstream structure for the reach,
cfs.

QL: Lateral inflow = QDN - QUP in cfs.

All the stage values are adjusted for error in datum plus a
constant of 12 feet.

CANAL C-38E)

LAY	TIN	HMEU	THED	ThETD	CMP	TxFU	UHS	UHS	UHS	UHS	TWEW	GHS	DH	0.1HF	QDP	QD*	QL
3*	6.00	43.05	28.02	34.06	34.97	0.9115	33.76	-0.0900	1.0076	1.8769	3	23876.5	5127.1				
3*	9.00	41.05	27.93	34.09	35.02	0.9426	34.01	-0.0733	0.6484	1.8804	5	24176.8	5347.3				
3*	10.00	41.12	27.83	34.13	34.90	0.7762	34.05	-0.0800	0.8592	1.7511	7	21956.1	4477.3				
3*	11.00	41.23	27.75	34.07	34.70	0.6368	34.16	-0.0899	0.5488	1.7924	9	19576.0	16217.6				
3*	12.00	41.35	27.68	34.25	34.88	0.4382	34.38	-0.0239	0.6809	1.7765	11	19717.5	19134.6				
3*	13.00	41.46	27.66	34.43	35.06	0.6374	34.29	-0.0339	0.6754	1.7765	13	19439.5	21494.2				
3*	14.00	41.58	27.92	34.61	35.11	0.5010	34.51	-0.0939	0.5010	1.7871	15	18517.1	17621.1				
3*	15.00	41.62	27.67	34.79	35.29	0.5078	34.56	-0.2390	0.7358	1.7682	17	17628.2	2444.2				
3*	16.00	41.69	27.67	34.87	35.47	0.5695	34.62	-0.3500	0.8579	1.7506	19	18213.5	7047.9				
3*	17.00	41.75	27.79	35.16	35.81	0.6301	34.98	-0.4898	1.1303	1.7124	21	21179.0	40349.4				
3*	18.00	41.81	27.79	35.18	35.98	0.8074	34.74	-0.4359	1.2426	1.6930	22	6882.2	23842.2				
3*	19.00	41.87	27.83	35.87	35.98	0.7935	34.40	-0.4800	1.7196	1.7196	23	23611.8	6613.4				
3*	20.00	41.93	27.87	34.98	35.77	0.7942	34.86	-0.1200	0.1142	1.7434	24	23379.1	5946.6				
3*	21.00	41.95	27.92	34.88	35.66	0.7684	34.87	-0.0000	0.7834	1.7607	25	15127.2	55117.5				
3*	22.00	41.98	27.96	34.79	35.57	0.7634	34.81	-0.1199	0.6634	1.7784	26	22906.8	51228.8				
3*	23.00	42.01	28.01	34.69	35.46	0.7751	34.94	-0.2497	0.2497	1.7970	27	22667.1	46796.3				
3*	24.00	42.04	28.05	34.80	35.37	0.7716	34.96	-0.3695	0.4016	1.8147	28	22442.9	4281.2				
3*	25.00	42.07	28.05	34.52	35.29	0.7704	35.00	-0.4709	0.4709	1.7939	29	22225.4	3989.7				
4*	1.00	42.10	28.07	34.44	35.20	0.7680	35.03	-0.4873	0.1790	1.9667	30	21277.4	3630.0				
4*	2.00	42.11	28.07	34.62	35.12	0.7652	35.04	-0.6800	0.0852	1.8576	31	21968.3	33961.1				
4*	3.00	42.11	28.08	34.55	35.04	0.7623	35.05	-0.0706	0.0876	1.8848	32	21800.1	51148.8				
4*	4.00	42.12	28.14	34.26	35.18	0.7533	35.06	-0.8939	-0.1416	1.8881	33	21578.7	26932.7				
4*	5.00	42.14	28.09	34.16	34.91	0.7528	35.08	-0.0399	0.1957	1.8057	34	21320.5	22621.6				
4*	6.00	42.15	28.11	34.06	34.79	0.7639	35.09	-1.1699	-0.4230	1.9233	35	21065.3	19303.3				
4*	7.00	42.16	28.13	33.92	34.66	0.7639	35.11	-1.4000	-0.5588	1.9400	36	20821.8	10153.3				
4*	8.00	42.18	28.15	33.81	34.55	0.7411	35.14	-1.5494	-0.1629	1.9497	37	20728.4	1231.0				
4*	9.00	42.19	28.14	33.75	34.49	0.7433	34.94	-1.0899	-0.3629	1.9497	38	20728.4	10779.5				
4*	10.00	42.20	28.13	33.70	34.43	0.7398	34.57	-0.4700	-0.1301	1.9575	39	20653.0	20653.0				
4*	11.00	42.21	28.13	33.65	34.38	0.7340	34.30	-0.5500	-0.0851	1.9581	40	20558.6	9017.8				
4*	12.00	42.21	28.13	33.59	34.32	0.7338	34.03	-0.3399	0.2958	1.9741	41	20444.8	7033.0				
4*	13.00	42.23	28.12	33.56	34.27	0.7351	33.76	-0.2139	0.1817	1.9817	42	20468.6	5511.7				
4*	14.00	42.25	28.12	33.49	33.95	0.7465	33.60	-0.0909	0.4554	1.8407	43	15159.9	24747.6				
4*	15.00	42.26	28.13	33.42	33.73	0.7473	33.60	-0.1699	0.6433	1.8406	44	12151.6	-19251.6				
4*	16.00	42.20	28.09	33.77	34.24	0.7411	33.71	-0.3620	0.8702	1.7671	45	16264.5	-1226.8				
4*	17.00	42.23	28.01	34.05	34.53	0.4812	33.02	-0.4300	0.9177	1.7767	46	17669.5	-6669.5				
4*	18.00	42.25	27.95	34.44	34.73	0.4877	33.62	-0.4300	1.0104	1.6643	47	721.9	-17650.3				
4*	19.00	42.25	27.98	34.53	34.94	0.4914	33.93	-0.3200	1.0104	1.6643	48	17650.3	1445.5				
4*	20.00	42.28	28.01	34.61	35.09	0.4876	33.99	-0.5349	1.0246	1.6621	49	16472.9	8111.0				
4*	21.00	42.26	28.04	34.69	35.17	0.4878	34.06	-0.5500	1.0348	1.6611	50	16750.3	6986.6				
4*	22.00	42.21	28.08	34.78	35.26	0.4879	34.12	-0.7700	1.0579	1.6590	51	17567.5	9771.1				
4*	23.00	42.25	28.11	34.86	35.34	0.4879	34.19	-0.5999	1.0764	1.6569	52	17634.5	10644.7				
4*	24.00	42.25	28.01	34.25	34.73	0.4877	34.26	-0.3620	1.0805	1.6559	53	17711.2	1411.4				
5*	1.00	42.27	28.01	35.00	35.48	0.4840	34.53	-0.6200	1.1040	1.6539	54	17767.7	-1226.8				
5*	2.00	42.27	28.13	35.00	35.48	0.4853	34.53	-0.6400	1.1258	1.6514	55	17650.3	1445.5				
5*	3.00	42.21	28.11	35.06	35.54	0.4876	34.39	-0.6600	1.1456	1.6479	56	1765.7	1866.5				
5*	4.00	42.25	28.09	35.12	35.60	0.4894	34.43	-0.6819	1.1744	1.6454	57	18070.4	1465.6				
5*	5.00	43.01	28.04	35.18	35.67	0.4911	34.46	-0.7119	1.2117	1.6415	58	1817.5	1615.6				
5*	6.00	43.05	28.03	35.24	35.73	0.4933	34.49	-0.1500	1.2433	1.6382	59	1908.1	17408.1				
5*	7.00	43.07	28.05	35.21	35.85	0.5026	34.53	-0.1700	1.3272	1.6285	60	1908.1	34111.1				
5*	8.00	43.07	28.05	35.21	35.85	0.5055	34.53	-0.1719	1.3272	1.6285	61	1908.1	32253.3				

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TIME (HRS) 8:00 A.M. 9:00 A.M. 10:00 A.M. 11:00 A.M. 12:00 P.M. 1:00 P.M. 2:00 P.M. 3:00 P.M. 4:00 P.M. 5:00 P.M. 6:00 P.M. 7:00 P.M.

DAY	TIME	HEAD	HWD	COMP	TWEU	CWT	IN	OUT	QUP	DWN	QL	DWN	QL
							IN	OUT	IN	OUT	IN	OUT	IN
1	7.00	41.77	28.125	24.84	35.40	0.5691	33.82	-0.10199	1.5891	16118.1	19164.4	3546.2	3546.2
2	8.00	41.66	28.125	24.84	35.36	0.5679	33.71	-0.10800	1.66779	16030.8	19129.6	3373.8	3373.8
3	9.00	41.56	28.125	24.84	35.32	0.5660	33.62	-0.12100	1.70600	16030.8	19129.6	3272.8	3272.8
4	10.00	41.45	28.125	24.84	35.28	0.5647	33.51	-0.12700	1.77747	15868.4	19169.4	3301.0	3301.0
5	11.00	41.35	28.125	24.84	35.24	0.5632	33.41	-0.13099	1.8227	15793.6	19033.3	3303.9	3303.9
6	12.00	41.24	28.125	24.84	35.21	0.5618	33.37	-0.0999	1.8708	15692.2	19033.3	3301.2	3301.2
7	13.00	41.14	28.125	24.84	35.18	0.5595	33.31	-0.0599	1.9372	15515.7	18896.6	3356.7	3356.7
8	14.00	41.03	28.125	24.84	35.15	0.5574	34.01	-0.16000	0.7174	15526.6	18896.2	3369.6	3369.6
9	15.00	40.93	28.125	24.84	35.12	0.5547	34.75	-0.2099	0.3376	13911.9	18835.0	4923.1	4923.1
10	16.00	40.86	28.125	24.84	35.08	0.5534	34.52	-0.2599	0.2742	12504.9	18816.6	5911.7	5911.7
11	17.00	40.76	28.125	24.84	35.04	0.5524	34.39	-0.3099	0.0289	12800.3	18764.6	3644.2	3644.2
12	18.00	40.67	28.125	24.84	35.00	0.5483	34.25	-0.3499	0.0889	12709.0	18712.0	3324.0	3324.0
13	19.00	40.58	28.125	24.84	34.96	0.5438	34.12	-0.3899	0.1382	12800.0	18684.6	3304.0	3304.0
14	20.00	40.49	28.125	24.84	34.92	0.5438	34.01	-0.4299	0.1799	11267.9	25755.0	25755.0	25755.0
15	21.00	40.41	28.125	24.84	34.88	0.5431	33.90	-0.4699	0.0591	11253.3	31357.9	25204.1	25204.1
16	22.00	40.32	28.125	24.84	34.84	0.5426	33.82	-0.5099	0.0799	11231.7	18689.4	2432.2	2432.2
17	23.00	40.22	28.125	24.84	34.79	0.5387	33.75	-0.2600	0.0865	11211.3	18606.1	2394.8	2394.8
18	24.00	40.12	28.125	24.84	34.75	0.5326	33.78	-0.2399	0.0844	11204.3	18504.3	2299.8	2299.8
19	25.00	40.02	28.125	24.84	34.71	0.5322	33.74	-0.2199	0.1025	11179.0	18427.5	2248.5	2248.5
20	26.00	39.94	28.125	24.84	34.67	0.5324	33.70	-0.2399	0.2100	11152.3	18350.2	2196.8	2196.8
21	27.00	39.87	28.125	24.84	34.63	0.5318	33.57	-0.2199	0.1110	11152.3	18350.2	2196.8	2196.8
22	28.00	39.80	28.125	24.84	34.60	0.5311	33.50	-0.1999	0.1088	11146.4	2100.0	2100.0	2100.0
23	29.00	39.71	28.125	24.84	34.56	0.5306	33.44	-0.1999	0.1174	11120.5	31381.2	2060.7	2060.7
24	30.00	39.62	28.125	24.84	34.52	0.5301	33.38	-0.1899	0.1253	11104.4	18089.4	1985.0	1985.0
25	31.00	39.51	28.125	24.84	34.48	0.5295	33.31	-0.1800	0.0424	10376.9	18089.4	4494.8	4494.8
26	32.00	39.46	28.125	24.84	34.44	0.5222	33.30	-0.0699	0.1567	10244.7	10202.8	777.1	777.1
27	33.00	39.40	28.125	24.84	34.40	0.5226	33.30	-0.02000	0.02045	10172.3	10002.1	829.8	829.8
28	34.00	39.35	28.125	24.84	34.36	0.5220	33.30	-0.03000	0.22225	10088.4	15191.1	1430.6	1430.6
29	35.00	39.31	28.125	24.84	34.32	0.5215	33.30	-0.03000	0.2529	10071.0	15151.1	1430.6	1430.6
30	36.00	39.26	28.125	24.84	34.28	0.5210	33.30	-0.03000	0.2329	10050.8	15050.8	1453.0	1453.0
31	37.00	39.21	28.125	24.84	34.24	0.5205	33.30	-0.03000	0.1929	10027.9	11484.7	1456.7	1456.7
32	38.00	39.17	28.125	24.84	34.20	0.5200	33.30	-0.0799	0.1632	10011.7	11473.2	1454.1	1454.1
33	39.00	39.14	28.125	24.84	34.16	0.5195	33.30	-0.0999	0.1432	10001.7	11461.7	1460.0	1460.0
34	40.00	39.12	28.125	24.84	34.12	0.5191	33.30	-0.1099	0.1334	9984.1	11461.7	1477.2	1477.2
35	41.00	39.10	28.125	24.84	34.08	0.5186	33.30	-0.1299	0.1134	9966.8	11450.2	1483.1	1483.1
36	42.00	39.06	28.125	24.84	34.04	0.5181	33.30	-0.1500	0.0934	9944.4	11438.6	1489.2	1489.2
37	43.00	39.02	28.125	24.84	34.00	0.5176	33.30	-0.1699	0.0138	9940.3	11438.6	1498.3	1498.3
38	44.00	38.98	28.125	24.84	33.96	0.5171	33.30	-0.1899	0.0538	9922.8	11427.1	1504.3	1504.3
39	45.00	38.94	28.125	24.84	33.92	0.5166	33.30	-0.2100	0.0324	9536.1	11411.6	1879.5	1879.5
40	46.00	38.90	28.125	24.84	33.88	0.5161	33.30	-0.2400	0.0023	9551.0	11392.4	1839.4	1839.4
41	47.00	38.86	28.125	24.84	33.84	0.5156	33.30	-0.2500	-0.0073	9561.1	11392.4	1831.3	1831.3
42	48.00	38.82	28.125	24.84	33.80	0.5151	33.30	-0.2699	-0.0271	9560.9	11392.4	1831.3	1831.3
43	49.00	38.78	28.125	24.84	33.76	0.5146	33.30	-0.2433	-0.0266	9560.5	11404.0	1843.4	1843.4
44	50.00	38.74	28.125	24.84	33.72	0.5141	33.30	-0.2699	-0.0266	9561.5	11404.0	1843.4	1843.4
45	51.00	38.70	28.125	24.84	33.68	0.5136	33.30	-0.2800	-0.0362	9561.7	11415.6	1863.8	1863.8
46	52.00	38.66	28.125	24.84	33.64	0.5131	33.30	-0.2900	-0.0459	9561.5	11415.6	1864.0	1864.0
47	53.00	38.62	28.125	24.84	33.60	0.5126	33.30	-0.3000	-0.0555	9551.2	11427.1	1875.9	1875.9

CANAL C-38 SEP 1974

DAY	TIME	HWD	LTD	HWD	CMP TWEU	CMP HWD	COHP UN	OBS TWEU	OBS HWD	DIFF	QUP	QDN	QL
11.	8.00	38.80	28.10	32.87	33.04	0.1719	33.15	0.2800	-0.1080	9442.8	1077.6		
11.	8.00	38.80	28.05	32.67	33.04	0.1722	33.15	0.2800	-0.1077	8368.8	1083.9		
11.	10.00	38.81	28.00	32.68	33.05	0.1723	33.14	0.2559	-0.0876	9452.9	1096.0		
11.	11.00	38.81	28.00	32.69	33.06	0.1725	33.14	0.2500	-0.0774	8361.4	9472.9	1111.4	
11.	12.00	38.81	28.00	32.70	33.07	0.1726	33.14	0.2400	-0.0673	9488.9	1128.8		
11.	13.00	38.81	28.00	32.70	33.07	0.1726	33.14	0.2400	-0.0673	8354.1	9482.9	1128.8	
11.	14.00	38.81	28.00	32.71	33.08	0.1727	33.12	0.2199	-0.0472	8366.6	9492.9	1144.2	
11.	15.00	38.82	28.00	32.92	33.09	0.1729	33.12	0.2090	-0.0370	8352.9	9502.9	1155.3	
11.	16.00	38.82	28.00	32.93	33.10	0.1730	33.12	0.1999	-0.0269	8339.2	9512.9	1177.7	
11.	17.00	38.82	28.00	32.93	33.10	0.1730	33.12	0.1989	-0.0269	8339.2	9512.9	1177.7	
11.	18.00	38.82	28.00	32.94	33.11	0.1732	33.12	0.1899	-0.0167	8331.8	9522.9	1191.1	
11.	19.00	38.82	28.00	32.95	33.12	0.1733	33.12	0.1799	-0.0066	8331.4	9532.9	1208.4	
11.	20.00	38.83	28.00	32.95	33.12	0.1733	33.12	0.1799	-0.0066	8331.1	9532.9	1208.4	
11.	21.00	38.83	28.00	32.96	33.13	0.1738	33.12	0.1599	-0.0340	8316.6	9562.8	1227.7	
11.	22.00	38.83	28.00	32.97	33.14	0.1739	33.12	0.1499	-0.0239	8316.6	9562.8	1246.0	
11.	23.00	38.83	28.00	32.98	33.15	0.1740	33.12	0.1399	-0.0139	8309.1	9582.6	1267.4	
11.	24.00	38.84	28.00	32.99	33.16	0.1742	33.12	0.1299	-0.0042	8309.1	9582.6	1273.4	
12.	1.00	38.94	28.00	32.99	33.16	0.1742	33.12	0.1299	-0.0042	8309.1	9582.6	1273.4	
12.	2.00	38.94	28.00	33.00	33.17	0.1743	33.12	0.1199	-0.0054	8301.7	9592.5	1290.7	
12.	3.00	38.94	28.00	33.01	33.17	0.1744	33.12	0.1099	-0.0064	8294.3	9602.4	1308.0	
12.	4.00	38.95	28.00	33.02	33.18	0.1746	33.11	0.0900	-0.0084	8294.2	9612.3	1318.0	
12.	5.00	38.95	28.00	33.02	33.19	0.1746	33.11	0.0900	-0.0084	8294.2	9612.3	1318.0	
12.	6.00	38.95	28.00	33.03	33.20	0.1747	33.11	0.0800	-0.0094	8286.7	9622.1	1333.4	
12.	7.00	38.95	28.00	33.03	33.21	0.1747	33.11	0.0699	-0.0106	8279.3	9632.0	1357.7	
12.	8.00	38.95	28.00	33.05	33.21	0.1661	33.11	0.0600	-0.0106	8278.4	9371.0	1092.6	
12.	9.00	38.96	28.00	33.05	33.19	0.1659	33.11	0.0600	-0.0085	8306.0	9351.9	1051.2	
12.	10.00	38.96	28.00	33.04	33.18	0.1658	33.11	0.0600	-0.0076	8308.0	9342.3	1034.2	
12.	11.00	38.96	28.00	33.04	33.18	0.1653	33.10	0.0600	-0.0073	8323.0	9323.0	1007.4	
12.	12.00	38.96	28.00	33.04	33.18	0.1652	33.10	0.0599	-0.0065	8333.0	9313.4	990.3	
12.	13.00	38.97	28.00	32.99	33.15	0.1651	33.10	0.1100	-0.0551	9304.8	9662.0		
12.	14.00	38.97	28.00	32.99	33.15	0.1646	33.10	0.1299	-0.0346	8352.7	9274.8	1511.7	
12.	15.00	38.97	28.00	32.96	33.12	0.1644	33.10	0.1400	-0.0244	8360.0	9265.1	903.0	
12.	16.00	38.97	28.00	32.95	33.11	0.1643	33.10	0.1500	-0.0143	8367.4	9255.4	888.0	
12.	17.00	38.97	28.00	32.94	33.11	0.1703	33.10	0.1599	-0.0103	1047.2	9236.0	-1181.1	
12.	18.00	38.97	28.00	32.94	33.11	0.1702	33.10	0.1599	-0.0102	1046.4	9226.3	-1200.0	
12.	19.00	38.97	28.00	32.93	33.10	0.1652	33.09	0.1699	-0.0087	1045.6	9226.3	-1507.8	
12.	20.00	38.97	28.00	32.92	33.08	0.1612	33.09	0.1699	-0.0087	1045.6	9226.3	-1511.7	
12.	21.00	38.98	28.00	32.92	33.08	0.1612	33.09	0.1699	-0.0012	1045.5	9240.7	-1511.7	
12.	22.00	38.98	28.00	32.92	33.08	0.1612	33.08	0.1699	-0.0012	10461.5	9240.7	-1520.7	
12.	23.00	38.98	28.00	32.92	33.08	0.1612	33.07	0.1500	-0.0112	10461.5	9236.0	-1511.1	
12.	24.00	38.98	28.00	32.93	33.09	0.1614	33.07	0.1400	-0.0214	10461.3	9236.0	-1511.1	
13.	1.00	38.98	28.00	32.93	33.09	0.1614	33.07	0.1400	-0.0214	10461.3	9236.0	-1511.1	
13.	2.00	38.98	28.00	32.93	33.09	0.1614	33.07	0.1400	-0.0214	1047.0	9226.3	-1520.0	
13.	3.00	38.99	28.00	32.93	33.09	0.1614	33.07	0.1400	-0.0214	1047.0	9226.3	-1510.5	
13.	4.00	38.99	28.00	32.94	33.10	0.1615	33.05	0.1099	-0.0515	1047.0	8959.6	-1510.5	
13.	5.00	38.99	28.00	32.94	33.05	0.1615	33.05	0.1099	-0.0515	1047.0	8959.6	-1510.5	
13.	6.00	38.99	28.00	32.94	33.05	0.1615	33.05	0.1099	-0.0515	1047.0	8959.6	-1510.5	
13.	7.00	38.99	28.00	32.94	33.05	0.1615	33.05	0.1099	-0.0515	1047.0	8959.6	-1510.5	

CANAL C-38EC

DAY	TIME	HMEU	TWED	HMED	COMP	TWEN	COMP DH	OBS DH	ODN	QD
13.	8.00	38.95	28.12	32.95	33.10	0.1314	33.05	0.0939	0.0514	8040.3
13.	9.00	38.95	28.10	32.93	33.08	0.1518	33.05	0.1200	0.0318	8076.6
13.	10.00	38.99	28.09	32.91	33.05	0.1519	33.06	0.1499	0.0317	8080.1
13.	11.00	39.01	28.08	32.90	33.05	0.1521	33.07	0.1700	0.0317	8087.0
13.	12.00	39.03	28.07	32.88	33.03	0.1522	33.07	0.1899	0.0337	8124.3
13.	13.00	39.05	28.06	32.87	33.01	0.1470	33.08	0.2100	0.0629	8861.4
13.	14.00	39.07	28.05	32.89	33.03	0.1464	33.09	0.2100	0.0629	8867.4
13.	15.00	39.13	28.13	32.92	33.00	0.1465	33.09	0.1999	0.0535	8175.7
13.	16.00	39.09	28.18	32.94	33.08	0.1453	33.09	0.1800	0.0338	8665.5
13.	17.00	39.09	28.22	32.97	33.12	0.1527	33.09	0.1499	-0.0046	8444.0
13.	18.00	39.09	28.20	32.96	33.11	0.1531	33.08	0.1099	0.0427	8893.3
13.	19.00	39.08	28.19	32.96	33.11	0.1334	33.07	0.1200	0.0331	8422.4
13.	20.00	39.08	28.17	32.96	33.11	0.1450	33.07	0.1100	0.0434	8912.3
13.	21.00	39.07	28.16	32.95	33.10	0.1452	33.06	0.1100	0.0440	8421.8
13.	22.00	39.07	28.14	32.95	33.10	0.1458	33.06	0.1099	0.0442	8774.6
13.	23.00	39.07	28.13	32.95	33.10	0.1530	33.05	0.0999	0.0548	8931.3
13.	24.00	39.06	28.11	32.95	33.10	0.1536	33.05	0.0993	0.0550	8421.1
14.	1.00	39.06	28.10	32.94	33.09	0.1538	33.04	0.0900	0.0556	8678.5
14.	2.00	39.06	28.09	32.94	33.09	0.1564	33.03	0.0899	0.0558	8420.5
14.	3.00	39.05	28.07	32.94	33.09	0.1567	33.02	0.0799	0.0664	8799.3
14.	4.00	39.05	28.05	32.94	33.09	0.1573	33.02	0.0799	0.0767	8412.8
14.	5.00	39.05	28.04	32.93	33.08	0.1574	33.01	0.0799	0.0773	8412.4
14.	6.00	39.04	28.02	32.93	33.08	0.1580	33.01	0.0800	0.0774	8925.5
14.	7.00	39.04	28.01	32.93	33.08	0.1583	33.00	0.0809	0.0780	8411.9
14.	8.00	39.04	28.00	32.93	33.07	0.1493	33.00	0.0699	0.0783	8411.7
14.	9.00	39.04	28.00	32.92	33.06	0.1492	33.00	0.0799	0.0692	8133.1
14.	10.00	39.04	28.00	32.92	33.06	0.1492	33.00	0.0799	0.0692	8133.1
14.	11.00	39.03	28.00	32.92	33.06	0.1491	33.00	0.0799	0.0691	8120.9
14.	12.00	39.03	28.00	32.92	33.06	0.1491	33.00	0.0799	0.0691	8784.1
14.	13.00	39.03	28.00	32.92	33.06	0.1491	33.00	0.0799	0.0691	8120.3
14.	14.00	39.03	28.00	32.92	33.06	0.1491	33.00	0.0799	0.0691	8784.1
14.	15.00	39.03	28.01	32.91	33.05	0.1488	33.00	0.0899	0.0588	8133.4
14.	16.00	39.03	28.01	32.91	33.05	0.1488	33.00	0.0899	0.0588	8133.4
14.	17.00	39.03	28.01	32.91	33.05	0.1488	33.00	0.0899	0.0588	8133.4
14.	18.00	39.03	28.01	32.91	33.05	0.1488	33.00	0.0899	0.0588	8133.4
14.	19.00	39.03	28.01	32.91	33.05	0.1488	33.00	0.0899	0.0588	8133.4
14.	20.00	39.02	28.01	32.90	33.04	0.1488	33.00	0.0999	0.0588	8133.4
14.	21.00	39.02	28.01	32.90	33.04	0.1488	33.00	0.1099	0.0588	8133.4
14.	22.00	39.02	28.01	32.90	33.04	0.1488	33.00	0.1099	0.0588	8133.4
15.	1.00	39.02	28.01	32.90	33.04	0.1488	33.00	0.1099	0.0588	8133.4
15.	2.00	39.02	28.01	32.90	33.04	0.1488	33.00	0.1099	0.0588	8133.4
15.	3.00	39.02	28.01	32.89	33.03	0.1488	33.00	0.1099	0.0588	8133.4
15.	4.00	39.02	28.01	32.89	33.03	0.1488	33.00	0.1099	0.0588	8133.4
15.	5.00	39.02	28.01	32.89	33.03	0.1488	33.00	0.1099	0.0588	8133.4
15.	6.00	39.02	28.01	32.89	33.03	0.1488	33.00	0.1099	0.0588	8133.4
15.	7.00	39.01	28.01	32.89	33.03	0.1488	33.00	0.1099	0.0588	8133.4
15.	8.00	39.01	28.01	32.89	33.03	0.1488	33.00	0.1099	0.0588	8133.4
15.	9.00	39.01	28.01	32.89	33.03	0.1488	33.00	0.1099	0.0588	8133.4
15.	10.00	39.01	28.01	32.88	33.02	0.1488	33.00	0.1199	0.0588	8140.8
15.	11.00	39.01	28.01	32.87	33.01	0.1488	33.00	0.1299	0.0588	8147.5
15.	12.00	39.01	28.01	32.87	33.01	0.1488	33.00	0.1299	0.0588	8120.4
15.	13.00	39.01	28.01	32.87	33.01	0.1488	33.00	0.1299	0.0588	8147.5

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CANAL C-38DC

DAY	TIME	HHRW	COMP THFU	HWEW	COMP DH	DSW	OHS-THEW	DSW	OHS-DHW	DSW	OHS-DHF	DHF	ODW
0	10:00	47.80	42.42	40.98	4.4419	4.50	0.5200	0.9219	15626.2	18760.3	3345.1		
1	10:00	47.80	42.42	40.98	4.4390	4.50	0.4500	0.9868	18808.1	3345.1			
2	10:00	47.80	42.42	40.98	4.4390	4.50	0.7800	0.4679	14254.3	17511.6	3287.5		
3	10:00	47.80	42.42	40.98	4.2479	4.50	0.4500	1.1117	14472.3	17942.4	3408.4		
4	11:00	47.70	42.30	41.23	42.51	4.50	0.1699	2.2037	14221.6	17860.5	3288.6		
5	12:00	47.70	42.30	41.23	42.60	4.50	-0.9500	2.2336	14747.6	17766.0	31663.3		
6	13:00	47.70	42.30	41.23	42.60	4.50	-1.0099	1.3925	14429.6	17810.5	3440.9		
7	14:00	47.75	42.35	41.46	42.68	4.50	-0.1800	1.3623	14332.0	17681.3	3113.3		
8	15:00	47.80	42.42	40.98	42.79	4.50	-0.1799	1.3546	14693.8	17509.7	3015.9		
9	16:00	48.05	42.57	41.69	42.84	4.50	-0.1899	1.3549	14883.5	17124.0	2404.4		
10	17:00	48.00	42.50	35.81	42.85	4.50	-0.2999	1.0913	14597.6	16941.4	2353.4		
11	18:00	48.17	42.57	35.98	41.81	4.50	-0.0039	1.0967	14604.0	17198.3	2546.2		
12	19:00	48.25	35.87	41.96	42.96	4.50	-0.0699	1.1667	14040.0	17198.3	30066.5		
13	20:00	48.18	35.77	41.93	43.03	4.50	-0.1799	1.2982	14265.9	17432.4	3066.5		
14	21:00	48.18	35.77	41.93	41.25	4.50	-0.1800	1.2082	14200.0	17198.3	3225.2		
15	22:00	48.25	35.77	41.95	43.07	4.50	-0.0500	1.1233	42.00	0.0500	0.0733	14569.7	
16	23:00	48.25	35.77	41.98	43.11	4.50	0.0200	1.1371	42.50	0.0200	1.1111	14794.9	3348.1
17	00:00	48.25	35.77	42.81	43.16	4.50	0.4500	1.1509	42.50	0.6609	1.4332	17370.0	3368.1
18	01:00	48.25	35.77	42.81	43.20	4.50	0.5600	1.1636	42.50	0.6036	1.4301.4	18143.3	3862.3
19	02:00	48.30	35.77	42.04	43.24	4.50	0.6399	1.1742	42.71	0.6286	1.4286.4	18224.4	4001.6
20	03:00	48.33	35.77	42.10	43.28	4.50	0.7119	1.1848	42.82	0.6468	1.4182.7	18445.5	4173.6
21	04:00	48.36	35.82	42.11	43.30	4.50	0.8100	1.1962	42.92	0.6150	1.4284.8	18559.2	4234.6
22	05:00	48.39	35.82	42.11	43.32	4.50	0.9099	1.2076	43.02	0.6150	1.4284.8	18559.2	4234.6
23	06:00	48.39	35.82	42.11	43.32	4.50	0.9999	1.2123	43.00	0.9999	0.2976	14296.6	4359.3
24	07:00	48.42	36.91	42.14	43.36	4.50	1.0600	1.2239	43.14	1.0600	0.2339	14872.2	4504.2
25	08:00	48.42	36.91	42.15	43.38	4.50	1.1000	1.2358	43.25	1.1000	0.1558	13942.9	5114.8
26	09:00	48.40	36.96	42.16	43.41	4.50	1.2561	1.2561	43.25	1.0900	0.1651	14853.4	5067.3
27	10:00	48.40	36.96	42.16	43.42	4.50	1.2073	43.25	1.0700	1.0700	0.2003	14355.9	5210.5
28	11:00	48.45	36.95	42.19	43.45	4.50	1.2787	43.30	1.1100	0.1647	0.1647	14182.7	5313.6
29	12:00	48.45	36.95	42.19	43.46	4.50	1.3447	43.35	1.1500	0.1660	0.0004	14207.3	17679.4
30	13:00	48.45	36.95	42.20	43.48	4.50	1.2847	43.35	1.1400	0.1500	0.1500	14152.9	5414.3
31	14:00	48.39	35.04	42.21	43.50	4.50	1.2909	43.35	1.1400	0.1509	0.1435.6	19650.6	5515.0
1	15:00	48.42	36.91	42.21	43.51	4.50	1.2984	43.35	1.1300	0.1690	0.1411.0	19741.1	5620.4
2	16:00	48.42	36.91	42.21	43.51	4.50	1.3043	43.35	1.1000	0.1803	0.1483	14816.8	5728.6
3	17:00	48.42	36.91	42.21	43.51	4.50	1.3238	43.35	1.1000	0.1803	0.0562	14270.2	4137.2
4	18:00	48.42	36.91	42.21	43.51	4.50	1.3420	43.35	1.0900	0.1707	0.1449.3	18410.6	5101.3
5	19:00	48.45	36.99	42.21	43.51	4.50	1.3858	43.40	1.0459	0.0358	0.14228.1	17871.9	3653.8
6	20:00	48.45	36.99	42.21	43.51	4.50	1.40634	43.45	1.0600	0.0004	0.14207.3	17679.4	3412.1
7	21:00	48.45	36.99	42.21	43.51	4.50	1.40500	43.50	1.0500	0.0064	0.14275.7	16647.3	2367.5
8	22:00	48.45	36.99	42.21	43.51	4.50	1.42984	43.55	1.0699	0.0697	0.14204.0	14204.0	2417.9
9	00:00	48.45	36.99	42.21	43.51	4.50	1.43336	43.66	1.0800	-0.1128	0.14122.1	16611.8	2439.6
10	01:00	48.45	36.99	42.21	43.51	4.50	1.43757	43.75	1.1100	0.1142	0.14050.6	16530.5	2539.9
11	02:00	48.45	36.99	42.21	43.51	4.50	1.49078	43.71	1.0100	-0.1021	0.13968.8	16589.9	2601.1
12	03:00	48.45	36.99	42.21	43.51	4.50	1.49667	43.70	0.9400	-0.0232	0.13983.6	16559.8	2656.1
13	04:00	48.45	36.99	42.21	43.51	4.50	1.48849	43.70	0.8459	0.0349	0.13799.1	16519.2	2740.1
14	05:00	48.45	36.99	42.21	43.51	4.50	1.49532	43.50	0.8200	0.0545	0.13764.0	16514.9	2750.8
15	06:00	48.45	36.99	42.21	43.45	4.50	1.49421	43.58	0.7900	0.0812	0.13730.8	16479.3	2748.5
16	07:00	48.45	36.99	42.21	43.51	4.50	1.49307	43.51	0.7500	0.1114	0.13683.7	16545.9	2711.1
17	08:00	48.45	36.99	42.21	43.51	4.50	1.49199	43.75	0.7199	0.1362	0.13502.7	16418.9	2708.7
18	09:00	48.45	36.99	42.21	43.51	4.50	1.49078	43.71	0.7199	0.13699	0.13616.3	16383.1	2708.7
19	10:00	48.45	36.99	42.21	43.51	4.50	1.48967	43.67	0.7199	0.1854	0.13777.2	16286.9	2708.9
20	11:00	48.45	36.99	42.21	43.45	4.50	1.48785	43.70	0.6870	0.1512	0.13544.3	16344.3	2829.5

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C4N41 C-398C (11/15/71)

DAY	TIME	HWEU	JTEED	HWEU	CUMP	TWEU	CUMP	WUE	UBS	TWEU	089	BH	J	Q	DIFF	QUP	ODN	WDN	QL
5.	8.00	48.40	47.79	43.09	43.32	43.01	43.95	43.95	0.8600	-0.0211	13438.7	16403.0	-2964.2						
5.	9.00	48.38	35.79	43.11	43.14	43.11	43.92	43.92	0.8400	-0.0213	13379.3	16426.1	-3046.7						
5.	10.00	48.37	35.80	43.14	43.97	43.97	44.05	44.05	0.8600	-0.0224	13322.7	16477.1	-3125.6						
5.	11.00	48.37	35.80	43.16	43.97	43.97	44.05	44.05	0.8600	-0.0224	13294.0	16548.3	-3178.0						
5.	12.00	48.37	35.81	43.19	43.97	43.97	44.05	44.05	0.8600	-0.0227	13251.9	16647.2	-3178.0						
5.	13.00	48.38	35.81	43.19	44.02	43.22	44.06	44.06	0.8600	-0.0227	13251.9	16649.3	-3242.5						
5.	14.00	48.38	35.82	43.21	44.04	43.21	44.08	44.08	0.8700	-0.0313	13252.5	16649.5	-3248.3						
5.	15.00	48.38	35.82	43.21	44.04	43.21	44.09	44.09	0.8700	-0.0313	13252.9	16649.6	-3248.2						
5.	16.00	48.37	35.83	43.23	44.05	43.23	44.10	44.10	0.8700	-0.0610	13190.3	16700.5	-3327.0						
5.	17.00	48.37	35.83	43.24	44.13	43.24	44.10	44.10	0.8700	-0.0395	13088.7	16737.9	-4290.5						
5.	18.00	48.38	35.84	43.23	44.13	43.23	44.10	44.10	0.8700	-0.0301	13104.0	16739.4	-4265.8						
5.	19.00	48.38	35.85	43.23	44.12	43.23	44.10	44.10	0.8700	-0.0291	13104.7	167357.4	-4252.7						
5.	20.00	48.39	35.85	43.23	44.12	43.23	44.11	44.11	0.8700	-0.0291	13106.1	16736.5	-4191.1						
5.	21.00	48.39	35.85	43.24	44.12	43.24	44.10	44.10	0.8800	-0.0159	13109.5	16730.8	-4213.8						
5.	22.00	48.26	35.87	43.21	44.11	43.21	44.16	44.16	0.9400	-0.0448	13174.9	16718.3	-4377.4						
5.	23.00	48.25	35.86	43.21	44.11	43.21	44.14	44.14	0.9200	-0.0244	12923.8	16329.3	-4405.5						
5.	24.00	48.23	35.85	43.21	44.11	43.21	44.13	44.13	0.9100	-0.0136	12891.5	16340.3	-4448.8						
6.	1.00	48.22	35.85	43.21	44.10	43.21	44.11	44.11	0.9000	-0.0032	12891.8	16328.6	-4436.9						
6.	2.00	48.21	35.84	43.21	44.09	43.21	44.09	44.09	0.8799	-0.0174	12874.5	16339.6	-4465.0						
6.	3.00	48.19	35.83	43.20	44.09	43.20	44.08	44.08	0.8799	-0.0184	12878.1	16338.8	-4481.5						
6.	4.00	48.18	35.84	43.19	44.08	43.19	44.06	44.06	0.8700	-0.0286	12857.2	16326.2	-4468.9						
6.	5.00	48.16	35.83	43.19	44.08	43.19	44.05	44.05	0.8600	-0.0493	12846.3	16338.0	-4513.7						
6.	6.00	48.16	35.82	43.19	44.09	43.19	44.03	44.03	0.8400	-0.0600	12807.7	16349.0	-4541.3						
6.	7.00	48.14	35.81	43.17	44.07	43.17	44.02	44.02	0.8479	-0.0517	12821.3	16336.0	-4515.1						
6.	8.00	48.14	35.81	43.16	44.06	43.16	44.02	44.02	0.8600	-0.0422	12830.3	16324.6	-4488.6						
6.	9.00	48.14	35.80	43.14	44.04	43.14	44.01	44.01	0.8700	-0.0340	12867.1	16312.3	-4434.3						
6.	10.00	48.14	35.80	43.14	44.03	43.14	44.00	44.00	0.8900	-0.0356	12878.1	16312.5	-4434.3						
6.	11.00	48.15	35.79	43.11	44.00	43.11	44.00	44.00	0.8993	-0.0493	12829.9	16299.0	-4996.0						
6.	12.00	48.16	35.78	43.10	44.09	43.10	44.00	44.00	0.9000	-0.0223	12859.5	16289.1	-5229.5						
6.	13.00	48.21	35.77	43.10	44.09	43.10	44.02	44.02	0.9799	-0.0824	11832.4	16230.4	-5398.0						
6.	14.00	48.21	35.77	42.98	42.87	42.98	42.86	42.86	1.1200	-0.2337	11600.3	16179.6	-5559.3						
6.	15.00	48.24	35.76	42.92	43.82	42.92	43.82	43.82	1.1399	-0.2399	11701.2	16100.5	-5399.3						
6.	16.00	48.21	35.75	42.86	43.76	42.86	43.75	43.75	0.8900	-0.0479	11737.4	16041.2	-5303.7						
6.	17.00	48.20	35.75	42.80	43.70	42.80	43.75	43.75	0.9500	-0.0490	11545.3	16049.6	-5424.2						
6.	18.00	48.20	35.73	42.75	43.65	42.75	43.70	43.70	0.8200	-0.0871	11281.0	16022.8	-4838.8						
6.	19.00	48.20	35.72	42.68	43.60	42.68	43.65	43.65	0.8400	-0.0871	11411.0	16049.8	-5438.8						
6.	20.00	48.22	35.72	42.61	43.51	42.61	43.65	43.65	0.8400	-0.0671	11457.3	16052.3	-5307.9						
6.	21.00	48.22	35.72	42.55	43.45	42.55	43.60	43.60	0.8400	-0.0529	11501.6	16070.8	-5203.0						
6.	22.00	48.24	35.71	42.48	43.39	42.48	43.50	43.50	0.1199	-0.0920	11550.1	16161.9	-5060.4						
6.	23.00	48.19	48.19	42.41	43.32	42.41	43.24	43.24	0.8300	-0.0870	11516.3	161572.0	-4995.6						
6.	24.00	48.20	48.18	42.35	43.27	42.35	43.19	43.19	0.8400	-0.0817	11582.4	161537.6	-4955.2						
6.	25.00	48.21	48.18	42.27	43.20	42.27	43.13	43.13	0.8500	-0.0767	11600.3	161489.9	-4839.6						
6.	26.00	48.21	48.17	42.25	43.15	42.25	43.08	43.08	0.8600	-0.0715	11618.3	161459.5	-4836.2						
6.	27.00	48.20	48.16	42.20	43.05	42.20	43.02	43.02	0.8600	-0.0763	11621.2	161419.7	-4795.6						
6.	28.00	48.20	48.15	42.16	43.04	42.16	42.97	42.97	0.8700	-0.0711	11630.0	161385.3	-4754.8						
6.	29.00	48.20	48.14	42.14	43.02	42.14	42.91	42.91	0.8700	-0.0760	11634.5	161369.5	-4709.1						
6.	30.00	48.21	48.13	42.11	43.00	42.11	42.86	42.86	0.8700	-0.0708	11635.4	161311.9	-4660.1						
6.	31.00	48.21	48.12	42.08	42.98	42.08	42.83	42.83	0.8900	-0.0269	11718.6	16216.8	-4948.1						

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CANAL C-38DC DATE 12/13/63

DAY	TIME	HHRD	J T W E D	HWEW	COMP TWEU	OBS UN	OBS TIME	OBS DIFF	GDN	QUP
7.	10:00	47.77	35.63	41.77	42.72	42.75	0.9800	-0.0279	16118.8	5035.4
7.	10:00	47.80	35.63	41.66	42.62	42.68	0.9400	-0.0279	16118.8	5035.4
7.	10:00	47.76	35.62	41.56	42.52	42.60	1.0600	-0.0178	11279.6	5031.6
7.	11:00	47.70	35.28	42.45	42.41	42.53	1.0999	-0.1312	10826.1	5031.2
7.	12:00	47.65	35.24	41.35	42.32	42.35	1.1500	-0.1745	11017.3	4776.8
7.	13:00	47.59	35.21	41.24	42.22	42.38	1.1500	-0.1693	11063.3	4629.5
7.	14:00	47.53	35.16	41.14	42.15	42.38	1.1399	-0.1263	12900.0	15616.2
7.	15:00	47.47	35.12	41.03	42.01	42.25	1.1200	-0.2372	10416.8	5110.4
7.	16:00	47.42	35.08	40.93	41.07	42.20	0.8230	0.0030	10034.9	39311.8
7.	17:00	47.37	34.79	40.76	41.44	41.60	0.8600	-0.1526	8778.6	3176.9
7.	18:00	47.32	34.41	40.67	41.25	41.47	0.8800	-0.0455	12300.3	3964.2
7.	19:00	47.26	34.33	40.58	41.31	41.59	0.7349	-0.0550	8912.0	3878.0
7.	20:00	47.21	34.25	40.49	41.23	41.44	0.7100	-0.0455	8987.7	37192.8
7.	21:00	47.16	34.19	40.43	40.97	41.22	0.7300	-0.1270	8355.7	12269.9
7.	22:00	47.11	34.15	40.37	40.97	41.10	0.7300	-0.1270	8355.7	12269.9
7.	23:00	47.06	33.91	40.28	40.88	41.02	0.6159	-0.1301	8401.3	2852.0
7.	24:00	47.01	33.86	40.20	40.81	40.94	0.6220	-0.1240	8439.9	11237.2
8.	1:00	46.97	33.82	40.12	40.74	40.86	0.6222	-0.1187	8478.8	11211.4
8.	2:00	46.92	33.78	40.04	40.67	40.75	0.6282	-0.1163	8516.4	11040.4
8.	3:00	46.87	33.74	39.96	40.59	40.71	0.6336	-0.1163	8554.8	11079.1
8.	4:00	46.82	33.77	39.88	40.51	40.63	0.6401	-0.1198	8641.4	2649.0
8.	5:00	46.77	33.60	39.79	40.43	40.55	0.6474	-0.1159	8641.4	2505.2
8.	6:00	46.72	33.55	39.74	40.36	40.48	0.6529	-0.1599	8779.1	11120.6
8.	7:00	46.67	33.49	39.62	40.28	40.40	0.6594	-0.1700	8716.1	11105.4
8.	8:00	46.73	33.34	39.55	40.14	40.32	0.6622	-0.1700	8733.4	10376.9
8.	9:00	46.70	33.45	39.46	40.05	40.25	0.6589	-0.1530	8821.8	10247.1
8.	10:00	46.67	33.50	39.46	40.05	40.23	0.6582	-0.1606	8829.5	10172.6
8.	11:00	46.64	33.57	39.46	40.01	40.17	0.6577	-0.1922	8832.0	10088.7
8.	12:00	46.61	33.55	39.46	40.01	40.19	0.6590	-0.2105	8831.4	10071.1
8.	13:00	46.58	33.51	39.32	39.94	40.17	0.6581	-0.2278	8801.1	10053.9
8.	14:00	46.55	33.51	39.32	39.90	40.11	0.6583	-0.2299	8846.8	10363.6
8.	15:00	46.52	33.46	39.29	39.87	40.13	0.6587	-0.2299	8846.8	10363.6
8.	16:00	46.50	33.44	39.21	39.83	40.11	0.6589	-0.2200	8850.2	10027.9
8.	17:00	46.47	33.43	39.17	39.79	40.08	0.6589	-0.2200	8850.2	10027.9
8.	18:00	46.45	33.41	39.14	39.73	40.05	0.6590	-0.2200	8860.5	10001.7
8.	19:00	46.43	33.39	39.10	39.69	40.04	0.6593	-0.2200	8870.4	10949.4
8.	20:00	46.41	33.37	39.07	39.66	40.01	0.6595	-0.2109	8880.7	10548.8
8.	21:00	46.39	33.35	39.03	39.62	39.95	0.6597	-0.2109	8882.4	10027.0
8.	22:00	46.36	33.33	39.00	39.56	39.92	0.6561	-0.2125	8889.8	10027.0
8.	23:00	46.34	33.30	38.99	39.55	39.88	0.6564	-0.3006	8890.0	9536.1
8.	24:00	46.32	33.29	38.99	39.55	39.86	0.6566	-0.3006	8890.0	9536.1
9.	1:00	46.30	33.28	38.98	39.54	39.83	0.6565	-0.3019	8897.2	9552.9
9.	2:00	46.28	33.28	38.98	39.54	39.83	0.6565	-0.3019	8897.2	9552.9
9.	3:00	46.25	33.26	38.98	39.54	39.83	0.6565	-0.3019	8897.2	9552.9
9.	4:00	46.23	33.27	38.98	39.53	39.83	0.6565	-0.3019	8897.2	9552.9
9.	5:00	46.21	33.27	38.98	39.53	39.83	0.6565	-0.3019	8897.2	9552.9
9.	6:00	46.19	33.27	38.98	39.52	39.83	0.6565	-0.3019	8897.2	9552.9
9.	7:00	46.17	33.27	38.98	39.52	39.83	0.6563	-0.3019	8897.2	9552.9
9.	8:00	46.17	33.27	38.98	39.52	39.83	0.6563	-0.3019	8897.2	9552.9

CANAL C-380C

DAY	TIME	AMBD	JHWED	CMPD	TMEU	OBGS	THW	bAG	bH	QUP	QDN	QL
9	8:00	47.15	33.00	38.96	39.52	0.6269	39.62	0.6599	-0.0923	9809.6	9568.4	753.3
9	9:00	47.13	33.04	38.95	39.51	0.5676	39.61	0.6579	-0.0915	8803.4	9517.0	773.5
9	10:00	47.12	33.23	38.95	39.51	0.5684	39.61	0.6559	-0.0915	8802.5	9535.5	513.5
9	11:00	47.10	33.22	38.95	39.50	0.5504	39.60	0.6530	-0.0916	8784.5	9420.1	163.4
9	12:00	47.09	33.21	38.96	39.50	0.5509	39.60	0.6100	-0.0463	9828.2	9444.7	163.4
9	13:00	47.08	33.20	38.94	39.55	0.5636	39.60	0.6239	-0.0169	9455.0	9385.0	529.9
9	14:00	46.99	33.27	39.02	39.63	0.6130	39.65	0.6500	-0.0350	9433.8	9396.2	522.3
9	15:00	46.87	33.22	38.99	39.00	0.6149	39.65	0.6700	-0.0533	9439.6	9396.0	556.4
9	16:00	46.84	33.22	38.99	39.00	0.6166	39.66	0.6899	-0.1911	9444.8	9455.6	481.9
9	17:00	46.83	33.21	38.98	39.58	0.6088	39.68	0.6900	-0.0801	9444.3	9411.5	501.5
9	18:00	46.79	33.19	38.96	39.57	0.6098	39.66	0.6899	-0.0794	9387.5	9314.5	511.2
9	19:00	46.75	33.18	38.96	39.57	0.6105	39.65	0.6939	-0.0837	9379.5	9314.7	522.6
9	20:00	46.73	33.17	38.95	39.56	0.6112	39.65	0.6900	-0.0748	9384.5	9306.1	522.6
9	21:00	46.70	33.17	38.94	39.25	0.6111	39.63	0.7000	-0.0880	9377.4	9306.7	522.6
9	22:00	46.68	33.16	38.94	39.00	0.6114	39.63	0.6900	-0.0926	9376.8	9306.9	1380.0
9	23:00	46.65	33.15	38.92	39.12	0.6003	39.62	0.6989	-0.1922	8858.8	8779.8	181.5
10	0:00	46.66	33.12	38.92	39.41	0.6907	39.61	0.6899	-0.1878	8556.9	8902.2	205.2
10	1:00	46.67	33.10	38.93	39.42	0.6921	39.61	0.6800	-0.1653	8586.1	8824.4	228.2
10	2:00	46.68	33.08	38.94	39.43	0.6934	39.60	0.6600	-0.1559	8595.7	8839.4	241.5
10	3:00	46.69	33.07	38.95	39.44	0.6940	39.60	0.6500	-0.1253	8589.5	8816.3	271.8
10	4:00	46.70	33.06	38.96	39.46	0.6946	39.59	0.6200	-0.0914	8588.7	8831.4	296.6
10	5:00	46.71	33.04	38.98	39.47	0.6959	39.59	0.6099	-0.0936	8585.4	8827.6	345.9
10	6:00	46.72	33.03	38.99	39.48	0.6965	39.58	0.5900	-0.0722	8581.0	8947.1	360.0
10	7:00	46.73	33.01	39.01	39.50	0.6977	39.58	0.5699	-0.0610	8587.0	8930.4	22.7
10	8:00	46.75	33.00	39.02	39.51	0.6989	39.58	0.5600	-0.0481	8709.7	8709.3	8719.8
10	9:00	46.78	33.02	39.03	39.53	0.5018	39.62	0.5699	0.0035	8825.5	8709.3	8719.8
10	10:00	46.73	33.05	39.05	39.62	0.5135	39.62	0.5699	-0.1140	8877.6	9685.1	956.6
10	11:00	46.70	33.06	38.96	39.66	0.5176	39.66	0.4943	-0.0483	8805.0	8877.3	884.0
10	12:00	46.68	33.04	38.96	39.66	0.5176	39.66	0.4599	-0.0912	8858.7	8831.4	1380.0
10	13:00	46.65	33.03	38.97	39.67	0.5176	39.75	0.4599	-0.1417	8856.5	9644.7	787.3
10	14:00	46.73	33.01	38.98	39.68	0.5182	39.75	0.4899	-0.1235	8839.7	9626.5	768.8
10	15:00	46.75	33.01	38.98	39.68	0.5185	39.73	0.4899	-0.1139	8819.7	9644.5	833.7
10	16:00	46.70	33.12	39.04	39.60	0.5680	39.72	0.6800	-0.1024	8709.7	9703.0	825.4
10	17:00	46.68	33.10	39.04	39.60	0.5675	39.71	0.6699	-0.1141	8488.2	9468.2	979.0
10	18:00	46.68	33.07	39.04	39.61	0.5438	39.70	0.6599	-0.1140	8495.3	9452.0	956.6
10	19:00	46.68	33.04	39.06	39.61	0.5441	39.66	0.6600	-0.1138	8501.3	9436.0	934.7
10	20:00	46.68	33.10	38.99	39.60	0.5441	39.66	0.6699	-0.1236	8511.5	9419.8	906.2
10	21:00	46.45	33.10	38.96	39.52	0.5463	39.63	0.6700	-0.1235	8511.5	9403.8	884.4
10	22:00	46.45	33.10	38.94	39.50	0.5464	39.62	0.6800	-0.1333	8531.6	8587.4	855.7
10	23:00	46.44	33.10	38.94	39.48	0.5466	39.62	0.6899	-0.1322	8537.6	9371.4	833.7
10	0:00	46.43	33.10	38.92	39.46	0.5467	39.61	0.6800	-0.1322	8537.6	9363.0	825.4
10	1:00	46.43	33.10	38.91	39.45	0.5467	39.59	0.6899	-0.1430	8549.1	9346.9	797.1
10	2:00	46.42	33.10	38.87	39.41	0.5467	39.58	0.6899	-0.1429	8555.7	9330.5	714.7
10	3:00	46.42	33.10	38.85	39.39	0.5457	39.55	0.6999	-0.1542	8463.7	9314.3	850.3
10	4:00	46.41	33.10	38.83	39.37	0.5457	39.53	0.6999	-0.1541	8469.7	9297.8	628.0
10	5:00	46.41	33.10	38.81	39.35	0.5459	39.51	0.7000	-0.1540	8475.6	9281.0	605.9
10	6:00	46.40	33.07	38.80	39.24	0.4499	39.50	0.7000	-0.2500	7903.6	8347.8	444.1
10	7:00	46.40	33.05	38.80	39.25	0.4512	39.53	0.7297	-0.2578	7902.8	8362.0	459.2

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FINAL C-380C

DAY	TIME	HWD	LTD	COMP	TUE	COMP DH	QUP	QDN	QUL
11.	8:00	46.-40	33.-04	38.-80	39.-25	39.-57	0.-3180	8669.-2	467.-0
11.	8:40	46.-40	33.-04	38.-80	39.-25	0.-7700	-0.-3481	8658.-9	466.-4
11.	9:20	46.-40	33.-04	38.-80	39.-25	0.-8000	-0.-3800	8647.-5	465.-4
11.	10:00	46.-40	33.-05	38.-81	39.-26	0.-5110	-0.-3960	8638.-8	464.-4
11.	11:00	46.-40	33.-06	38.-81	39.-26	0.-4504	-0.-4095	8629.-5	463.-0
11.	12:00	46.-40	33.-07	38.-81	39.-25	0.-4498	-0.-4095	8620.-0	462.-0
11.	13:00	46.-40	33.-07	38.-81	39.-25	0.-4498	-0.-4090	8611.-4	461.-4
11.	14:00	46.-41	33.-08	38.-81	39.-25	0.-4492	-0.-4090	8602.-1	460.-0
11.	15:00	46.-41	33.-09	38.-82	39.-26	0.-4484	-0.-4090	8592.-5	459.-4
11.	16:00	46.-41	33.-10	38.-82	39.-26	0.-4477	-0.-4090	8582.-2	458.-4
11.	17:00	46.-41	33.-11	38.-82	39.-26	0.-4477	-0.-4090	8572.-2	457.-9
11.	18:00	46.-41	33.-11	38.-82	39.-26	0.-4471	-0.-4090	8562.-0	456.-1
11.	19:00	46.-41	33.-12	38.-82	39.-26	0.-4464	-0.-4090	8551.-8	455.-9
11.	20:00	46.-42	33.-12	38.-83	39.-27	0.-4464	-0.-4090	8541.-1	455.-9
11.	21:00	46.-41	33.-13	38.-83	39.-27	0.-4456	-0.-4090	8531.-0	454.-7
11.	22:00	46.-40	33.-14	38.-83	39.-27	0.-4449	-0.-4090	8521.-7	454.-7
11.	23:00	46.-40	33.-15	38.-83	39.-27	0.-4441	-0.-4090	8511.-6	454.-7
11.	24:00	46.-40	33.-16	38.-84	39.-28	0.-4408	-0.-4090	8501.-5	454.-7
12.	1:00	46.-41	33.-16	38.-84	39.-28	0.-4408	-0.-4090	8491.-4	454.-7
12.	2:00	46.-42	33.-17	38.-84	39.-28	0.-4403	-0.-4090	8481.-4	454.-7
12.	3:00	46.-42	33.-18	38.-84	39.-27	0.-3959	-0.-4090	8471.-7	454.-7
12.	4:00	46.-42	33.-19	38.-85	39.-28	0.-3889	-0.-4090	8461.-7	454.-7
12.	5:00	46.-44	33.-19	38.-85	39.-28	0.-4390	-0.-6500	8451.-0	454.-7
12.	6:00	46.-45	33.-20	38.-85	39.-28	0.-4384	-0.-6500	8441.-7	454.-7
12.	7:00	46.-44	33.-21	38.-85	39.-28	0.-4377	-0.-6500	8431.-7	454.-7
12.	8:00	46.-44	33.-21	38.-85	39.-28	0.-4376	-0.-6500	8421.-7	454.-7
12.	9:00	46.-44	33.-19	38.-85	39.-29	0.-4388	-0.-6500	8411.-7	454.-7
12.	10:00	46.-44	33.-18	38.-86	39.-29	0.-3959	-0.-6500	8401.-7	454.-7
12.	11:00	46.-44	33.-19	38.-86	39.-30	0.-4402	-0.-6500	8391.-7	454.-7
12.	12:00	46.-44	33.-16	38.-86	39.-30	0.-4400	-0.-6500	8381.-7	454.-7
12.	13:00	46.-44	33.-15	38.-87	39.-31	0.-4414	-0.-6500	8371.-7	454.-7
12.	14:00	46.-44	33.-13	38.-87	39.-31	0.-4428	-0.-6500	8361.-7	454.-7
12.	15:00	46.-44	33.-12	38.-87	39.-31	0.-4434	-0.-6500	8351.-7	454.-7
12.	16:00	46.-44	33.-11	38.-87	39.-31	0.-4441	-0.-6500	8341.-7	454.-7
12.	17:00	46.-44	33.-11	38.-87	39.-32	0.-6429	-0.-6500	8331.-7	454.-7
12.	18:00	46.-44	33.-10	38.-87	39.-32	0.-6438	-0.-6500	8321.-7	454.-7
12.	19:00	46.-44	33.-09	38.-87	39.-32	0.-6456	-0.-6500	8311.-7	454.-7
12.	20:00	46.-44	33.-08	38.-89	39.-32	0.-6455	-0.-6500	8301.-7	454.-7
12.	21:00	46.-43	33.-08	38.-89	39.-32	0.-6455	-0.-6500	8291.-7	454.-7
12.	22:00	46.-43	33.-08	38.-90	39.-32	0.-6454	-0.-6500	8281.-7	454.-7
12.	23:00	46.-43	33.-08	38.-90	39.-32	0.-6454	-0.-6500	8271.-7	454.-7
12.	24:00	46.-43	33.-09	38.-91	39.-32	0.-6444	-0.-6500	8261.-7	454.-7
13.	1:00	46.-42	33.-09	38.-91	39.-32	0.-6443	-0.-6500	8251.-7	454.-7
13.	2:00	46.-42	33.-09	38.-92	39.-32	0.-6442	-0.-6500	8241.-7	454.-7
13.	3:00	46.-42	33.-09	38.-92	39.-32	0.-6442	-0.-6500	8231.-7	454.-7
13.	4:00	46.-41	33.-09	38.-93	39.-57	0.-6431	-0.-5700	8221.-7	454.-7
13.	5:00	46.-41	33.-10	38.-93	39.-57	0.-6431	-0.-5700	8211.-7	454.-7
13.	6:00	46.-41	33.-10	38.-94	39.-58	0.-6430	-0.-5600	8201.-7	454.-7
13.	7:00	46.-41	33.-10	38.-94	39.-58	0.-6430	-0.-5600	8191.-7	454.-7

CANAL C-3-HDC

DAY	TIME	HHR/EU	THED	COMP TWL		OBS DM	ODD	QUP	QI		
				HHRD	TWL						
					OBS	TWE					
13.	8.00	46.41	33.10	28.95	39.35	0.4077	29.50	0.5500	-0.1622	7429.3	
13.	9.00	46.42	33.08	38.36	39.37	0.4053	39.50	0.5300	-0.1211	7422.8	
13.	10.00	46.44	33.05	38.19	39.39	0.4039	39.50	0.5100	-0.1000	7422.2	
13.	11.00	46.35	33.05	39.01	39.42	0.4104	39.50	0.4900	-0.0195	7422.4	
13.	12.00	46.48	33.03	39.03	39.44	0.4115	39.50	0.4700	-0.0700	7424.2	
13.	13.00	46.50	33.01	39.05	39.46	0.4162	39.50	0.4500	-0.0337	7425.4	
13.	14.00	46.49	33.03	39.07	39.48	0.4148	39.50	0.4300	-0.0151	7425.3	
13.	15.00	46.48	33.06	39.10	39.53	0.4180	39.50	0.4000	0.0380	7428.5	
13.	16.00	46.47	33.08	39.09	39.52	0.4289	39.50	0.4100	0.0269	7429.1	
13.	17.00	46.46	33.12	39.09	39.52	0.4345	39.50	0.4100	0.0245	7429.2	
13.	18.00	46.45	33.11	39.08	39.51	0.4351	39.50	0.4200	0.0151	7422.7	
13.	19.00	46.45	33.11	39.08	39.51	0.4351	39.50	0.4200	0.0151	7422.4	
13.	20.00	46.45	33.11	39.08	39.51	0.4351	39.50	0.4200	0.0151	7422.2	
13.	21.00	46.45	33.10	39.07	39.50	0.4351	39.50	0.4300	0.0051	7421.8	
13.	22.00	46.45	33.10	39.07	39.50	0.4351	39.51	0.4399	-0.0041	7421.7	
13.	23.00	46.44	33.10	39.07	39.50	0.4351	39.52	0.4499	-0.0164	7361.5	
13.	24.00	46.44	33.10	39.08	39.49	0.4351	39.52	0.4600	-0.0262	7361.1	
14.	1.00	46.44	33.09	39.06	39.49	0.4365	39.52	0.4600	-0.0336	7350.5	
14.	2.00	46.44	33.09	39.06	39.49	0.4365	39.53	0.4699	-0.0336	7350.6	
14.	3.00	46.44	33.09	39.05	39.48	0.4364	39.53	0.4799	-0.0336	7352.5	
14.	4.00	46.43	33.09	39.05	39.48	0.4364	39.53	0.4799	-0.0336	7352.6	
14.	5.00	46.43	33.08	39.05	39.48	0.4369	39.54	0.4899	-0.0336	7352.4	
14.	6.00	46.43	33.08	39.04	39.47	0.4370	39.54	0.5000	-0.0629	7351.0	
14.	7.00	46.43	33.08	39.04	39.47	0.4369	39.54	0.5000	-0.0630	7351.1	
14.	8.00	46.43	33.07	39.07	39.44	0.4384	39.54	0.5099	-0.0105	7351.5	
14.	9.00	46.43	33.06	39.04	39.44	0.4089	39.54	0.5000	-0.0910	7351.2	
14.	10.00	46.43	33.06	39.04	39.44	0.4091	39.54	0.5000	-0.0908	7350.7	
14.	11.00	46.43	33.06	39.03	39.44	0.4091	39.53	0.5000	-0.0908	7350.2	
14.	12.00	46.45	33.06	39.03	39.43	0.4092	39.52	0.4900	-0.0807	7351.9	
14.	13.00	46.45	33.06	39.03	39.43	0.4092	39.52	0.4900	-0.0807	7352.0	
14.	14.00	46.46	33.05	39.03	39.43	0.4098	39.51	0.4800	-0.0701	7351.8	
14.	15.00	46.46	33.05	39.03	39.43	0.4098	39.51	0.4800	-0.0800	7351.5	
14.	16.00	46.47	33.05	39.03	39.43	0.4099	39.50	0.4700	-0.0599	7351.2	
14.	17.00	46.47	33.05	39.03	39.43	0.4106	39.50	0.4700	-0.0599	7351.7	
14.	18.00	46.47	33.05	39.03	39.43	0.4106	39.50	0.4700	-0.0599	7351.4	
14.	19.00	46.47	33.05	39.03	39.43	0.4106	39.50	0.4700	-0.0599	7351.1	
14.	20.00	46.47	33.04	39.02	39.43	0.4106	39.50	0.4700	-0.0599	7350.8	
14.	21.00	46.47	33.04	39.02	39.43	0.4106	39.51	0.4900	-0.0973	7350.5	
14.	22.00	46.47	33.04	39.02	39.43	0.4108	39.51	0.4900	-0.0983	7350.2	
14.	23.00	46.47	33.04	39.02	39.43	0.4106	39.52	0.5000	-0.0893	7350.7	
14.	24.00	46.47	33.04	39.02	39.43	0.4106	39.52	0.5000	-0.0893	7350.4	
15.	1.00	46.47	33.04	39.02	39.43	0.4106	39.52	0.5000	-0.0893	7350.1	
15.	2.00	46.47	33.04	39.02	39.43	0.4106	39.52	0.5000	-0.0893	7350.8	
15.	3.00	46.47	33.03	39.02	39.43	0.4112	39.52	0.5099	-0.0987	7351.5	
15.	4.00	46.47	33.03	39.02	39.43	0.4112	39.52	0.5099	-0.0987	7351.2	
15.	5.00	46.47	33.03	39.02	39.43	0.4112	39.52	0.5200	-0.1087	7351.9	
15.	6.00	46.47	33.03	39.02	39.43	0.4112	39.54	0.5200	-0.1186	7351.6	
15.	7.00	46.47	33.03	39.02	39.43	0.4113	39.54	0.5200	-0.1286	7352.3	
15.	8.00	46.47	33.03	39.02	39.43	0.4113	39.55	0.5299	-0.1341	7352.0	
15.	9.00	46.45	33.02	39.01	39.42	0.4118	39.54	0.5200	-0.1181	7351.7	
15.	10.00	46.45	33.02	39.01	39.42	0.4118	39.54	0.5199	-0.1081	7351.4	
15.	11.00	46.45	33.01	39.01	39.42	0.4123	39.53	0.5199	-0.1076	7351.1	
15.	12.00	46.44	33.01	39.01	39.42	0.4123	39.52	0.5099	-0.0976	7350.8	
15.	13.00	46.44	33.01	39.01	39.42	0.4123	39.52	0.5099	-0.0976	7350.5	

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CANAL C-38C B

DAY	TIME	HHRD.	THED	COMP	TWEW	OBS	TWEW	OBS	QUP	QDN	QL
0.1	8.00	52.24	39.08	45.51	46.30	46.12	46.09	46.07	4.8777	4.974.1	1164.6
	8.40	52.23	39.08	45.51	46.30	46.12	46.09	46.07	0.1716	3.815.5	4.973.6
1.	10.00	52.2	39.09	45.50	46.30	46.12	46.09	46.07	0.1514	4.973.1	1155.5
1.	11.00	52.25	39.09	45.50	46.30	46.15	46.12	46.09	0.1459	4.972.6	1150.7
1.	12.00	52.25	39.08	45.50	46.27	46.16	46.15	46.1	0.1172	3.882.8	4.872.5
1.	13.00	52.26	39.08	45.53	46.30	46.16	46.15	46.1	0.1369	3.897.0	4.892.1
1.	14.00	52.28	39.08	45.57	46.34	46.19	46.16	46.1	0.1349	3.897.5	4.874.0
1.	15.00	52.28	39.08	45.60	46.38	46.20	46.19	46.1	0.1515	3.818.5	4.893.3
1.	16.00	52.29	39.08	45.64	46.40	46.20	46.19	46.1	0.1686	3.812.9	4.910.8
1.	17.00	52.31	39.11	45.66	46.45	46.21	46.20	46.1	0.1639	4.915.6	4.926.0
1.	18.00	52.45	39.11	45.69	46.47	47.04	46.45	46.4	0.2314	3.804.0	4.937.2
1.	19.00	52.44	39.23	45.70	46.47	47.05	46.45	46.4	0.2059	4.617.9	4.913.4
1.	20.00	52.42	39.31	45.72	46.58	46.63	46.56	46.5	0.0263	4.667.9	4.894.5
1.	21.00	52.42	39.33	45.80	46.66	46.67	46.63	46.6	0.0263	5.212.9	5.205.3
1.	22.00	52.44	39.41	45.90	46.84	46.62	46.62	46.6	0.0476	4.826.1	5.297.4
1.	23.00	52.44	39.40	45.95	46.89	46.65	46.65	46.6	0.1639	4.734.5	5.711.9
1.	24.00	52.44	39.44	45.95	47.03	46.84	46.66	46.6	0.6939	4.734.5	5.718.2
1.	25.00	52.45	39.43	45.98	47.01	47.03	46.84	46.6	0.3431	4.653.6	6.144.8
1.	26.00	52.48	39.43	45.98	47.00	47.03	46.86	46.6	0.3431	4.653.6	6.144.8
1.	27.00	52.48	39.42	45.98	47.00	47.05	46.69	46.6	0.7799	4.722.1	5.287.9
1.	28.00	52.50	39.41	45.98	46.98	47.05	46.70	46.7	0.7599	4.728.51	5.222.1
1.	29.00	52.51	39.40	45.98	46.98	47.11	46.71	46.7	0.2487	4.722.1	5.132.3
2.	4.00	52.51	39.40	45.98	46.98	47.11	46.71	46.7	0.2487	4.713.7	5.130.9
2.	5.00	52.53	39.39	45.95	46.95	47.11	46.75	46.7	0.2199	4.714.8	6.116.3
2.	6.00	52.54	39.37	45.98	46.93	47.13	46.75	46.7	0.8639	4.714.8	6.117.4
2.	7.00	52.56	39.36	45.96	46.94	47.13	46.78	46.7	0.9039	4.717.3	6.122.1
2.	8.00	52.54	39.44	45.95	46.95	47.13	46.78	46.7	0.9299	4.717.3	6.117.6
2.	9.00	52.55	39.41	45.91	45.83	47.11	46.79	46.7	0.9639	4.717.9	6.135.9
2.	10.00	52.53	39.38	45.82	46.82	47.11	47.11	47.1	0.3042	5.245.1	6.139.7
2.	11.00	52.51	39.36	45.81	46.81	47.22	46.81	46.8	0.2785	5.242.7	6.180.7
2.	12.00	52.51	39.34	45.81	46.81	47.10	47.05	47.1	0.1039	4.727.5	6.162.1
2.	13.00	52.50	39.29	45.79	47.09	47.09	47.05	47.1	0.0267	5.263.3	6.166.1
2.	14.00	52.50	39.28	45.78	47.09	47.09	47.05	47.1	0.1861	4.759.9	6.162.1
2.	15.00	52.50	39.27	45.77	47.09	47.09	47.05	47.1	0.1731	5.336.3	6.171.6
2.	16.00	52.48	39.26	45.76	47.07	47.09	47.05	47.1	0.3525	5.243.7	6.187.9
2.	17.00	52.48	39.25	45.76	47.07	47.09	47.05	47.1	0.1779	5.241.0	6.189.7
2.	18.00	52.48	39.24	45.75	47.07	47.09	46.91	46.9	0.1339	5.249.3	6.143.9
2.	19.00	52.51	39.24	45.82	46.88	47.11	46.79	46.8	0.1789	5.245.3	6.187.0.5
2.	20.00	52.55	39.24	45.82	46.88	47.11	46.79	46.8	0.1930	6.626.3	8.870.7
2.	21.00	52.56	40.27	45.82	46.88	47.20	46.79	46.8	1.2279	7.476.6	8.899.2
2.	22.00	52.57	40.27	45.82	46.88	47.20	46.79	46.8	1.3027	6.623.3	8.899.0
2.	23.00	52.57	40.27	45.82	46.88	47.20	46.79	46.8	1.3027	6.623.3	8.899.0
2.	24.00	52.55	40.27	45.82	46.88	47.20	46.79	46.8	1.3027	6.623.3	8.899.0
2.	25.00	52.54	40.27	45.82	46.88	47.20	46.79	46.8	1.3027	6.623.3	8.899.0
2.	26.00	52.54	40.27	45.82	46.88	47.20	46.79	46.8	1.3027	6.623.3	8.899.0
2.	27.00	52.54	40.27	45.82	46.88	47.20	46.79	46.8	1.3027	6.623.3	8.899.0
2.	28.00	52.54	40.27	45.82	46.88	47.20	46.79	46.8	1.3027	6.623.3	8.899.0
3.	2.00	53.31	41.74	46.89	46.95	50.77	50.95	51.01	3.999.9	4.829.9	5.238.7
3.	3.00	53.31	41.89	46.95	47.09	50.90	3.815.9	51.01	-0.1140	1.037.3	1.577.5
3.	4.00	53.32	42.00	47.09	47.13	50.90	3.815.9	51.01	-0.0224	1.036.1	1.542.1
3.	5.00	53.32	42.12	47.25	51.06	3.817.5	51.09	51.16	1.757.9	1.581.2	1.541.4
3.	6.00	53.32	42.33	47.44	51.16	3.767.3	51.16	51.20	3.815.8	1.571.9	1.505.1
3.	7.00	54.12	42.37	47.34	51.07	3.734.0	51.20	51.20	3.815.8	1.555.8	1.455.8

CANAL C-3461H

DAY	TIME	WIND DIRECTION	WIND SPEED	CUMPS	TIDE	OBS DHI	QUP	QUD
13.00	8.00	42°	42.42	47.30	51.01	51.28	3.9799	-0.2895
		44°	46.65	47.35	51.05	51.34	3.8899	-0.1772
3.	10.00	54.63	42.36	47.40	50.64	51.40	4.0000	-0.7504
4.	11.00	54.63	43.13	47.70	50.95	51.40	3.6999	-0.4446
2.	12.00	54.62	42.51	47.90	51.18	51.40	3.3000	-0.2174
3.	13.00	54.68	42.60	47.90	51.18	51.41	3.2823	-0.2174
3.	14.00	54.68	42.68	47.95	51.21	51.41	3.2660	-0.2174
3.	15.00	54.95	42.79	47.95	51.21	51.41	3.2127	-0.2174
3.	16.00	55.01	42.86	47.90	51.08	51.44	3.1886	-0.2812
3.	17.00	55.10	42.84	48.05	51.28	51.44	3.2325	-0.1514
3.	18.00	55.16	42.85	48.20	51.52	51.44	3.2320	-0.1514
3.	19.00	55.20	43.16	48.29	51.45	51.45	3.2954	-0.0804
3.	20.00	55.20	43.24	48.16	48.15	51.54	3.2954	-0.0804
3.	21.00	55.32	43.07	48.13	51.34	51.45	3.1933	-0.1939
3.	22.00	55.34	43.11	48.16	51.37	51.45	3.1946	-0.1939
3.	23.00	55.34	43.16	48.25	51.46	51.45	3.2111	-0.2699
3.	24.00	55.40	43.20	48.27	51.44	51.45	3.2111	-0.2699
4.	1.00	55.41	43.24	48.10	51.47	51.45	3.1768	-0.2299
4.	2.00	55.29	43.28	48.33	51.49	51.51	3.1768	-0.2299
4.	3.00	55.46	43.30	48.36	51.53	51.51	3.1778	-0.1899
4.	4.00	55.30	43.32	48.39	51.53	51.51	3.1778	-0.1899
4.	5.00	55.50	43.36	48.42	51.60	51.51	3.1900	-0.1599
4.	6.00	55.53	43.38	48.20	51.24	51.51	3.1903	-0.3199
4.	7.00	55.54	43.41	48.40	51.54	51.51	3.1640	-0.3199
4.	8.00	55.57	43.45	48.40	51.52	51.51	3.1223	-0.3199
4.	9.00	55.57	43.46	48.45	51.59	51.62	3.1487	-0.1699
4.	10.00	55.57	43.48	48.45	51.58	51.62	3.1487	-0.1699
4.	11.00	55.57	43.50	48.45	51.55	51.62	3.1263	-0.1699
4.	12.00	55.57	43.51	48.45	51.56	51.62	3.1136	-0.1699
4.	13.00	55.57	43.53	48.45	51.55	51.63	3.1032	-0.1699
4.	14.00	55.56	43.40	48.45	51.55	51.63	3.1906	-0.1699
4.	15.00	55.56	43.42	48.45	51.52	51.63	3.1719	-0.1699
4.	16.00	55.54	43.43	48.45	51.61	51.63	3.1691	-0.0680
4.	17.00	55.53	43.45	48.45	51.60	51.63	3.1569	-0.0830
4.	18.00	55.51	43.43	48.45	51.63	51.63	3.1892	-0.0736
4.	19.00	55.48	43.45	48.45	51.57	51.62	3.1263	-0.1799
4.	20.00	55.50	43.45	48.45	51.60	51.63	3.1136	-0.1799
4.	21.00	55.48	43.55	48.45	51.56	51.63	3.1032	-0.1799
4.	22.00	55.48	43.61	48.45	51.52	51.63	3.0783	-0.2699
4.	23.00	55.48	43.67	48.45	51.49	51.63	3.0406	-0.2699
4.	24.00	55.48	43.73	48.45	51.42	51.63	2.9738	-0.2699
4.	25.00	55.48	43.73	48.45	51.38	51.63	2.9391	-0.2699
5.	1.00	55.48	43.75	48.45	51.37	51.71	2.9246	-0.2699
5.	2.00	55.48	43.78	48.45	51.36	51.71	2.9114	-0.2699
5.	3.00	55.48	43.81	48.45	51.34	51.69	2.8892	-0.2399
5.	4.00	55.48	43.83	48.45	51.32	51.67	2.8793	-0.2299
5.	5.00	55.45	43.85	48.45	51.31	51.66	2.8863	-0.2099
5.	6.00	55.41	43.88	48.45	51.29	51.63	2.8463	-0.1899
5.	7.00	55.40	43.90	48.45	51.25	51.62	2.8427	-0.1690

CANAL C738C6

DAY	TIME	HHRD	JHRD	COMP TWO	COMP ONE	OBS TWO	OBS ONE	DIFF	QUP	QDN
5. 10.00	55.34	55.27	48.40	51.19	51.15	2.7974	51.59	3.1999	-0.4045	1392.5
5. 10.00	55.34	55.27	48.40	51.19	51.15	2.7712	51.59	3.2099	-0.4374	1393.8
5. 11.00	55.31	43.97	48.37	51.12	51.12	2.7914	51.57	3.2099	-0.5858	13323.7
5. 11.00	55.31	43.97	48.37	51.10	51.09	2.7387	51.56	3.1900	-0.4512	11373.2
5. 12.00	55.28	44.99	48.37	51.09	51.09	2.7227	51.56	3.1900	-0.4672	13256.3
5. 13.00	55.25	44.02	48.37	51.02	51.02	2.7227	51.56	3.1900	-0.4367	12886.1
5. 14.00	55.20	44.02	48.37	51.07	51.07	2.7084	51.54	3.1599	-0.4418	12667.2
5. 14.00	55.17	44.04	48.37	51.07	51.07	2.7084	51.54	3.1499	-0.4418	12224.7
5. 15.00	55.15	44.03	48.37	51.04	51.04	2.7065	51.50	3.1299	-0.4234	11241.0
5. 16.00	55.12	44.05	48.37	51.03	51.03	2.6943	51.46	3.1199	-0.4256	11226.0
5. 17.00	55.11	44.13	48.38	51.03	51.03	2.6620	51.46	3.0899	-0.3379	11196.7
5. 18.00	55.11	44.13	48.38	51.03	51.03	2.6642	51.45	3.0799	-0.4257	11198.7
5. 19.00	55.11	44.12	48.38	51.03	51.03	2.6551	51.44	3.0599	-0.4088	1120.2
5. 20.00	54.98	44.12	48.39	51.02	51.02	2.6550	51.42	3.0399	-0.3849	1104.6
5. 21.00	54.98	44.02	48.39	51.04	51.04	2.6550	51.41	3.0499	-0.4042	2037.0
5. 22.00	54.96	44.11	48.36	51.00	51.00	2.6447	51.41	3.0499	-0.4042	1312.1
5. 23.00	54.96	44.11	48.26	50.86	50.86	2.6014	51.38	3.1299	-0.2121	1985.0
5. 24.00	54.79	44.11	48.23	50.82	50.82	2.5923	51.37	3.1199	-0.5185	11241.0
6. 1.00	54.67	44.10	48.22	50.80	50.80	2.5923	51.35	3.1299	-0.5376	11196.7
6. 2.00	54.62	44.10	48.21	50.79	50.79	2.5691	51.34	3.1199	-0.5308	11031.4
6. 3.00	54.26	44.09	48.19	50.76	50.76	2.5623	51.32	3.1099	-0.5276	10956.4
6. 4.00	54.50	44.08	48.18	50.75	50.75	2.5765	51.29	3.1099	-0.5276	10896.4
6. 5.00	54.49	44.08	48.18	50.75	50.75	2.5748	51.29	3.1099	-0.5334	12874.8
6. 6.00	54.49	44.08	48.18	50.75	50.75	2.5748	51.29	3.1099	-0.5351	2007.5
6. 7.00	54.35	44.09	48.16	50.72	50.72	2.5643	51.26	3.1099	-0.5456	10760.7
6. 8.00	54.29	44.09	48.14	50.70	50.70	2.5622	51.25	3.1099	-0.5437	12940.8
6. 9.00	54.23	44.07	48.14	50.69	50.69	2.5580	51.23	3.0899	-0.5319	11054.1
6. 10.00	54.15	44.04	48.14	50.69	50.69	2.5587	51.21	3.0769	-0.5212	11292.1
6. 11.00	54.07	44.03	48.14	50.70	50.70	2.5605	51.20	3.0599	-0.4994	10528.8
6. 12.00	54.00	44.00	48.14	50.70	50.70	2.5608	51.17	3.0399	-0.4791	10850.7
6. 13.00	53.98	43.99	48.14	50.73	50.73	2.5804	51.16	3.0399	-0.4295	12857.2
6. 14.00	53.91	43.93	48.20	50.45	50.45	2.5758	51.15	2.9499	-0.6798	2070.5
6. 15.00	53.87	43.87	48.21	50.40	50.40	2.5610	51.07	2.8699	-0.6774	12820.9
6. 16.00	53.84	43.82	48.24	50.34	50.34	2.5425	51.01	2.7199	-0.5759	11031.4
6. 17.00	53.75	43.76	48.21	50.36	50.36	2.5140	50.95	2.6990	-0.5304	1020.2
6. 18.00	53.62	43.65	48.26	50.35	50.35	2.5097	50.87	2.6039	-0.5192	2231.1
6. 19.00	53.54	43.58	48.31	50.34	50.34	2.5019	50.84	2.5899	-0.5517	2277.3
6. 20.00	53.45	43.51	48.28	50.29	50.29	2.4939	50.81	2.5578	-0.5517	2194.9
6. 21.00	53.40	43.45	48.26	50.28	50.28	2.4943	50.78	2.5000	-0.4896	11283.0
6. 22.00	53.35	43.39	48.24	50.28	50.28	2.4918	50.71	2.4539	-0.4356	11411.1
6. 23.00	53.28	43.32	48.19	50.24	50.24	2.4056	50.60	2.4229	-0.3881	11600.2
6. 24.00	53.23	43.27	48.14	50.20	50.20	2.4066	50.56	2.4119	-0.3636	11576.8
6. 25.00	53.23	43.20	48.09	50.17	50.17	2.0814	50.50	2.4099	-0.3521	11545.3
6. 26.00	53.23	43.15	48.05	50.16	50.16	2.0939	50.45	2.3979	-0.3285	11562.3
6. 27.00	53.20	43.15	48.05	50.10	50.10	2.1061	50.40	2.3979	-0.3045	11618.0
6. 28.00	53.15	43.04	47.95	50.04	50.04	2.1134	50.34	2.3899	-0.2938	11646.7
6. 29.00	53.07	42.98	47.91	50.04	50.04	2.1131	50.29	2.3797	-0.2717	11600.3
6. 30.00	53.02	42.93	47.86	50.00	50.00	2.1441	50.23	2.3679	-0.2446	11608.2
6. 31.00	52.98	42.82	47.81	49.98	49.98	2.1725	50.17	2.3699	-0.1974	11717.6

-0/03-

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CANAL C-38CB 5.16.64 - 5.19.64

DAY	TIME	HHRN	LMED	COMP	THRD	CL	DIFF	CLIP	CLIP	CLIP	CLIP	CLIP	CLIP	CLIP	CLIP
9. New	8:00H	52.17	39.56	47.15	48.63	1.4851	48.75	1.6039	-0.1248	5919.2	8915.8	2899.6			
9. New	9:20H	52.20	39.53	47.13	48.61	1.4894	48.76	1.5999	-0.1105	6891.4	8810.6	2823.2			
9.	10:00	52.23	39.51	47.12	48.61	1.4914	48.76	1.5999	-0.0885	5908.5	8903.4	2823.3			
9.	11:00	52.25	39.52	47.10	48.59	1.4977	48.66	1.5597	-0.0622	6015.5	8803.3	2785.7			
9.	12:00	52.28	39.52	47.09	48.58	1.4973	48.62	1.5399	-0.0426	6048.9	8746.6	2735.7			
9.	13:00	52.32	39.53	47.08	48.80	1.4978	48.59	1.5139	-0.02078	6455.9	9628.3	3285.3			
9.	14:00	52.31	39.63	46.89	48.63	1.7402	48.62	1.7399	-0.0102	6495.5	9632.0	2959.3			
9.	15:00	52.31	39.61	46.81	48.61	1.7462	48.65	1.7890	-0.0337	6508.1	9453.8	2945.7			
9.	16:00	52.29	39.60	46.84	48.59	1.7510	48.66	1.8239	-0.0789	6501.1	949.7	2915.7			
9.	17:00	52.29	39.58	46.83	48.57	1.7488	48.67	1.8639	-0.1211	6537.5	944.8	3068.3			
9.	18:00	52.29	39.57	46.79	48.74	1.7537	48.69	1.8999	-0.1442	6594.6	3028.8	3028.8			
9.	19:00	52.29	39.57	46.76	48.72	1.7615	48.67	1.9199	-0.1584	6415.8	9411.1	2995.2			
9.	20:00	52.29	39.56	46.73	48.49	1.7669	48.66	1.9395	-0.1730	6437.0	2966.5	2966.5			
9.	21:00	52.29	39.55	46.73	48.49	1.7731	48.66	1.9599	-0.1868	6466.3	3346.6	2928.3			
9.	22:00	52.28	39.54	46.68	48.45	1.7774	48.65	1.9700	-0.1925	6461.7	9377.5				
9.	23:00	52.28	39.52	46.65	48.21	1.7895	48.53	1.9869	-0.2029	6585.7	1865.7				
10.	0:00	52.28	39.51	46.69	48.43	1.7843	48.62	1.9859	-0.2856	6587.9	1559.7	1955.6			
10.	1:00	52.28	39.52	46.67	48.25	1.5811	48.62	1.9599	-0.7088	6632.1	8586.7	1964.8			
10.	2:00	52.28	39.42	46.68	48.25	1.5777	48.62	1.9399	-0.7622	6526.6	8556.1	1965.5			
10.	3:00	52.28	39.43	46.68	48.26	1.7745	48.65	1.9199	-0.3454	6613.0	8599.7	1985.1			
10.	4:00	52.28	39.44	46.69	48.26	1.7704	48.59	1.8999	-0.3295	6608.9	8583.5	1985.6			
10.	5:00	52.28	39.47	46.71	48.27	1.7671	48.59	1.8799	-0.3128	6602.9	8588.7	1987.8			
10.	6:00	52.26	39.48	46.72	48.28	1.5644	48.57	1.8595	-0.2955	6587.9	8588.4	1991.0			
10.	7:00	52.26	39.50	46.73	48.28	1.5593	48.57	1.8339	-0.2806	6596.8	8581.7	1994.9			
10.	8:00	52.25	39.51	46.75	48.30	1.5551	48.56	1.8049	-0.2548	6455.7	6455.7	2011.2			
10.	9:00	52.25	39.53	46.76	48.30	1.6833	48.76	1.7800	-0.1516	6455.7	8916.7	2438.7			
10.	10:00	52.25	39.62	46.73	48.35	1.6218	48.54	1.8199	-0.3819	6829.5	2299.9				
10.	11:00	52.25	39.61	46.70	48.27	1.7004	48.59	1.8599	-0.2294	6561.2	8805.8	2238.6			
10.	12:00	52.26	39.61	46.71	48.27	1.6376	48.53	1.8995	-0.2623	6594.5	8876.5	2186.0			
10.	13:00	52.26	39.62	46.72	48.26	1.6101	48.51	1.9293	-0.2537	6601.1	8851.4	2255.3			
10.	14:00	52.26	39.60	46.56	48.26	1.6100	48.51	1.9439	-0.2749	6622.1	8839.9	2217.8			
10.	15:00	52.26	39.60	46.56	48.27	1.6175	48.50	1.9700	-0.1290	6653.4	8819.9	2176.5			
10.	16:00	52.26	39.60	46.53	48.20	1.6192	48.50	1.9999	-0.2334	6506.5	8759.9	2294.4			
10.	17:00	52.26	39.60	46.50	48.17	1.6165	48.50	1.9899	-0.3819	6512.8	8489.2	1916.3			
10.	18:00	52.27	39.58	46.48	48.08	1.6020	48.16	1.9816	-0.3738	6563.6	8495.2	1928.9			
10.	19:00	52.26	39.61	46.68	48.31	1.6305	48.54	1.8599	-0.2294	6561.2	8805.8	2238.6			
10.	20:00	52.26	39.60	46.63	48.26	1.6376	48.53	1.8995	-0.2623	6594.5	8876.5	2186.0			
10.	21:00	52.26	39.60	46.59	48.26	1.6137	48.40	1.9339	-0.2362	6523.3	8513.4	1951.1			
10.	22:00	52.26	39.59	46.56	48.06	1.6184	48.37	1.9193	-0.3015	6567.9	8519.4	1952.7			
10.	23:00	52.26	39.59	46.55	48.07	1.6212	48.34	1.8999	-0.2749	6581.7	8469.7	1899.9			
11.	0:00	52.26	39.58	46.54	48.06	1.6283	48.32	1.8799	-0.2536	6537.6	1975.1				
11.	1:00	52.26	39.55	46.53	48.05	1.6281	48.29	1.8699	-0.4118	6566.0	8531.6	1977.5			
11.	2:00	52.26	39.54	46.53	48.06	1.6315	48.26	1.8339	-0.3084	6551.0	8549.6	1991.8			
11.	3:00	52.19	39.51	46.42	48.07	1.6111	48.41	1.9599	-0.3488	6574.0	8501.3	1927.2			
11.	4:00	52.17	39.39	46.42	48.03	1.6137	48.40	1.9339	-0.3262	6523.3	8513.4	1951.1			
11.	5:00	52.17	39.37	46.41	48.02	1.6121	48.21	1.7999	-0.1878	6573.3	8463.7	1899.3			
11.	6:00	52.17	39.35	46.40	48.00	1.6164	48.20	1.7799	-0.1735	6569.7	8469.7	1899.9			
11.	7:00	52.19	39.34	46.40	47.85	1.6001	48.17	1.7799	-0.1799	6199.7	7903.6	1703.8			
11.	7:00	52.19	39.34	46.40	47.85	1.4337	48.15	1.7599	-0.3067	6550.6	6201.2	1695.6			

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DAY	TIME	HHRD	JTHED	HMED	COMP TWO	OBS DH	OBS TIME	OBS DH	QDN	
11.	8:00	52.19	39.25	46.40	47.85	1.4336	48.13	1.7339	-0.2863	
11.	52.20	39.23	46.40	47.85	1.4539	48.12	1.7200	-0.2660	7902.5	
11.	52.20	39.26	46.40	47.85	1.4524	48.10	1.7099	-0.2575	1695.2	
11.	10:00	52.20	39.26	46.40	47.85	1.4528	48.09	1.6999	-0.2368	1689.4
11.	11:00	52.20	39.25	46.40	47.85	1.4531	48.09	1.6899	-0.2170	1682.4
11.	12:00	52.20	39.25	46.40	47.85	1.4531	48.09	1.6799	-0.2170	1675.8
11.	13:00	52.21	39.25	46.41	47.85	1.4529	48.07	1.6699	-0.2170	1670.3
11.	14:00	52.21	39.25	46.41	47.86	1.4520	48.06	1.6499	-0.1979	1670.4
11.	15:00	52.23	39.26	46.41	47.86	1.4507	48.04	1.6399	-0.1892	1668.0
11.	16:00	52.23	39.26	46.41	47.86	1.4510	48.03	1.6199	-0.1689	1660.0
11.	17:00	52.23	39.26	46.41	47.86	1.4513	48.01	1.6099	-0.1586	1659.0
11.	18:00	52.23	39.26	46.41	47.86	1.4515	48.00	1.5999	-0.1484	1652.0
11.	19:00	52.25	39.26	46.41	47.85	1.4517	48.00	1.5899	-0.1452	1652.5
11.	20:00	52.25	39.27	46.41	47.85	1.4517	47.98	1.5799	-0.1452	1650.0
11.	21:00	52.25	39.27	46.41	47.85	1.4420	47.98	1.5699	-0.1279	1647.7
11.	22:00	52.27	39.27	46.40	47.85	1.4436	47.98	1.5599	-0.1363	1640.0
11.	23:00	52.28	39.27	46.40	47.85	1.4454	47.98	1.5499	-0.1454	1638.0
11.	24:00	52.28	39.28	46.40	47.85	1.3930	47.98	1.5399	-0.1969	1630.6
12.	1:00	52.29	39.28	46.41	47.85	1.3916	47.98	1.5299	-0.1983	1620.1
12.	2:00	52.29	39.28	46.41	47.85	1.3903	47.98	1.5199	-0.1896	1614.3
12.	3:00	52.31	39.27	46.42	47.86	1.3894	47.98	1.5099	-0.1805	1608.5
12.	4:00	52.31	39.28	46.42	47.86	1.3891	47.98	1.4999	-0.1797	1604.2
12.	5:00	52.32	39.28	46.43	47.86	1.3875	47.98	1.4899	-0.1739	1600.0
12.	6:00	52.32	39.28	46.44	47.86	1.3860	47.98	1.4799	-0.1724	1594.9
12.	7:00	52.34	39.28	46.44	47.86	1.3852	47.98	1.4699	-0.1639	1588.9
12.	8:00	52.34	39.28	46.44	47.86	1.3871	47.98	1.4599	-0.1447	1582.7
12.	9:00	52.34	39.29	46.44	47.86	1.3867	47.98	1.4499	-0.1397	1577.7
12.	10:00	52.34	39.29	46.44	47.86	1.3854	47.98	1.4399	-0.1352	1571.7
12.	11:00	52.35	39.29	46.44	47.86	1.3859	47.98	1.4299	-0.1345	1565.5
12.	12:00	52.37	39.30	46.44	47.86	1.3857	47.98	1.4199	-0.1340	1568.6
12.	13:00	52.37	39.28	46.44	47.86	1.3859	47.98	1.4099	-0.1336	1562.2
12.	14:00	52.37	39.28	46.44	47.86	1.3859	47.98	1.3999	-0.1336	1556.8
12.	15:00	52.38	39.31	46.44	47.86	1.3850	47.98	1.3899	-0.1336	1550.6
12.	16:00	52.38	39.31	46.44	47.86	1.3852	47.98	1.3799	-0.1336	1544.6
12.	17:00	52.38	39.31	46.44	47.86	1.3846	47.98	1.3699	-0.1336	1538.0
12.	18:00	52.38	39.31	46.44	47.86	1.3846	47.98	1.3599	-0.1336	1532.5
12.	19:00	52.38	39.32	46.44	47.86	1.3846	47.98	1.3499	-0.1336	1527.0
12.	20:00	52.38	39.32	46.44	47.86	1.3849	47.98	1.3399	-0.1336	1521.5
12.	21:00	52.38	39.53	46.44	47.86	1.3851	47.98	1.3299	-0.1336	1516.0
12.	22:00	52.38	39.53	46.44	47.86	1.3861	47.98	1.3199	-0.1336	1510.4
12.	23:00	52.38	39.54	46.43	47.86	1.3852	47.98	1.3099	-0.1336	1504.8
12.	0:00	52.38	39.54	46.43	47.86	1.3852	47.98	1.2999	-0.1336	1499.2
13.	1:00	52.38	39.55	46.43	47.86	1.3846	47.98	1.2899	-0.1336	1493.6
13.	2:00	52.38	39.55	46.43	47.86	1.3846	47.98	1.2799	-0.1336	1488.0
13.	3:00	52.37	39.56	46.42	47.86	1.3847	47.98	1.2699	-0.1336	1482.4
13.	4:00	52.37	39.57	46.42	47.86	1.3847	47.98	1.2599	-0.1336	1476.9
13.	5:00	52.37	39.57	46.41	47.86	1.3832	47.98	1.2499	-0.1336	1472.0
13.	6:00	52.37	39.58	46.41	47.86	1.3832	47.98	1.2399	-0.1336	1465.5
13.	7:00	52.37	39.58	46.41	47.86	1.3821	47.98	1.2299	-0.1336	1459.6

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CANAL C-38CB

DAY	TIME	HHR/EU	HME/DH	DMH/EU	CMP/DH	GHS/TWEU	TWEU	OHS/DH	QINN	QUP
13.	8.00	52.37	39.35	46.41	47.74	1.3300	47.95	1.5319	-0.2049	626.0
13.	9.00	52.37	39.37	46.42	47.74	1.3258	47.95	1.5299	-0.2041	621.4
13.	10.00	52.37	39.39	46.44	47.76	1.3205	47.95	1.5039	-0.1894	623.1
13.	11.00	52.37	39.42	46.46	47.78	1.3226	47.95	1.4899	-0.1673	624.2
13.	12.00	52.37	39.44	46.48	47.79	1.3162	47.94	1.4599	-0.1437	630.0
13.	13.00	52.37	39.46	46.50	47.88	1.3089	47.94	1.4399	-0.0510	6309.6
13.	14.00	52.37	39.48	46.52	47.87	1.3073	47.94	1.4499	-0.0626	6317.6
13.	15.00	52.37	39.53	46.58	47.86	1.3017	47.92	1.4699	-0.0682	6328.8
13.	16.00	52.35	39.52	46.57	47.85	1.3040	47.92	1.4599	-0.0759	6326.7
13.	17.00	52.35	39.52	46.56	47.84	1.3058	47.91	1.4599	-0.0741	6322.8
13.	18.00	52.35	39.51	46.55	47.83	1.3086	47.91	1.4699	-0.0813	6331.9
13.	19.00	52.35	39.51	46.55	47.83	1.3095	47.91	1.4699	-0.0814	6331.9
13.	20.00	52.34	39.51	46.55	47.83	1.3082	47.91	1.4599	-0.0717	6330.6
13.	21.00	52.34	39.50	46.55	47.83	1.3074	47.91	1.4599	-0.0704	6329.8
13.	22.00	52.34	39.50	46.55	47.83	1.3084	47.91	1.4599	-0.0705	6330.1
13.	23.00	52.34	39.50	46.54	47.83	1.3090	47.91	1.4699	-0.0790	6326.7
13.	24.00	52.34	39.49	46.54	47.82	1.3090	47.90	1.4599	-0.0679	6328.0
14.	1.00	52.34	39.49	46.54	47.82	1.3017	47.90	1.4599	-0.0682	6326.6
14.	2.00	52.34	39.49	46.54	47.82	1.3018	47.90	1.4599	-0.0681	6328.2
14.	3.00	52.34	39.48	46.54	47.82	1.3018	47.90	1.4599	-0.0681	6328.2
14.	4.00	52.32	39.48	46.54	47.82	1.3090	47.88	1.4599	-0.0569	6321.3
14.	5.00	52.32	39.48	46.55	47.83	1.3042	47.88	1.4599	-0.0567	6326.5
14.	6.00	52.32	39.47	46.53	47.82	1.3042	47.87	1.4499	-0.0542	6325.8
14.	7.00	52.32	39.47	46.53	47.82	1.3057	47.87	1.4499	-0.0542	6322.7
14.	8.00	52.32	39.47	46.53	47.82	1.3057	47.87	1.4499	-0.1288	6310.5
14.	9.00	52.32	39.44	46.53	47.75	1.3211	47.87	1.4499	-0.1288	6310.5
14.	10.00	52.32	39.44	46.53	47.75	1.3211	47.87	1.4499	-0.1206	6316.4
14.	11.00	52.31	39.43	46.54	47.76	1.3023	47.87	1.4399	-0.1196	6316.4
14.	12.00	52.31	39.43	46.53	47.76	1.3042	47.87	1.4399	-0.1196	6316.4
14.	13.00	52.31	39.43	46.55	47.76	1.3190	47.87	1.4299	-0.1109	6315.1
14.	14.00	52.31	39.43	46.56	47.76	1.3190	47.87	1.4299	-0.1109	6315.1
14.	15.00	52.29	39.43	46.56	47.76	1.3166	47.88	1.4199	-0.1025	6316.0
14.	16.00	52.29	39.43	46.57	47.76	1.3166	47.88	1.4199	-0.1026	6316.0
14.	17.00	52.29	39.43	46.57	47.76	1.3165	47.88	1.4199	-0.0936	6332.3
14.	18.00	52.29	39.43	46.57	47.76	1.3162	47.88	1.4199	-0.1037	6311.3
14.	19.00	52.25	39.43	46.57	47.76	1.3157	47.88	1.4199	-0.0942	6326.6
15.	2.00	52.25	39.43	46.57	47.76	1.3161	47.88	1.4199	-0.1038	6301.6
15.	3.00	52.25	39.43	46.57	47.76	1.3162	47.88	1.4199	-0.1037	6318.8
15.	4.00	52.25	39.43	46.57	47.76	1.3169	47.88	1.4199	-0.1037	6304.5
15.	5.00	52.25	39.43	46.57	47.76	1.3154	47.88	1.4199	-0.1045	6297.4
15.	6.00	52.25	39.43	46.57	47.76	1.3157	47.88	1.4199	-0.1047	6297.7
15.	7.00	52.25	39.43	46.57	47.76	1.3101	47.88	1.4299	-0.1209	6131.8
15.	8.00	52.25	39.42	46.57	47.76	1.3103	47.88	1.4299	-0.0988	6130.8
15.	9.00	52.25	39.42	46.56	47.77	1.3119	47.85	1.3999	-0.0886	6142.2
15.	10.00	52.25	39.42	46.56	47.76	1.3130	47.85	1.3999	-0.0886	6142.2
15.	11.00	52.25	39.42	46.56	47.76	1.3129	47.85	1.3999	-0.0886	6142.2
15.	12.00	52.26	39.42	46.56	47.75	1.3127	47.82	1.3799	-0.0670	6141.7
15.	13.00	52.26	39.42	46.56	47.75	1.3114	47.82	1.3799	-0.0653	6162.1

- 7/7 -

- 7/7 -

7.11 Computed Storage and Lateral Inflow Values for
Each Reach.

Explanatory notes pertaining to the listings:

S-65D - S-65E: reach between Structures 65E and 65D.

S-65C - S-65D: reach between Structures 65D and 65C.

S-65B - S-65C: reach between Structures 65C and 65B.

Day: Calendar day number for the month of October in the year 1969.

Hour: Actual clock time of the day = 1,2,...,23,24. 1 corresponds to 1:00AM of the day and 24 corresponds to midnight of the day.

QD-QU: Average QL of two consecutive hours.

DSTORE: Change in the water storage of the reach between two consecutive hours.

QLAT: (QD-QU) + DSTORE.

SUM: Cumulative QLAT.

AF: Acre feet.

Discrepancies in all the numbers are due to rounding off truncation errors.

S-65D - S-65E

S-65C - S-65J

S-65H - S-65L

	DAY	HOUR	QD-QU AF	DSTORE AF	SUM AF	OLAT AF	QD-QU AF	DSTORE AF	OLAT AF	SUM AF	QD-QU AF	DSTORE AF	OLAT AF	SUM AF	
1	9	62.	-44.	18.	17.	61.	-11.	49.	49.	96.	-18.	77.	76.	-----	
	10	60.	-42.	16.	33.	62.	1.	63.	111.	95.	0.	95.	17.	-----	
	11	40.	-45.	27.	64.	55.	176.	244.	91.	95.	0.	95.	281.	-----	
	12	23.	-21.	44.	72.	69.	-0.	68.	111.	106.	-10.	80.	347.	-----	
	13	25.	-21.	46.	118.	72.	0.	71.	315.	87.	59.	145.	493.	-----	
	14	26.	-22.	48.	166.	70.	0.	69.	384.	88.	80.	168.	661.	-----	
	15	28.	-22.	50.	215.	68.	0.	67.	452.	90.	61.	151.	812.	-----	
	16	29.	-22.	52.	267.	66.	0.	66.	517.	92.	83.	174.	981.	-----	
	17	48.	-41.	89.	356.	79.	10.	89.	606.	81.	90.	171.	1156.	-----	
	18	66.	-10.	411.	96.	76.	172.	178.	47.	22.	12.	12.	122.	-----	
	19	64.	-10.	53.	463.	101.	80.	181.	959.	24.	19.	43.	1271.	-----	
	20	50.	-10.	39.	502.	101.	92.	193.	1152.	41.	87.	180.	1406.	-----	
	21	49.	-3.	52.	555.	98.	27.	125.	1277.	49.	193.	242.	1649.	-----	
	22	53.	-6.	46.	601.	105.	63.	168.	1446.	59.	299.	2007.	2007.	-----	
	23	44.	11.	55.	656.	111.	-13.	97.	1343.	81.	130.	211.	2219.	-----	
	24	26.	12.	38.	693.	113.	19.	132.	1675.	102.	193.	231.	2516.	-----	
2	1	8.	11.	19.	712.	115.	-13.	101.	1176.	120.	-52.	57.	2592.	-----	
	2	10.	11.	21.	734.	114.	-13.	100.	1876.	119.	-52.	63.	2645.	-----	
	3	12.	0.	12.	745.	114.	-13.	100.	1977.	117.	-51.	65.	2714.	-----	
	4	14.	23.	37.	782.	113.	-13.	99.	2076.	116.	-51.	64.	2777.	-----	
	5	16.	0.	16.	798.	113.	-13.	99.	2175.	116.	-50.	63.	2841.	-----	
	6	18.	23.	41.	839.	112.	-13.	98.	2272.	113.	-50.	62.	2903.	-----	
	7	12.	33.	972.	111.	111.	-13.	97.	2370.	88.	-34.	53.	2954.	-----	
	8	54.	32.	86.	958.	113.	36.	149.	2518.	106.	93.	198.	3156.	-----	
	9	69.	1.	90.	1048.	114.	-40.	74.	2592.	135.	-49.	95.	3240.	-----	
	10	97.	1.	97.	1145.	112.	-40.	71.	2653.	136.	-22.	112.	3353.	-----	
	11	112.	-15.	127.	1273.	109.	-26.	82.	2745.	137.	-22.	113.	3466.	-----	
	12	72.	-83.	-11.	1260.	109.	-36.	72.	2817.	137.	-22.	114.	3582.	-----	
	13	30.	-9.	29.	98.	98.	-36.	61.	2878.	139.	-21.	117.	3694.	-----	
	14	30.	-9.	29.	1289.	98.	-36.	61.	2974.	139.	-23.	117.	3814.	-----	
	15	48.	11.	69.	1338.	84.	-12.	71.	3019.	139.	-24.	115.	3922.	-----	
	16	39.	-70.	33.	1371.	84.	-12.	71.	3019.	139.	-23.	115.	4042.	-----	
	17	30.	11.	41.	1412.	83.	-12.	70.	3039.	139.	-23.	115.	4256.	-----	
	18	39.	-48.	147.	1559.	98.	195.	293.	3382.	147.	66.	215.	4853.	-----	
	19	30.	-138.	617.	2176.	105.	195.	260.	3642.	114.	537.	5451.	5652.	-----	
	20	406.	-138.	298.	2474.	119.	245.	364.	4006.	113.	251.	-166.	5482.	-----	
	21	349.	-61.	365.	2839.	262.	281.	544.	4550.	86.	-251.	6463.	5482.	-----	
	22	234.	341.	3249.	344.	344.	803.	1193.	1196.	5047.	67.	911.	978.	-----	
	23	303.	107.	341.	3590.	344.	342.	686.	6879.	1171.	2955.	3127.	11845.	-----	
	24	414.	153.	650.	4260.	297.	513.	811.	7690.	258.	-249.	6.	11854.	-----	
2	3	1	362.	153.	516.	5322.	371.	260.	631.	8320.	221.	-175.	145.	11997.	-----
	3	3	362.	159.	522.	5844.	380.	295.	679.	8999.	322.	-267.	2974.	15173.	-----
	4	373.	75.	685.	6834.	170.	303.	473.	10109.	449.	957.	1420.	16579.	-----	
	5	396.	92.	488.	7422.	173.	335.	508.	10617.	449.	1167.	1616.	1819.	-----	
	6	386.	81.	466.	7788.	214.	452.	667.	1124.	440.	960.	1404.	1959.	-----	
	7	379.	95.	474.	8262.	260.	152.	412.	11689.	404.	-257.	-123.	19441.	-----	
	8	409.	506.	8767.	271.	155.	426.	12123.	354.	-377.	-22.	19415.	-----		

S-650 - S-65E

S-65C - S-650

S-64W - S-65C

DAY HOUR			QD-QU	DISTORE AF	QIAT AF	SUM AF	QIAT AF	DISTORE AF	QIAT AF	SUM AF	QIAT AF	DISTORE AF	QIAT AF	SUM AF
3 9	433.	62.	495.	9262.	279.	195.	473.	12596.	322.	363.	691.	20109.	348.	
10	406.	-29.	376.	9638.	275.	-20.	254.	12850.	665.	-1041.	-175.	19335.	377.	
11	252.	-187.	65.	9703.	278.	371.	649.	13459.	241.	2218.	2599.	21791.	381.	
12	146.	308.	454.	10157.	277.	352.	609.	14108.	277.	13707.	23707.			
13	170.	336.	506.	10663.	266.	307.	672.	14680.	287.	335.	623.	24330.	384.	
14	80.	258.	338.	11001.	274.	314.	1528.	15128.	271.	-186.	24670.			
15	0.	377.	376.	11378.	281.	122.	403.	15730.	245.	-7408.	-223.	24196.	385.	
16	390.	429.	1807.	12606.	263.	162.	16156.	244.	1394.	15516.	25194.	386.		
17	196.	547.	743.	12549.	225.	131.	356.	16512.	284.	1519.	1603.	27594.	387.	
18	451.	183.	634.	13184.	199.	163.	361.	16873.	292.	-3176.	-92.	27513.	388.	
19	549.	-233.	315.	13499.	205.	230.	495.	17906.	284.	2843.	981.			
20	511.	-229.	281.	13780.	234.	228.	462.	17707.	262.	-1184.	-92.	27571.	389.	
21	474.	-227.	264.	14026.	261.	94.	325.	18125.	235.	251.	438.	28076.	390.	
22	440.	-200.	239.	14264.	274.	129.	404.	18287.	234.	630.	653.	28924.	391.	
23	406.	-218.	186.	14451.	290.	130.	425.	18349.	238.	-86.	151.	29025.	392.	
3 24	371.	-194.	176.	14627.	309.	129.	438.	1987.	224.	124.	354.	2946.	393.	
4	342.	-165.	175.	14802.	324.	127.	461.	19938.	227.	234.	461.	29839.	394.	
5	317.	-163.	153.	14955.	338.	127.	485.	20303.	225.	232.	457.	30346.	395.	
6	293.	158.	133.	15088.	350.	56.	496.	20708.	226.	283.	510.	30856.	396.	
7	269.	-152.	115.	15203.	359.	56.	415.	21123.	224.	290.	520.	31375.	397.	
8	240.	-219.	20.	15223.	371.	102.	473.	21596.	231.	249.	430.	31875.	398.	
9	205.	-207.	-2.	15220.	401.	57.	459.	22055.	195.	-2321.	-426.	29726.	399.	
10	169.	-198.	-29.	15191.	420.	72.	225.	22547.	184.	1996.	2172.	21906.	400.	
11	134.	-174.	-40.	15149.	426.	99.	525.	23072.	206.	-74.	2051.	22746.	401.	
12	109.	-91.	18.	15167.	437.	52.	489.	23561.	208.	507.	718.			
13	82.	-74.	21.	15186.	443.	48.	491.	24053.	210.	-38.	174.	32940.	402.	
14	67.	-87.	8.	15192.	452.	48.	500.	24552.	210.	-37.	172.	33092.	403.	
15	52.	-91.	-20.	15174.	461.	51.	511.	25084.	208.	-39.	168.	33577.	404.	
16	32.	-71.	-19.	15154.	469.	48.	518.	25585.	201.	-41.	160.	33416.	405.	
17	86.	-201.	-18.	14865.	488.	-185.	222.	28030.	215.	321.	535.	33954.	406.	
18	400.	-211.	211.	15076.	332.	124.	456.	26259.	227.	-66.	184.	34376.	407.	
19	-129.	301.	15377.	311.	105.	436.	26695.	224.	-37.	181.	34235.	408.		
20	337.	258.	294.	15636.	309.	105.	479.	27094.	224.	-45.	177.	34306.	409.	
21	367.	370.	16005.	241.	36.	278.	27132.	224.	1119.	1347.	34467.	410.		
22	63.	155.	219.	16224.	198.	205.	403.	27775.	224.	-128.	100.	34947.	411.	
23	70.	159.	230.	16454.	203.	245.	448.	28222.	219.	-148.	71.	35018.	412.	
24	77.	162.	240.	16694.	208.	210.	418.	28640.	210.	-121.	97.	35105.	413.	
25	84.	167.	271.	16965.	212.	254.	466.	29106.	200.	-134.	65.	35170.	414.	
26	91.	169.	260.	17225.	218.	257.	476.	29582.	208.	-237.	224.	35146.	415.	
27	98.	193.	291.	17515.	224.	257.	481.	30063.	205.	-126.	90.	35226.	416.	
28	106.	111.	217.	17722.	227.	108.	335.	30398.	207.	-50.	196.	35384.	417.	
29	117.	124.	251.	17933.	227.	106.	334.	30731.	204.	-44.	198.	35542.	418.	
30	128.	136.	264.	18247.	228.	146.	374.	31105.	199.	-67.	130.	35672.	419.	
31	137.	277.	18524.	229.	107.	336.	31441.	197.	-47.	149.	35817.	420.		
32	152.	138.	200.	18814.	229.	107.	336.	31777.	190.	-53.	135.	35952.	421.	
33	220.	197.	417.	19231.	226.	135.	361.	32138.	188.	-60.	126.	36080.	422.	
34	277.	-70.	206.	19457.	229.	85.	314.	32452.	184.	-245.	141.	36127.	423.	
35	265.	-70.	195.	19631.	239.	95.	324.	32176.	174.	-338.	-169.	36153.	424.	

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S-650 - S-65E

S-650 - S-65C

S-65C - S-65D

S-650 - S-65E

DAY	HOUR	WD-QU AF	DS-TURE AF	QLAT AF	SUM AF	WD-QU AF	DS-TURE AF	QLAT AF	SUM AF	WD-QU AF	DS-TURE AF	QLAT AF	SUM AF
5	9	258.	-0.	258.	198.89.	248.	179.	328.	3,4104.	167.	-237.	-71.	35,781.
10	256.	23.	279.	206.68.	255.	118.	373.	3,3477.	162.	-154.	0.	35,780.	
11	254.	50.	253.	206.21.	260.	80.	341.	3,2817.	159.	-44.	117.	35,780.	
12	251.	23.	247.	208.95.	265.	118.	383.	3,4201.	158.	-56.	79.	36,009.	
13	250.	-0.	249.	209.44.	267.	1.	268.	3,4459.	160.	83.	743.	36,242.	
14	249.	23.	272.	212.6.	269.	78.	347.	3,4816.	162.	-130.	31.	36,210.	
15	249.	23.	272.	214.87.	271.	-1.	269.	3,7085.	162.	-6.	156.	3,643.	
16	248.	-0.	248.	217.35.	272.	81.	353.	3,5648.	164.	-37.	126.	3,6502.	
17	241.	26.	238.	219.73.	315.	186.	501.	3,5939.	160.	-66.	95.	3,6557.	
18	175.	50.	173.	221.66.	354.	-9.	314.	3,6292.	160.	7.	167.	36,575.	
19	175.	23.	198.	233.44.	352.	-1.	350.	3,6802.	166.	-8.	198.	36,982.	
20	205.	52.	257.	260.1.	349.	-7.	36943.	172.	176.	89.	661.	37,243.	
21	233.	-22.	210.	288.11.	347.	-38.	308.	3,7250.	176.	-270.	-94.	37,140.	
22	232.	-22.	210.	230.21.	355.	-1.	376.	3,7603.	164.	-912.	-746.	3,6397.	
23	232.	-22.	209.	232.30.	363.	2.	364.	3,7968.	153.	-99.	53.	3,6442.	
24	231.	-22.	208.	234.38.	366.	1.	367.	3,8335.	154.	-183.	-221.	3,6442.	
5	1	231.	0.	231.	236.69.	367.	-40.	327.	3,9462.	156.	-89.	170.	36,911.
6	2	231.	-22.	208.	238.77.	368.	-2.	369.	3,9031.	162.	-101.	59.	36,551.
3	230.	-22.	208.	240.85.	370.	-38.	331.	3,9362.	165.	-169.	-4.	36,544.	
4	231.	-1.	232.	243.11.	370.	-40.	329.	3,9631.	169.	-85.	83.	36,624.	
5	231.	-22.	208.	245.25.	371.	-1.	312.	4,0863.	173.	-183.	-13.	36,615.	
6	230.	-21.	208.	247.33.	374.	-2.	374.	4,0454.	176.	-101.	74.	3,668.	
7	230.	-21.	208.	249.41.	374.	-8.	295.	4,0134.	183.	-49.	113.	3,668.	
8	231.	0.	231.	251.72.	372.	-39.	332.	4,1056.	191.	202.	-10.	36,982.	
9	232.	-21.	210.	253.81.	369.	-77.	291.	4,1357.	202.	212.	-270.	37,243.	
10	232.	-22.	209.	255.90.	367.	-37.	329.	4,1686.	213.	-8.	211.	37,416.	
11	232.	0.	232.	256.22.	390.	-94.	295.	4,1981.	176.	-48.	7119.	37,306.	
12	233.	-22.	210.	260.32.	423.	-43.	379.	4,2360.	185.	3.	187.	37,306.	
13	234.	-22.	211.	262.43.	439.	-244.	194.	4,2554.	201.	-129.	71.	37,317.	
14	234.	0.	238.	248.81.	453.	-246.	206.	4,2760.	179.	-125.	24.	37,431.	
15	243.	-22.	220.	267.01.	453.	-234.	218.	4,2976.	176.	-208.	37817.		
16	241.	-22.	224.	269.26.	442.	-245.	206.	4,3184.	186.	-176.	10.	37,639.	
17	252.	0.	222.	271.77.	443.	-242.	201.	4,3384.	185.	-166.	351.	38,172.	
18	256.	-22.	233.	274.10.	457.	-201.	43639.	172.	-159.	12.	38,192.		
19	256.	-22.	237.	276.47.	458.	-269.	188.	4,3827.	177.	-359.	936.	38,728.	
20	266.	0.	266.	279.13.	444.	-267.	176.	4,4003.	231.	-287.	-306.	38,671.	
21	271.	-22.	248.	281.61.	434.	-242.	212.	4,4125.	275.	-101.	167.	38,838.	
22	271.	0.	276.	284.38.	424.	-238.	165.	4,4380.	284.	-98.	185.	39,024.	
23	280.	-68.	211.	284.49.	416.	-251.	164.	4,4554.	287.	-326.	-55.	38,987.	
24	278.	-68.	209.	288.57.	411.	-242.	198.	4,4742.	290.	-334.	-42.	38,943.	
7	1	216.	-67.	207.	290.65.	407.	-246.	159.	4,4901.	292.	-322.	-31.	38,912.
3	212.	-67.	206.	294.75.	398.	-207.	190.	4,5093.	294.	-249.	-29.	38,947.	
6	24.	-68.	204.	297.6.	395.	-205.	188.	4,5472.	293.	-325.	-17.	38,905.	
7	1	216.	-67.	207.	391.	-202.	188.	4,5679.	299.	-243.	-76.	38,961.	
4	269.	-67.	199.	298.75.	387.	-201.	185.	4,5849.	301.	-313.	-11.	38,989.	
5	266.	-66.	196.	300.71.	378.	-367.	114.	4,5855.	305.	-266.	-39.	38,981.	
6	264.	-66.	197.	302.68.	394.	-367.	52.	4,5997.	308.	-767.	-459.	38,526.	
7	8	267.	-65.	222.	304.90.	394.	-341.	52.	4,5997.	308.	-767.	-459.	38,526.

S-65D - S-65E

S-65C - S-65D

S-65H - S-65C

DAY	HOUR	QD-QU		DS-TRE		GLAT		SUM		QD-QU		DS-TRE		GLAT		SUM	
		AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF
7	9	269.	-85.	183.	30673.	406.	-345.	68.	45065.	341.	556.	894.	39424.	-	-	-	-
10	271.	295.	184.	30857.	404.	-315.	68.	46053.	354.	579.	-415.	39008.	-	-	-	-	
11	272.	-84.	187.	31044.	410.	-331.	78.	46131.	335.	-322.	12.	39020.	-	-	-	-	
12	273.	-84.	188.	31232.	400.	-394.	105.	46236.	338.	-260.	-	39017.	-	-	-	-	
13	274.	-63.	211.	31443.	389.	-319.	69.	46305.	342.	-312.	24.	39126.	-	-	-	-	
14	277.	-82.	194.	31636.	304.	-550.	53.	46358.	441.	889.	1331.	40436.	-	-	-	-	
15	278.	-82.	195.	31831.	323.	-544.	-21.	46336.	406.	-1907.	38949.	-	-	-	-		
16	243.	-67.	215.	32106.	371.	-543.	-75.	46263.	275.	-559.	856.	39782.	-	-	-	-	
17	17.	448.	-537.	-90.	32016.	314.	-577.	-26.	46000.	211.	-195.	22.	39486.	-	-	-	-
18	287.	-517.	130.	1884.	318.	-185.	13.	46132.	164.	195.	349.	40154.	-	-	-	-	
19	282.	-121.	160.	32044.	320.	-206.	117.	46248.	175.	197.	40526.	-	-	-	-	-	
20	276.	-119.	156.	32201.	317.	-200.	116.	46364.	186.	200.	383.	40912.	-	-	-	-	
21	243.	-200.	42.	32243.	277.	-319.	-102.	46261.	180.	-169.	10.	40922.	-	-	-	-	
22	210.	-99.	110.	32353.	238.	-182.	55.	46117.	171.	-34.	136.	41058.	-	-	-	-	
23	204.	-83.	120.	32473.	233.	-159.	74.	46390.	176.	-37.	146.	41195.	-	-	-	-	
24	199.	-68.	131.	32606.	229.	-156.	71.	46462.	180.	-31.	142.	41337.	-	-	-	-	
6	1	194.	-93.	100.	32703.	224.	-153.	70.	46512.	184.	-36.	144.	41484.	-	-	-	-
7	2	188.	-65.	122.	32825.	220.	-151.	68.	46600.	183.	-36.	152.	41636.	-	-	-	-
8	184.	-77.	106.	32931.	214.	-165.	48.	46647.	173.	21.	183.	41870.	-	-	-	-	
9	184.	-89.	88.	33019.	209.	-141.	67.	46714.	194.	-57.	160.	42010.	-	-	-	-	
10	178.	-62.	109.	33128.	204.	-137.	66.	46780.	202.	-36.	165.	42116.	-	-	-	-	
11	172.	-62.	109.	33221.	200.	-132.	66.	46846.	207.	-37.	165.	42365.	-	-	-	-	
12	167.	-73.	93.	33221.	196.	-167.	33.	46843.	213.	-16.	194.	42539.	-	-	-	-	
13	101.	-110.	79.	33211.	166.	-167.	55.	46848.	230.	-21.	216.	42760.	-	-	-	-	
14	9	51.	185.	124.	-68.	-68.	49.	46898.	244.	-157.	86.	42846.	-	-	-	-	
15	66.	61.	127.	33522.	114.	-65.	49.	46946.	244.	-157.	86.	42846.	-	-	-	-	
16	70.	164.	33686.	107.	-61.	57.	47004.	244.	-157.	86.	42846.	-	-	-	-		
17	119.	-24.	94.	33780.	103.	-61.	41.	47045.	243.	-157.	83.	43020.	-	-	-	-	
18	120.	-26.	95.	33875.	101.	-60.	40.	47085.	243.	-153.	83.	43109.	-	-	-	-	
19	120.	-26.	96.	33971.	99.	-59.	39.	47125.	260.	-184.	87.	43184.	-	-	-	-	
20	123.	-22.	100.	34653.	88.	-54.	54.	47178.	277.	-153.	123.	43307.	-	-	-	-	
21	123.	-22.	101.	34753.	86.	-54.	39.	47218.	276.	-149.	123.	43423.	-	-	-	-	
22	124.	-22.	101.	34869.	68.	-57.	39.	47255.	275.	-95.	110.	43612.	-	-	-	-	
23	124.	-22.	116.	34869.	52.	-12.	40.	47501.	226.	-98.	126.	44684.	-	-	-	-	
24	154.	-34.	119.	34988.	54.	0.	54.	47556.	225.	-101.	121.	44607.	-	-	-	-	
8	24.	152.	-10.	140.	35128.	-	-	-	-	-	-	-	-	-	-	-	
9	1	151.	-110.	140.	35268.	55.	-12.	42.	47597.	225.	-98.	125.	44933.	-	-	-	-
10	2.	152.	0.	152.	35420.	56.	0.	56.	47653.	224.	-99.	124.	45057.	-	-	-	-
11	152.	0.	152.	35573.	57.	57.	47710.	223.	-146.	125.	45132.	-	-	-	-		
12	153.	0.	153.	35726.	58.	-13.	44.	47754.	221.	-97.	125.	45359.	-	-	-	-	
13	154.	-10.	142.	35868.	59.	0.	59.	47812.	220.	-95.	125.	45382.	-	-	-	-	
14	154.	0.	154.	36022.	59.	-13.	45.	47856.	219.	-113.	111.	45504.	-	-	-	-	
15	155.	0.	155.	36177.	59.	0.	59.	47917.	232.	-92.	143.	45772.	-	-	-	-	
16	132.	-7.	123.	36300.	61.	1.	62.	47979.	241.	-92.	143.	45772.	-	-	-	-	

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DAY	HOUR	QD-QU		DSTORE		QD-QU		DSTORE		QD-QU		DSTORE	
		AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF
9	9	109.	-10.	97.	36397.	62.	-12.	49.	48028.	23.	-89.	147.	59112.
10	10.	108.	-10.	96.	36394.	63.	0.	64.	48091.	23.	-45.	147.	46106.
11	11.	114.	-11.	102.	36396.	56.	-7.	48.	48140.	23.	-37.	144.	46245.
12	12.	120.	-10.	108.	36705.	51.	27.	78.	48218.	223.	-48.	174.	46431.
13	117.	-10.	105.	36610.	51.	19.	33.	52.	48270.	249.	320.	168.	46390.
14	113.	64.	178.	36988.	14.	95.	79.	48349.	258.	-897.	164.	46355.	
15	110.	-22.	86.	37074.	45.	-26.	79.	48366.	244.	-83.	196.	46519.	
16	105.	-22.	82.	37156.	42.	-12.	32.	48398.	242.	-131.	110.	46624.	
17	105.	-22.	82.	37238.	42.	-16.	25.	48443.	247.	-48.	119.	46626.	
18	101.	-12.	88.	3726.	39.	-12.	26.	48449.	252.	-173.	76.	46904.	
19	95.	-10.	83.	37410.	41.	-12.	28.	48476.	249.	-129.	123.	47023.	
20	94.	-10.	83.	37493.	42.	-12.	29.	48505.	246.	-125.	20.	47149.	
21	94.	0.	94.	37587.	43.	-13.	29.	48555.	243.	-122.	119.	47265.	
22	93.	-10.	82.	37669.	43.	-12.	30.	48585.	241.	-61.	150.	47428.	
23	92.	-10.	81.	37749.	79.	-18.	60.	48625.	193.	-396.	174.	47228.	
9	24	112.	-10.	101.	37851.	65.	-50.	14.	48639.	158.	61.	219.	47447.
10	1	132.	-20.	110.	37961.	16.	14.	30.	48669.	162.	37.	194.	47647.
11	130.	-20.	108.	38069.	18.	14.	32.	48701.	163.	36.	201.	47847.	
12	128.	-10.	118.	38187.	19.	14.	33.	48741.	163.	36.	201.	48046.	
4	124.	-9.	117.	3803.	21.	21.	27.	48753.	164.	36.	200.	48249.	
5	126.	-20.	105.	38408.	23.	14.	38.	48811.	164.	36.	202.	48451.	
6	124.	-9.	114.	38429.	25.	14.	39.	48829.	164.	39.	203.	48654.	
7	122.	-20.	102.	38824.	27.	28.	55.	48914.	165.	36.	201.	48856.	
8	113.	-12.	100.	38724.	29.	14.	43.	48988.	166.	80.	245.	49101.	
9	106.	-21.	127.	38851.	16.	15.	31.	48989.	164.	229.	413.	49514.	
10	77.	33.	110.	38761.	16.	15.	31.	48989.	195.	30.	301.	49848.	
11	69.	21.	69.	39030.	73.	-14.	62.	94088.	187.	-226.	15.	59466.	
12	52.	32.	64.	39114.	73.	-0.	72.	49217.	183.	-199.	117.	59632.	
13	56.	22.	77.	39191.	69.	0.	69.	49266.	183.	-124.	59.	49307.	
14	74.	38.	112.	39303.	64.	-1.	63.	49349.	185.	-116.	68.	49575.	
15	68.	-22.	65.	39369.	65.	1.	66.	49444.	182.	66.	49641.	49701.	
16	61.	-21.	59.	39427.	68.	1.	69.	49483.	185.	-121.	63.	49707.	
17	56.	-15.	56.	39483.	75.	-9.	65.	49588.	174.	-161.	13.	49718.	
18	67.	0.	67.	39550.	80.	-27.	52.	49601.	159.	-32.	125.	49841.	
19	68.	0.	68.	39618.	78.	-27.	51.	49611.	159.	-32.	122.	49967.	
20	70.	0.	70.	39689.	76.	-26.	49.	49700.	160.	-3.	163.	50130.	
21	72.	0.	72.	39761.	74.	-26.	47.	49767.	161.	-31.	129.	50252.	
22	74.	0.	74.	39835.	72.	-26.	45.	49792.	162.	-3.	130.	50554.	
23	76.	0.	76.	39910.	70.	-26.	43.	49835.	163.	-32.	129.	50681.	
10	24	77.	0.	77.	39987.	69.	-12.	55.	49830.	163.	-33.	129.	50681.
11	1	79.	0.	79.	40066.	67.	-26.	40.	49930.	164.	3.	167.	50896.
12	2	80.	0.	80.	40146.	65.	-26.	38.	49939.	165.	-32.	133.	50981.
13	82.	0.	82.	40229.	67.	-26.	40.	50009.	161.	-22.	135.	51116.	
4	84.	0.	84.	40313.	69.	-25.	43.	50033.	157.	-31.	124.	51244.	
5	66.	0.	66.	40398.	68.	-25.	41.	50094.	177.	-29.	123.	51365.	
6	88.	-12.	75.	4074.	52.	-93.	-1.	50092.	169.	-149.	19.	51384.	
7	77.	-20.	69.	40542.	37.	1.	38.	50170.	140.	0.	141.	51524.	
11	8	89.	-10.	78.	40521.	38.	0.	39.	50168.	140.	0.	140.	51664.

CF-QU	AF	DSTUR	AF	QLAT	AF	SUM	AF	SUM	AF
-	-	-	-	-	-	-	-	-	-
39.	0.	0.	0.	39.	50.207.	50.207.	0.	50.207.	50.207.
39.	12.	0.	0.	50.	50.257.	50.257.	12.	50.257.	50.257.
39.	0.	0.	0.	38.	50.296.	50.296.	0.	50.296.	50.296.
38.	0.	0.	0.	38.	50.333.	50.333.	0.	50.333.	50.333.
38.	0.	0.	0.	38.	50.371.	50.371.	0.	50.371.	50.371.
37.	0.	0.	0.	37.	50.408.	50.408.	0.	50.408.	50.408.
37.	12.	0.	0.	49.	50.47.	50.47.	12.	50.47.	50.47.
37.	0.	0.	0.	36.	50.493.	50.493.	0.	50.493.	50.493.
36.	0.	0.	0.	36.	50.529.	50.529.	0.	50.529.	50.529.
36.	0.	0.	0.	36.	50.555.	50.555.	0.	50.555.	50.555.
35.	0.	0.	0.	35.	50.600.	50.600.	0.	50.600.	50.600.
35.	13.	0.	0.	48.	50.648.	50.648.	13.	50.648.	50.648.
36.	0.	0.	0.	35.	50.683.	50.683.	0.	50.683.	50.683.
35.	0.	0.	0.	35.	50.718.	50.718.	0.	50.718.	50.718.
35.	-1.	0.	0.	42.	50.761.	50.761.	-1.	50.761.	50.761.
52.	13.	0.	0.	52.	50.825.	50.825.	13.	50.825.	50.825.
52.	0.	0.	0.	52.	50.878.	50.878.	0.	50.878.	50.878.
51.	0.	0.	0.	51.	50.929.	50.929.	0.	50.929.	50.929.
51.	0.	0.	0.	50.	50.979.	50.979.	0.	50.979.	50.979.
50.	13.	0.	0.	50.	51.042.	51.042.	13.	51.042.	51.042.
50.	0.	0.	0.	50.	51.092.	51.092.	0.	51.092.	51.092.
49.	0.	0.	0.	49.	51.141.	51.141.	0.	51.141.	51.141.
49.	0.	0.	0.	48.	51.189.	51.189.	0.	51.189.	51.189.
48.	0.	0.	0.	48.	51.237.	51.237.	0.	51.237.	51.237.
50.	14.	0.	0.	50.	51.301.	51.301.	14.	51.301.	51.301.
51.	0.	0.	0.	51.	51.352.	51.352.	0.	51.352.	51.352.
52.	0.	0.	0.	52.	51.404.	51.404.	0.	51.404.	51.404.
52.	0.	0.	0.	52.	51.457.	51.457.	0.	51.457.	51.457.
53.	13.	0.	0.	53.	51.523.	51.523.	13.	51.523.	51.523.
53.	0.	0.	0.	53.	51.579.	51.579.	0.	51.579.	51.579.
55.	1.	0.	0.	56.	51.635.	51.635.	1.	51.635.	51.635.
56.	0.	0.	0.	56.	51.692.	51.692.	0.	51.692.	51.692.
57.	0.	0.	0.	57.	51.749.	51.749.	0.	51.749.	51.749.
146.	104.	0.	0.	146.	51.942.	51.942.	104.	51.942.	51.942.
236.	0.	0.	0.	236.	52.179.	52.179.	0.	52.179.	52.179.
237.	1.	0.	0.	237.	52.417.	52.417.	1.	52.417.	52.417.
239.	13.	0.	0.	239.	52.669.	52.669.	13.	52.669.	52.669.
239.	0.	0.	0.	239.	52.908.	52.908.	0.	52.908.	52.908.
240.	13.	0.	0.	240.	52.962.	52.962.	13.	52.962.	52.962.
241.	0.	0.	0.	241.	53.162.	53.162.	0.	53.162.	53.162.
241.	13.	0.	0.	241.	53.402.	53.402.	13.	53.402.	53.402.
241.	0.	0.	0.	241.	53.656.	53.656.	0.	53.656.	53.656.
241.	0.	0.	0.	241.	54.998.	54.998.	0.	54.998.	54.998.
242.	13.	0.	0.	242.	55.153.	55.153.	13.	55.153.	55.153.
242.	0.	0.	0.	242.	55.346.	55.346.	0.	55.346.	55.346.
243.	13.	0.	0.	243.	55.652.	55.652.	13.	55.652.	55.652.
243.	0.	0.	0.	243.	55.896.	55.896.	0.	55.896.	55.896.
244.	0.	0.	0.	244.	56.146.	56.146.	0.	56.146.	56.146.
244.	13.	0.	0.	244.	56.384.	56.384.	13.	56.384.	56.384.
244.	0.	0.	0.	244.	56.622.	56.622.	0.	56.622.	56.622.
245.	0.	0.	0.	245.	56.859.	56.859.	0.	56.859.	56.859.
245.	0.	0.	0.	245.	57.106.	57.106.	0.	57.106.	57.106.
148.	-94.	0.	0.	148.	57.452.	57.452.	-94.	57.452.	57.452.

3-650

$$S = 650 - 5 - 65E$$

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S-650 - S-65F

5-65C - 5-65D

S-65H - S-65C

DAY	HOUR	QU-QU	DSTORE	QLAT	SUM	CL-QU	DSTORE	QLAT	SUM	CL-QU	DSTORE	QLAT	SUM
		Af	Af	Af	Af	Af	Af	Af	Af	Af	Af	Af	Af
13	0	68.	-20.	46.	42046.	53.	27.	80.	5,632.	98.	31.	127.	57705.
10	65.	-21.	43.	42089.	55.	28.	83.	5,564.	98.	66.	121.	57705.	
11	63.	-20.	52.	42141.	57.	27.	85.	5,5699.	92.	73.	165.	58125.	
12	60.	-20.	39.	42180.	59.	28.	87.	5,5786.	86.	62.	167.	58125.	
13	50.	-12.	38.	42218.	48.	30.	78.	5,5864.	102.	147.	244.	58125.	
14	42.	-21.	63.	42280.	37.	27.	66.	5,5928.	117.	117.	34.	58125.	
15	29.	-32.	61.	42341.	53.	104.	56032.	5,6022.	114.	41.	12.	58125.	
16	16.	-21.	37.	42376.	64.	-13.	50.	5,6082.	112.	-32.	76.	58125.	
17	35.	-27.	63.	42441.	62.	-10.	61.	5,6143.	112.	-32.	77.	58125.	
18	39.	-10.	29.	42470.	61.	-13.	48.	5,6191.	111.	-32.	73.	58125.	
19	40.	0.	40.	42510.	61.	0.	61.	5,6252.	111.	0.	111.	58928.	
20	41.	-10.	42.	42551.	61.	0.	61.	5,6313.	111.	0.	111.	59019.	
21	42.	-10.	31.	42583.	61.	-13.	48.	5,6361.	112.	1.	111.	59152.	
22	43.	0.	43.	42626.	61.	0.	61.	5,6422.	112.	0.	112.	59264.	
23	44.	0.	44.	42670.	61.	0.	61.	5,6483.	111.	-24.	77.	59341.	
13	24.	46.	0.	46.	42716.	61.	-13.	47.	5,6530.	112.	1.	113.	59455.
14	1	47.	-10.	36.	42752.	61.	0.	61.	5,6591.	112.	0.	112.	59565.
3	48.	0.	47.	42779.	61.	-13.	47.	5,6651.	112.	0.	113.	59678.	
4	50.	0.	49.	42847.	60.	0.	60.	5,6698.	112.	1.	113.	59791.	
5	50.	-10.	40.	42897.	60.	0.	60.	5,6758.	112.	-32.	78.	59869.	
6	51.	0.	51.	42937.	60.	0.	61.	5,6819.	112.	0.	112.	59881.	
7	53.	0.	53.	42986.	60.	-13.	46.	5,6865.	112.	1.	114.	60029.	
8	54.	-3.	51.	43041.	60.	0.	60.	5,6925.	113.	0.	113.	60208.	
9	54.	-10.	44.	43092.	60.	-12.	56971.	98.	-72.	25.	60233.		
10	54.	0.	54.	43135.	61.	0.	61.	5,7033.	84.	-0.	84.	60316.	
11	54.	0.	54.	43189.	61.	0.	61.	5,7094.	85.	34.	111.	60433.	
12	54.	0.	54.	43243.	60.	-13.	47.	5,7141.	86.	1.	87.	60522.	
13	54.	0.	54.	43298.	60.	0.	60.	5,7200.	87.	34.	121.	60643.	
14	53.	-10.	42.	43354.	59.	0.	59.	5,7260.	87.	1.	88.	60731.	
15	52.	0.	52.	43447.	60.	0.	60.	5,7320.	88.	34.	122.	60854.	
16	52.	0.	52.	43499.	59.	0.	59.	5,7379.	89.	0.	124.	61095.	
17	52.	0.	52.	43551.	59.	0.	59.	5,7439.	89.	34.	124.	61197.	
18	52.	0.	52.	43604.	59.	0.	59.	5,7498.	90.	34.	56.	61225.	
19	52.	-10.	41.	43656.	59.	0.	59.	5,7557.	91.	-34.	76.	61335.	
20	52.	0.	51.	43696.	59.	-12.	46.	5,7616.	90.	1.	92.	61428.	
21	51.	0.	51.	43747.	59.	0.	59.	5,7720.	91.	0.	91.	61519.	
22	51.	0.	51.	43798.	59.	0.	59.	5,7779.	92.	0.	92.	61610.	
23	51.	0.	51.	43849.	59.	0.	59.	5,7838.	92.	0.	92.	61702.	
14	24.	51.	0.	51.	43899.	59.	0.	59.	5,7897.	92.	0.	92.	61794.
15	1	51.	0.	51.	43950.	59.	0.	59.	5,7956.	92.	0.	92.	61886.
3	20.	-10.	39.	44040.	59.	0.	59.	5,8015.	92.	0.	92.	61975.	
4	49.	0.	49.	44086.	59.	0.	59.	5,8074.	92.	0.	92.	62076.	
5	49.	0.	49.	44137.	59.	0.	59.	5,8133.	93.	0.	93.	62165.	
6	49.	0.	49.	44186.	59.	0.	59.	5,8193.	93.	0.	93.	62256.	
7	49.	0.	49.	44235.	59.	-13.	45.	5,8252.	100.	-6.	93.	62346.	
15	8.	49.	0.	44283.	58.	0.	58.	5,8356.	107.	1.	101.	62436.	
													62525.

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S-650 - S-65E

S-65R = 5-65C

S-65C = 5-65C

S-65R = 5-65C

DAY HOUR	WD-QU		DISTRE		QLAT		DISTRE		QLAT		SUM		SUM		LSTURE		QLAT		SUM	
	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	AF	
15 9	48*	-10.	38*	44321*	59.	0.	59.	54415*	106.	-35.	73.	92636.	106.	00-00	LSTURE	QLAT	AF	AF	---	
10	48*	0.	48.	44369.	60.	0.	60.	54675.	105.	-24.	74.	92707.	105.	00-00	---	QLAT	AF	AF	---	
11	48*	-10.	37.	44406.	60.	0.	60.	54835.	105.	0.	104.	52611.	105.	00-00	---	QLAT	AF	AF	---	
12	47*	0.*	47.	44453.	61.	0.	61.	54996.	104.*	-32.	70.	62981.	104.*	00-00	---	QLAT	AF	AF	---	
13	47.	0.	47.	44501.	61.	0.	61.	54857.	103.*	-6.	103.	52989.	103.*	00-00	---	QLAT	AF	AF	---	

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7.12 Basis for Developing the Limits.

Maximum allowable gate opening

<u>Structure</u>	<u>Reference</u>
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65E	Curve from C of E	SAJWS	8-6-64
65D	Curve from C of E	SAWJS	8-6-64
65C	"	"	7-29-64
65B	"	"	8-5-64

Discharge Nomographs - submerged controlled

S-65C	Received from C of E	23 Sept 1964
S-65D	"	"
S-65E	"	"
S-65B	"	"

These discharges must be associated with allowable gate openings.

Apron elevation used as "A" in computation of approximate straight line equation was from "As Built" plans.

Maximum head from C of E Operations Manual.

Tieback heights from plans.

Headwater elevation at S-65B from Operations Manual, page 0-44, December 1968.

Table 1. Pertinent information concerning rainfall stations in the lower Kissimmee River Basin and its neighboring areas.

Rainfall Station	Coordinates East-West X	North-South Y	Record Length	Responsible Agency	Maximum Daily Rainfall (inches)	Daily Average Rainfall (inches)
Structure 65 Indian Lake Forestry Tower Yeehaw Jct.-7W	135,300 193,700	1,261,500 1,255,250	March 65 - Dec. 70 Jan. 69 - Dec. 70	FCD FCD	4.86 6.48	0.1321 0.1908
Structure 65A Lake Arbuckle Avon Park Bombing Range	426,300 454,200 371,400 413,900	1,173,100 1,206,900 1,210,700 1,200,100	June 65 - Dec. 70 Sept. 69 - Dec. 70 Apr. 65 - Dec. 70 Aug. 66 - Dec. 70	FCD FCD FCD FCD	6.00 6.10 7.80 5.83	0.1233 0.1298 0.1181 0.1241
Structure 65B Ft. Pierce-3W Structure 65C Structure 68 Highland Park Estates	436,1000 696,200 462,400 454,700 395,300	1,151,600 1,120,400 1,114,600 1,092,100 1,081,100	May 65 - Dec. 70 Jan. 65 - Dec. 70 June 66 - Dec. 70 Feb. 65 - Dec. 70+ June 65 - Dec. 70	FCD FCD FCD FCD FCD	7.15 4.50 4.38 5.15 5.12	0.1207 0.1490 0.1214 0.1174 0.1347
Structure 65D Okeechobee Fld. Station	494,600 567,900	1,082,300 1,061,400	Feb. 65 - Dec. 70 Jan. 65 - Dec. 70	FCD FCD	6.55 4.33	0.1298 0.1442
Structure 65E Brighton H.G.S./#6	509,500 467,800 565,600 533,400 340,700 446,100 378,600 538,400	1,051,100 1,049,700 1,044,200 1,177,200 1,181,300 1,115,400 1,080,600 1,173,100	Nov. 64 - Dec. 70 Jan. 65 - Dec. 70 1919 to date Jan. 70 - Dec. 70 1898 to date 1955 to date 1933-1968 1956 to date	FCD FCD USWB FCD USWB USWB USWB	3.64 7.30 3.78** 2.92 5.51** 4.08** 5.27** 8.56**	0.1279 0.1740** 0.0992 0.1435** 0.1050** 0.1304** 0.1282*
Rocking K Ranch Avon Park Cornwall 11-4NW Lake Placid-2SW Fort Drum						X-values are in terms of East Zone of Florida coordinates. FCD-Central & Southern Florida Flood Control District USWB-means United States Weather Bureau *-refers to the values obtained using the records of length Jan. 1961 thru Dec. 1970 **-refers to the values obtained using the records of length Jan. 1961 thru Dec. 1966.

Table 2. Discharge Equations for S-65B, S-65C, S-65D and S-65E

Structure Name	Discharge Equations	Coefficient of determination, R^2	Mean Squared Error	Standard error of estimates b	c
S-65B	$Q = 160.77(G_0)^{1.0029}(E_H)^{0.4979}$	0.9999	0.00012	0.0012	0.0010
S-65C	$Q = 162.39(G_0)^{0.9917}(E_H)^{0.4982}$	0.9997	0.00058	0.0027	0.0020
S-65D	$Q = 162(G_0)^{0.994}(E_H)^{0.5}$	0.9998	0.00027	0.0019	0.0015
S-65E	$Q = 159.17(G_0)^{1.002}(E_H)^{0.5079}$	0.9998	0.00025	0.0018	0.0027

Table 3. Data for Estimating Minimum Depth (Y5)

<u>Y5/GOAV</u>	<u>F1</u>	<u>S</u>
1.0	1.1	1.0
1.0	1.1	1.5
0.0	1.1	2.0
1.25	1.2	1.0
1.30	1.2	1.5
0.5	1.2	2.0
1.4	1.3	1.0
1.5	1.3	1.5
1.0	1.3	2.0
2.0	1.5	1.0
2.4	1.5	1.5
2.0	1.5	2.0
2.5	1.7	1.0
3.0	1.7	1.5
2.7	1.7	2.0
2.7	1.8	1.0
3.4	1.8	1.5
3.4	1.8	2.0
3.25	2.0	1.0
4.25	2.0	1.5
4.4	2.0	2.0

Table 4. Data for Estimating Length of Eddy Region (EL)

<u>EL</u> <u>H</u>	<u>H</u> <u>GOAV</u>
6.9	0.1
3.73	1.0
3.73	1.0
3.3482	1.792
2.2644	6.0218
2.4154	6.0218
2.9438	3.312
2.9438	3.312
2.8683	3.312
2.36	3.4
2.3	4.2
2.0	5.0
2.05	5.4
1.9	6.12
2.05	6.5
1.7	10.0

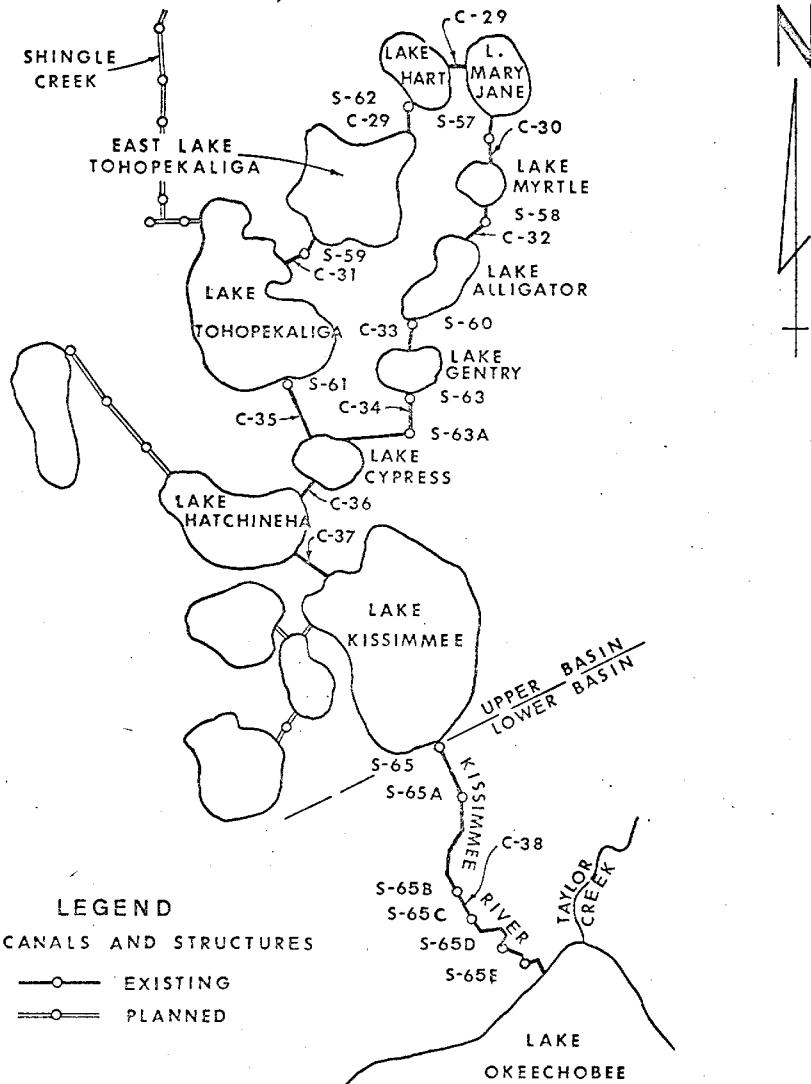
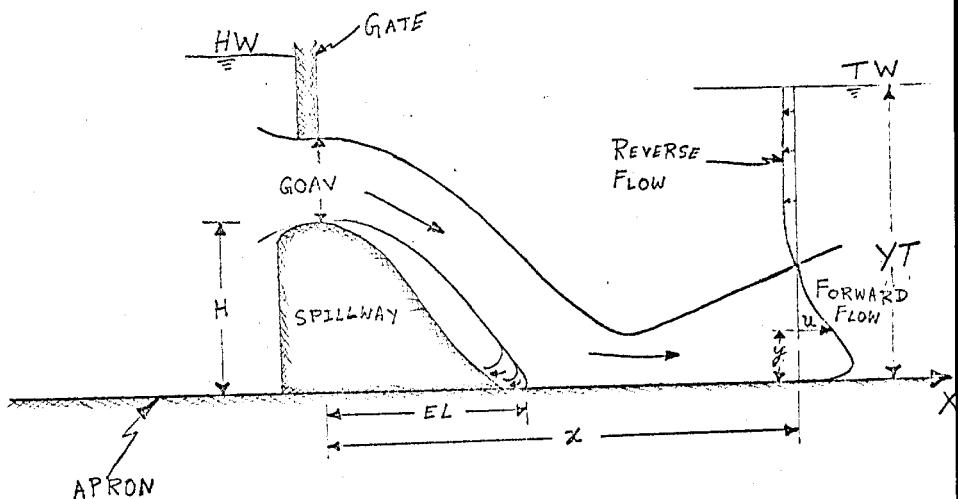
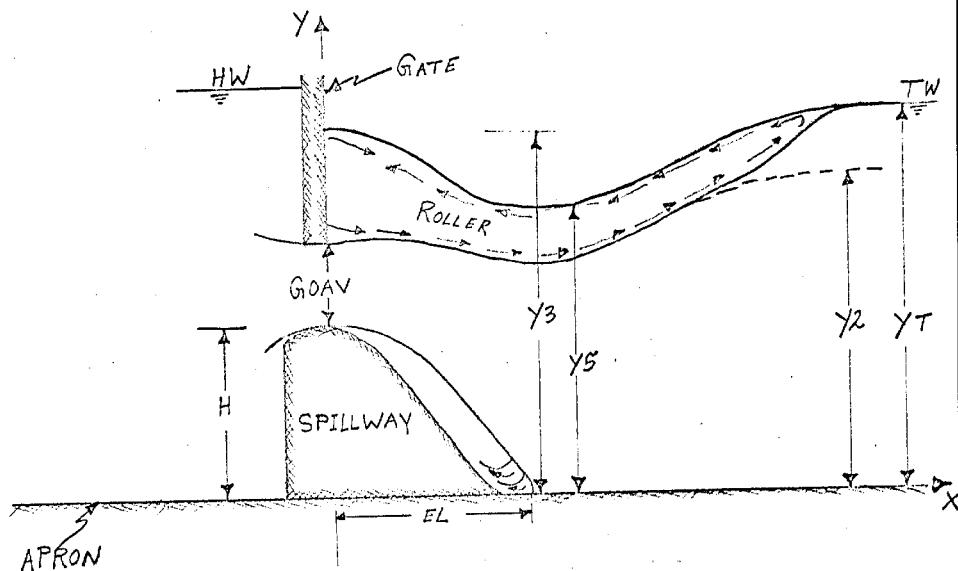


Figure 1. KISSIMMEE RIVER BASIN



a. Jet View Point



b. Hydraulic Jump View Point

Figure 2. Conceptual Definition of Energy Dissipation Phenomena

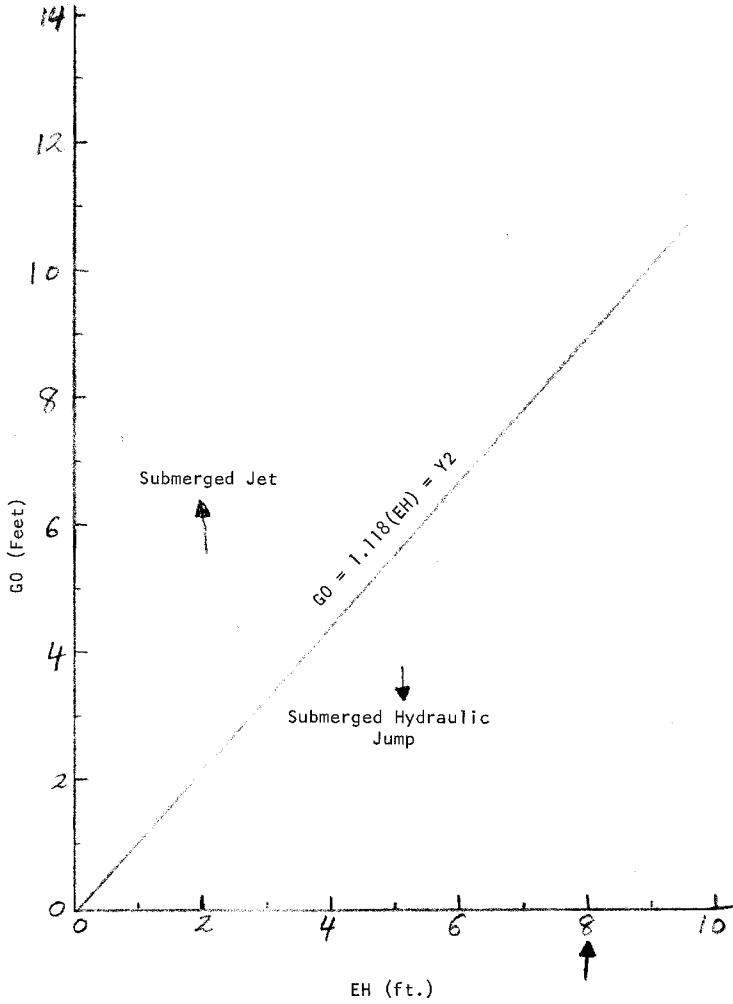


Figure 3. Graphical Representation of
Equation 12 (S-65D)

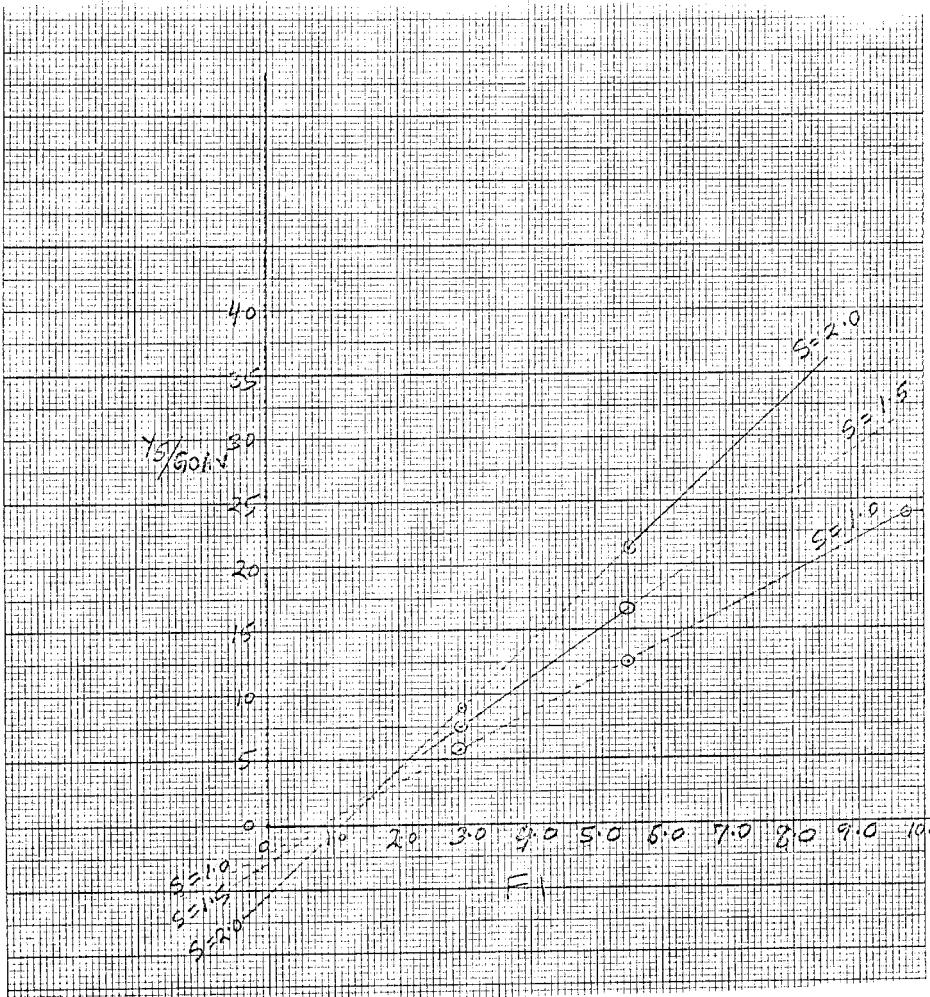


Figure 4. A Plot of $Y_5/G0AV$ vs. $F1$

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